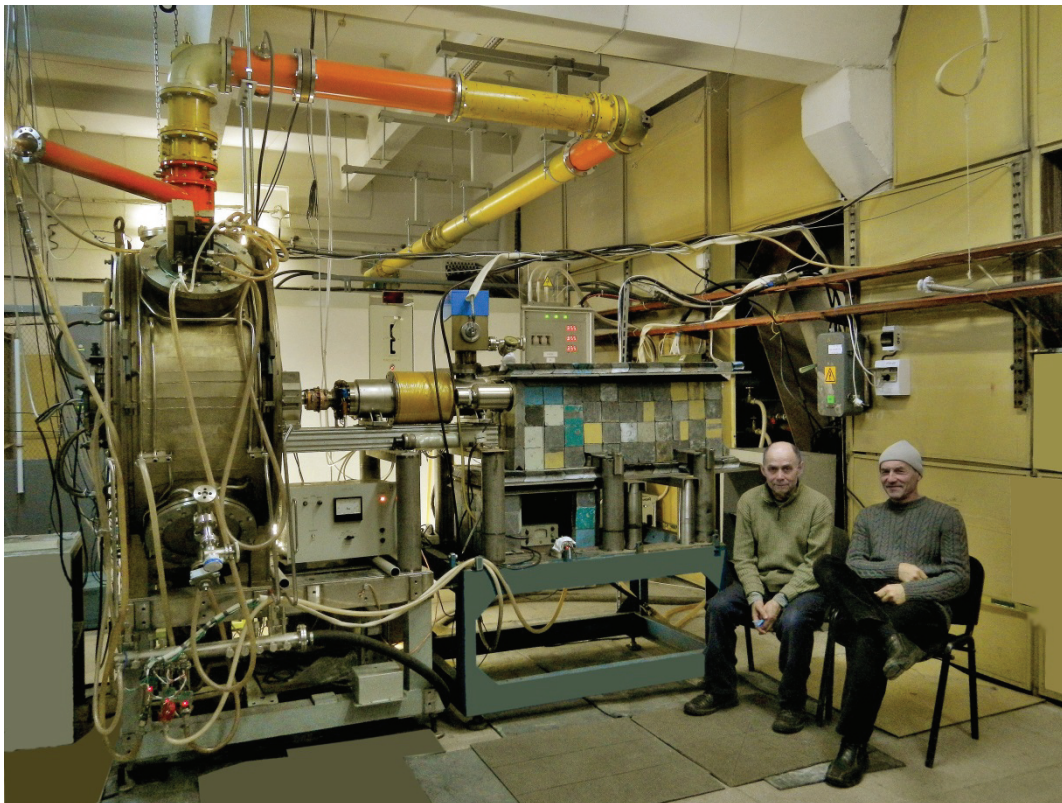


CW 100 mA Electron RF Gun for Novosibirsk ERL FEL

V. Volkov, V. Arbuzov, E. Kenzhebulatov, E. Kolobanov, A. Kondakov, E. Kozyrev, S. Krutikhin, I. Kuptsov, G. Kurkin, S. Motygin, A. Murasev, V. Ovchar, V.M. Petrov, A. Pilan, V. Repkov, M. Scheglov, I. Sedlyarov, S. Serednyakov, O. Shevchenko, S. Tararyshkin, A. Tribendis, N. Vinokurov
,BINP SB RAS, Novosibirsk

RF Gun Stand



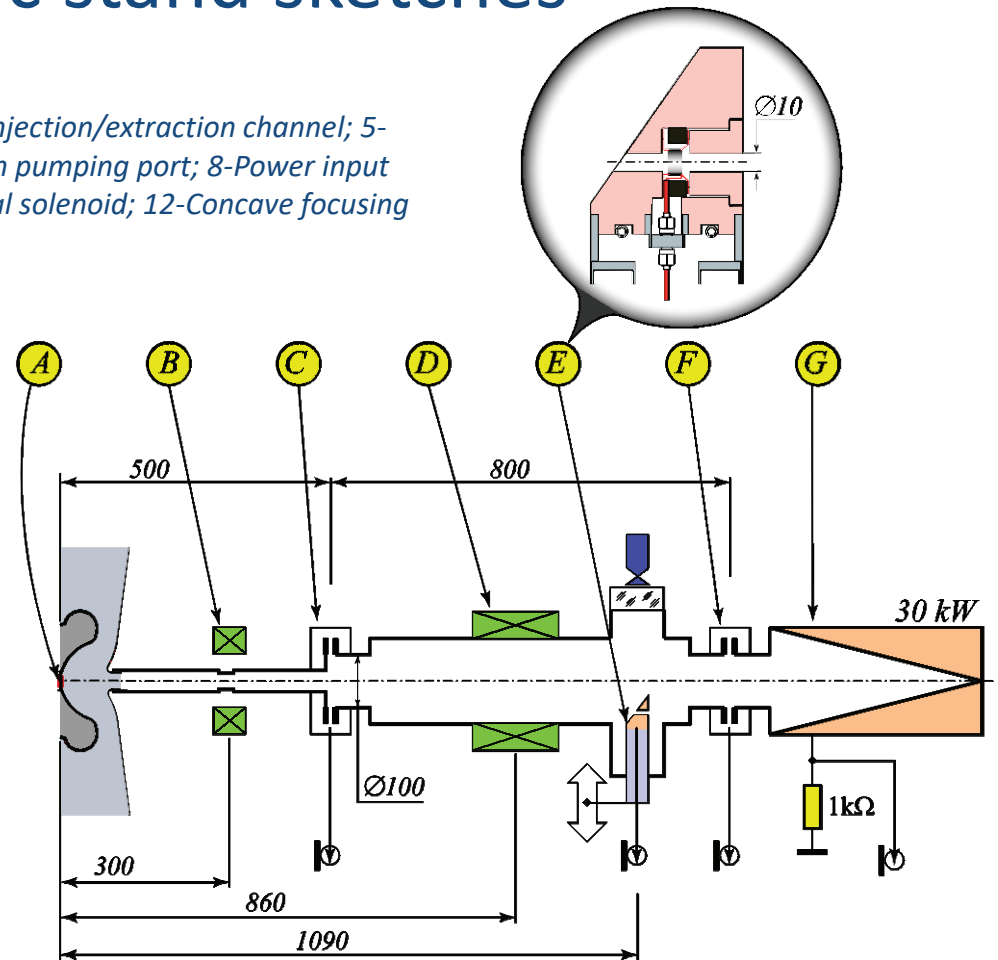
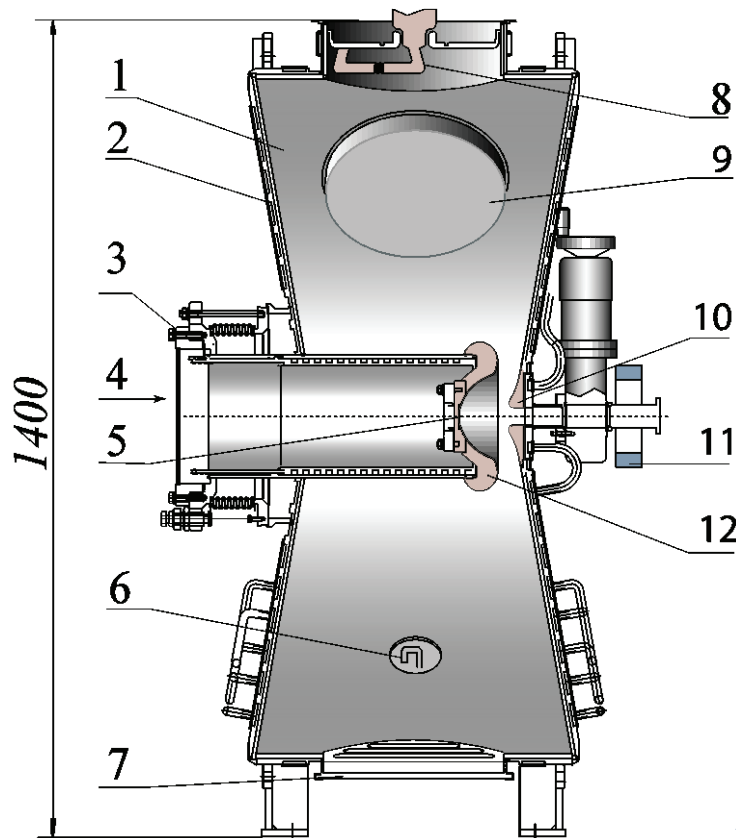
Measured rf gun characteristics

Average beam current, mA	0.003 ÷ 100
Bunch energy, keV	100 ÷ 400
Bunch duration (FWHM), ns	0.2 ÷ 2.0
Bunch emittance, mm mrad	10
Bunch charge, nC	0.3 ÷ 3.8
Repetition frequency, MHz	0.01 ÷ 90

Perfections: 30 kW water cooled beam dump, 5 cm lead radiation shield, wideband Wall Current Monitor (WCM), New scheme of cathode-grid modulator with GaN rf transistor, Transition radiation sensor, and pair of standard WCM

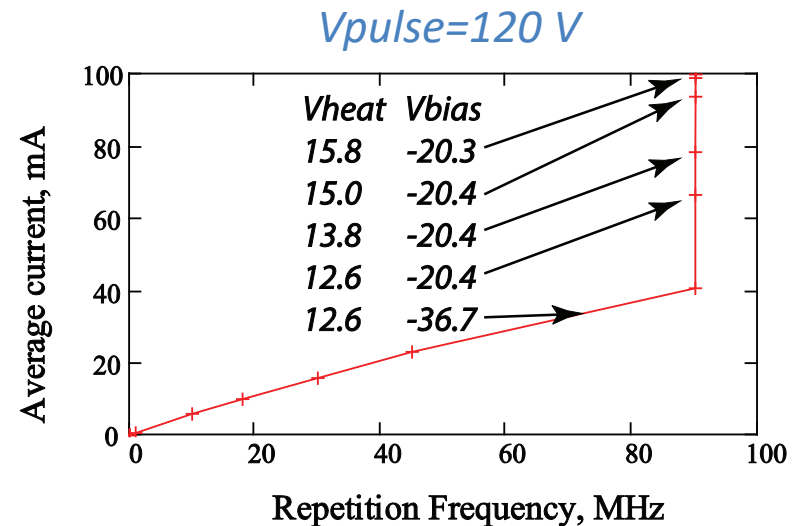
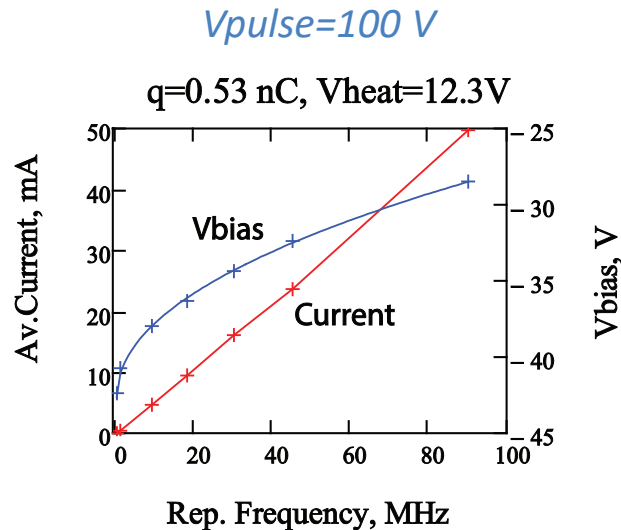
RF Gun and Diagnostic stand sketches

1- Cavity shell; 2-Cavity back wall; 3-Insert; 4-Cathode injection/extraction channel; 5- Thermionic cathode-grid unit; 6-Loop coupler; 7-Vacuum pumping port; 8-Power input coupler; 9-Sliding tuner; 10-Cone like nose; 11-Peripheral solenoid; 12-Concave focusing electrode



A-Thermionic cathode-grid unit; B-Emittance compensation solenoid; C-First Wall Current Monitor (WCM); D-Solenoid; E-Wideband WCM and transition radiation sensor; F-third WCM; G-Faraday cup and Water-cooled beam dump

Beam current vs Repetition frequency (F)



Typical mode of load rise

The current depends on the heating voltage (V_{heat}) because the cathode-grid distance is changed inversely of heating power due to thermal elongation.

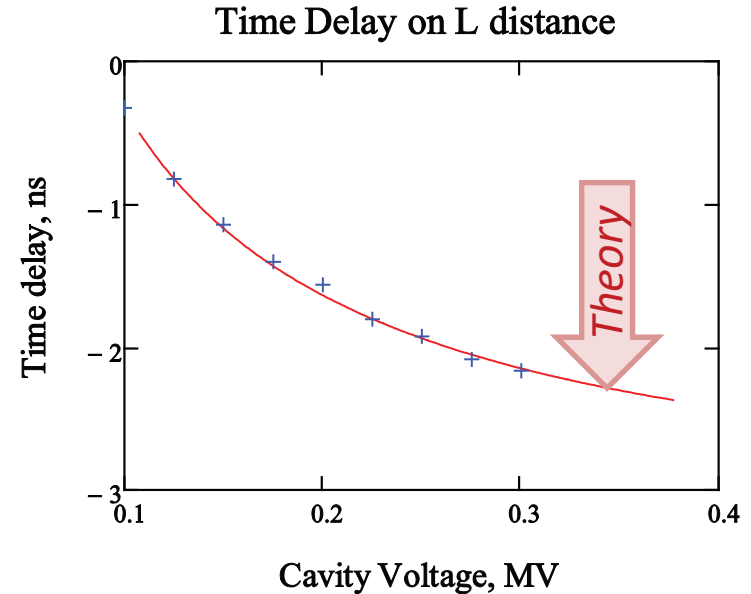
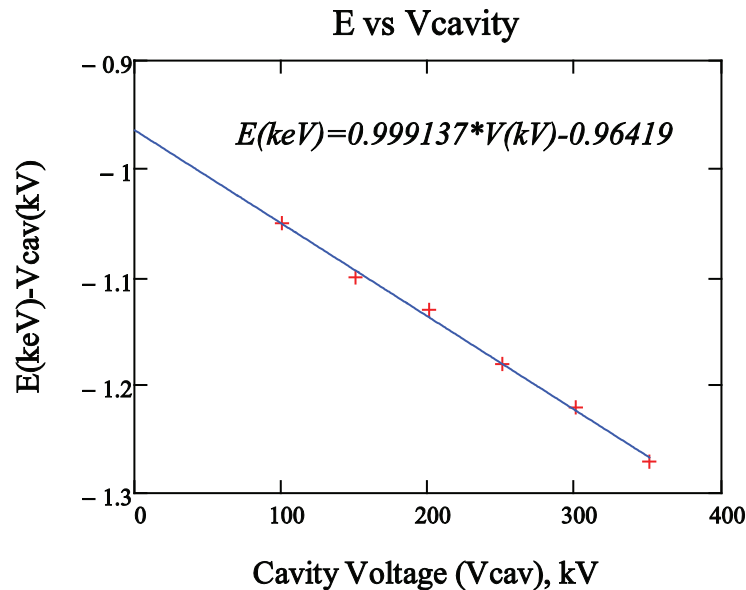
Optimal heating voltage for maximal cathode life time is $14 \div 15\text{ V}$ instead of 12.6 V established for rf tubes due to the presence of reflecting anode surface.

Also it depends on bias voltage (V_{bias}), and Modulator pulse voltage (V_{pulse})

Calibration of Cavity Voltage meter

with using of two wall current monitors

by time delay measuring between them



Calibrated $L = 0.96078 \text{ m}$

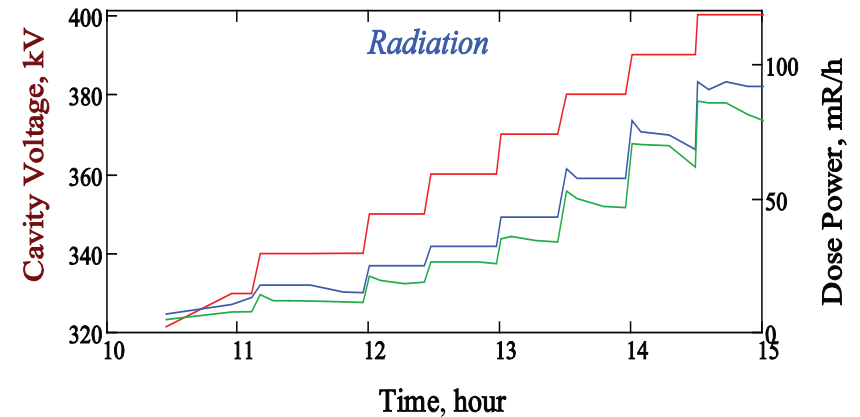
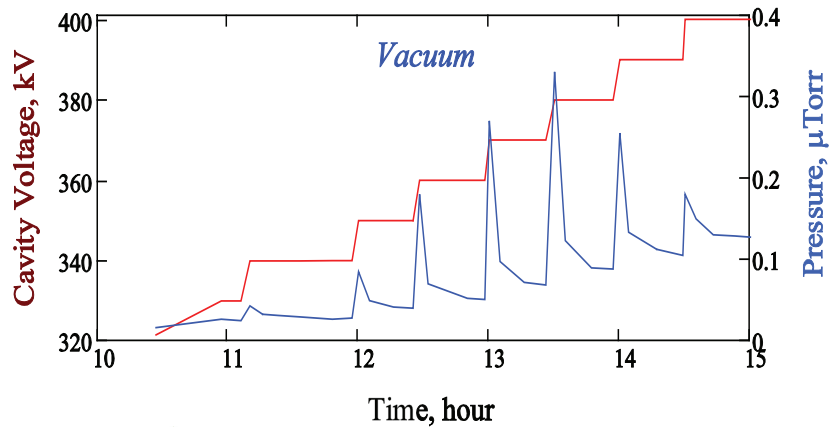
Bunch velocity (β) vs bunch energy (E)

$$\beta(E) := \sqrt{1 - \frac{1}{\left(1 + \frac{E}{mc^2}\right)^2}}$$

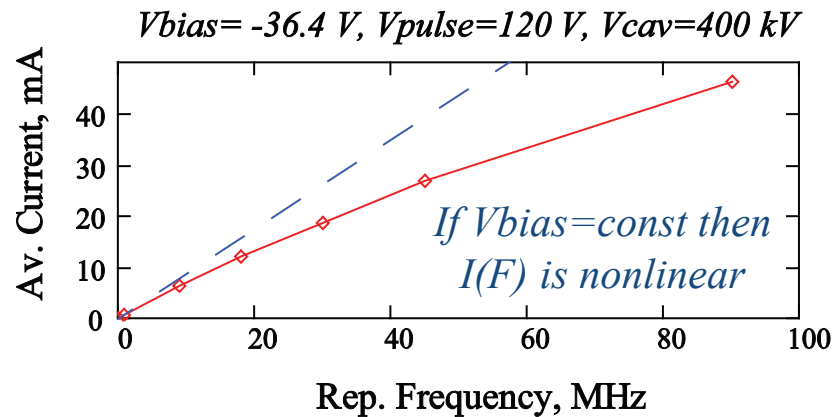
Time delay (T) vs Energy

$$T(E) := \frac{L \cdot 10^9}{299792458 \cdot \beta(E)}$$

Cavity testing up to 400 kV



$\frac{1}{2}$ hour
operation
time needs to
normalize
pressure level



Two radiation
sensors, one
at the
distance of
1.5 along
axis, second
2 m aside

Maximal Beam Dump power (30 kW) limits the current

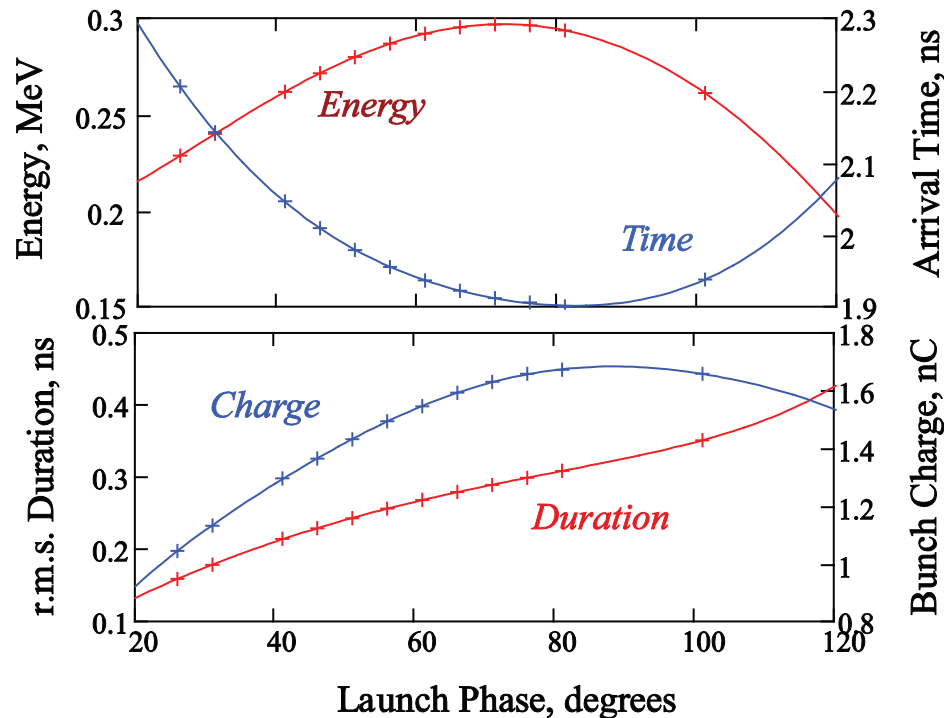
Launch Phase functions

determines bunching and jitter compensation effects.

Numerical calculation results

V_{cav}=300 kV

*Launch Pulse
duration is
1 ns FWHM*



*Launch Phase must be <120
degrees, otherwise there
appeared back
bombardment electrons
with maximal power of
300 W at the cathode.*

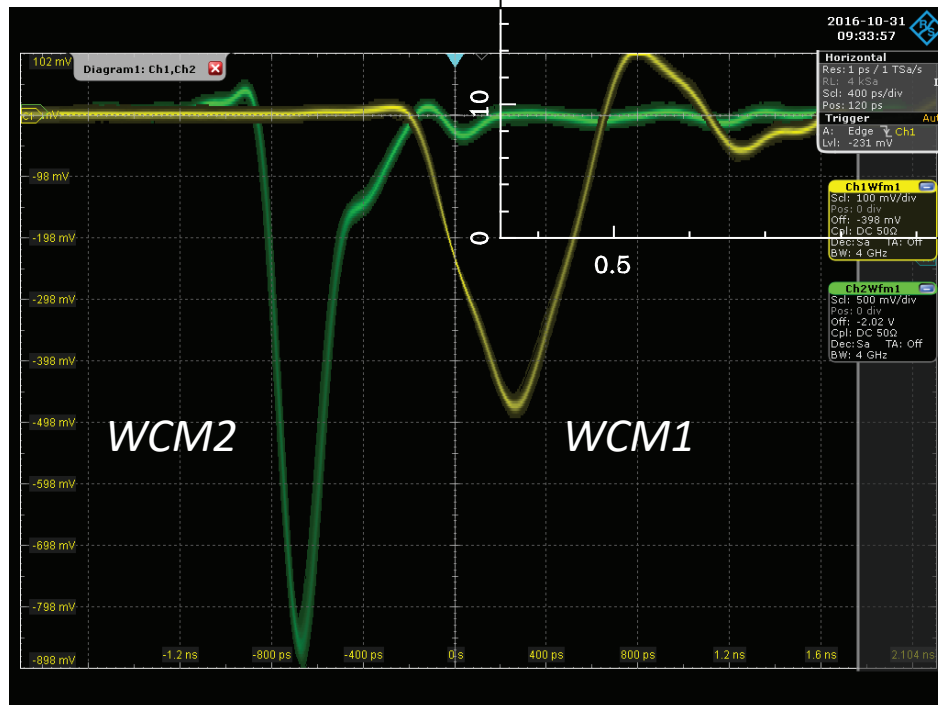
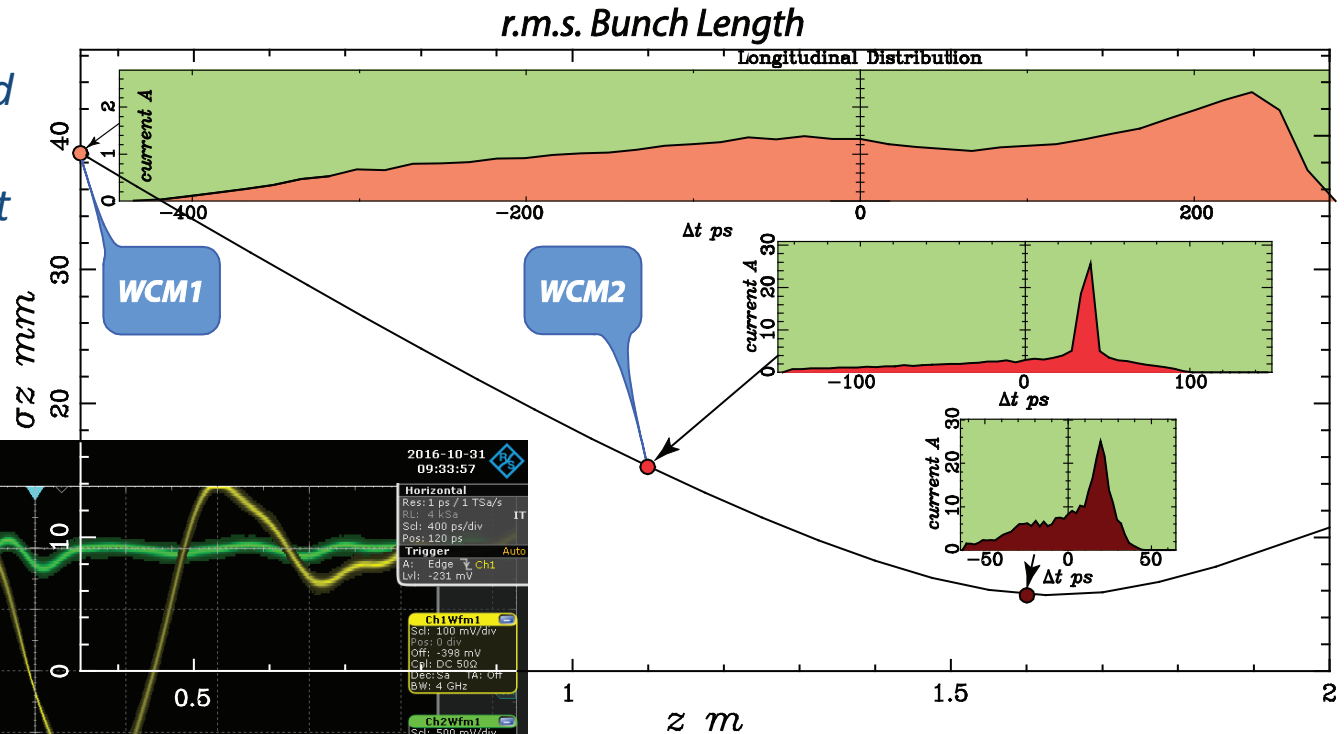
*Launch Pulse duration
determines minimal Launch
Phase >20 degrees*

Velocity Modulation Bunching

measured with wideband WCM2 and 4 GHz oscilloscope

Wall Current Monitor (WCM)

Frontal spike is formed into cathode-grid gap due to bunching effect there.



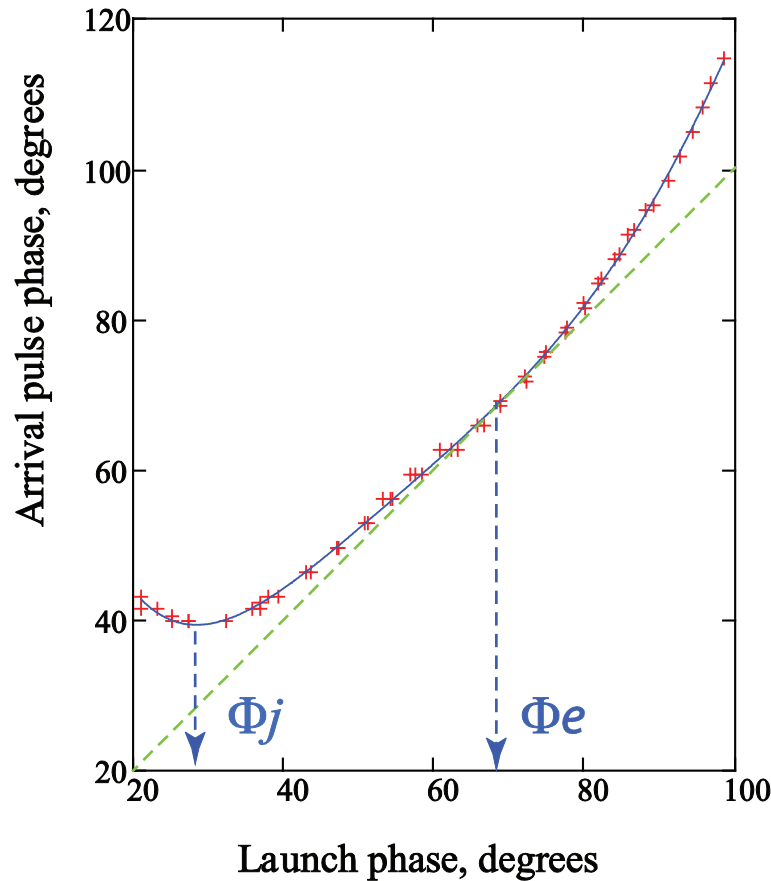
r.m.s. and FWHM be differ a lot

Numerical calculations predict FWHM $\tau_{FWHM}=20$ ps, unfortunately the 4 GHz oscilloscope cannot show pulses $\tau < 200$ ps, it all viewed as $\tau=200$ ps

Modulator Jitter Compensation

measured with Wall Current Monitor 3 ($L=1.2$ m)

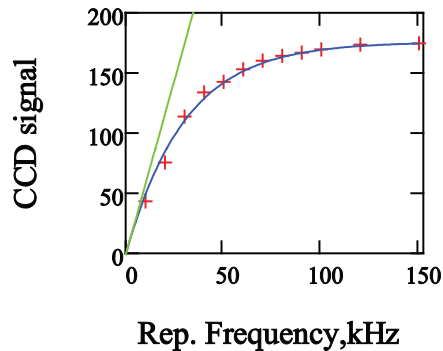
Arrival pulse phase is independent on Launch phase at $\Phi_j=27$ degrees, i.e. the jitter is compensated there



Maximal bunch energy is at $\Phi_e=68$ degrees where it coincides with arrival one by accurate within some constant

Emittance Measurements

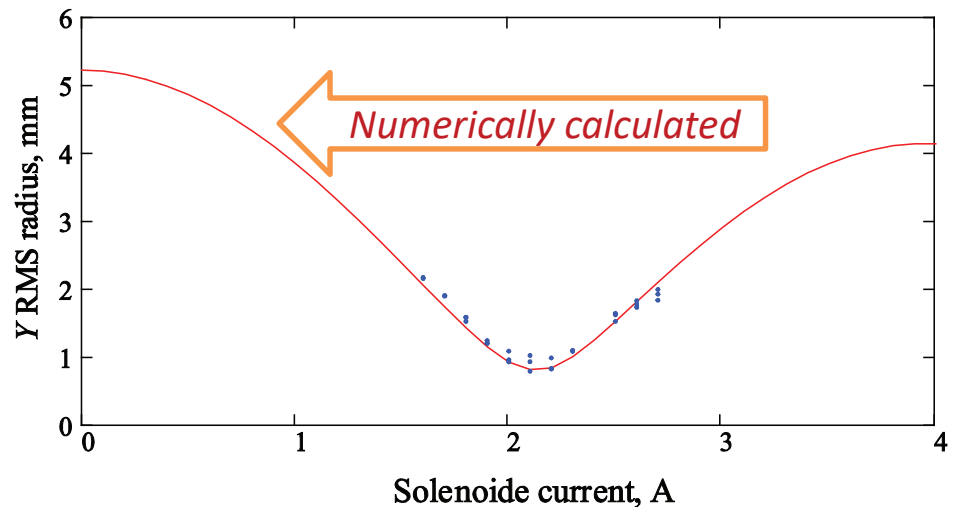
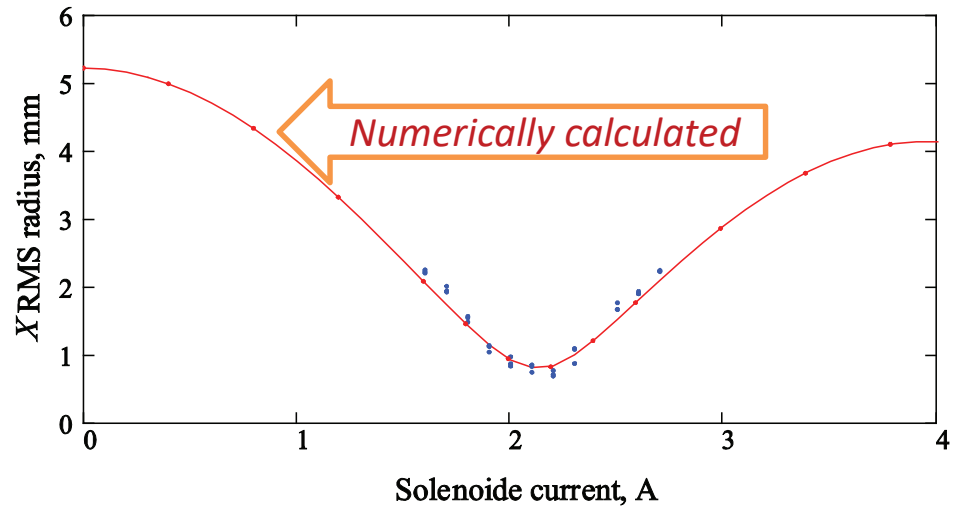
by solenoid focusing method with using transition radiation sensor



Measured normalized emittance $\varepsilon=15.5$ mm mrad can be compensated by solenoid focusing to $\varepsilon=10$ mm mrad.

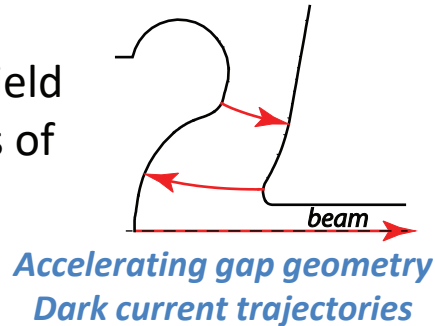
Numerical data processing of CCD camera image and distortion compensated optics were used.

Deviation of measured radius from calculated one is 9% so we can trust to our numerical calculations.



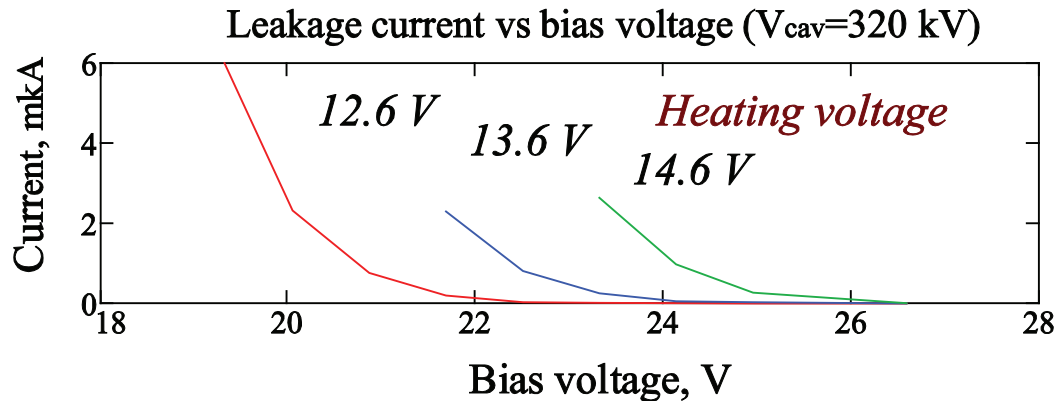
Dark and Leakage Currents

Two places with peak surface field of 10-14 MV/m are the sources of field emitted dark currents



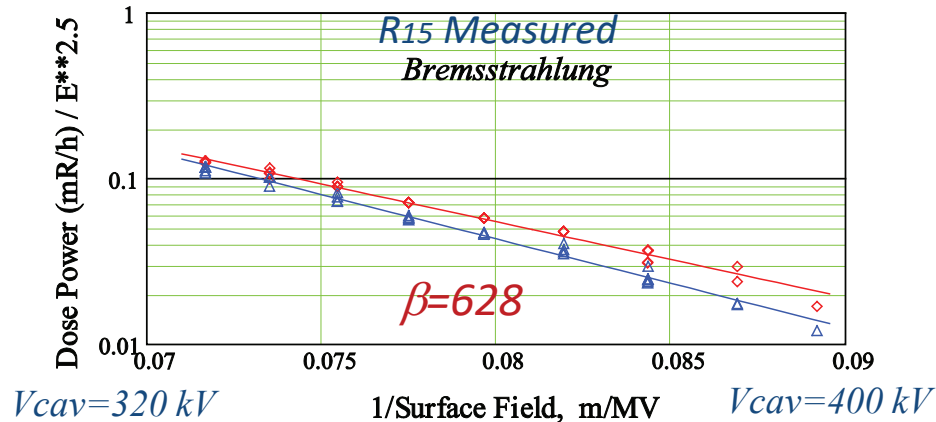
There are no dark currents in the beam absolutely

*Leakage current depends on heating voltage because cathode-grid gap changed.
To exclude leakage current from the beam we must chose proper bias voltage.*



Radiation Background

measured with radiation sensor at 1.5 m along axis and 2 m aside one



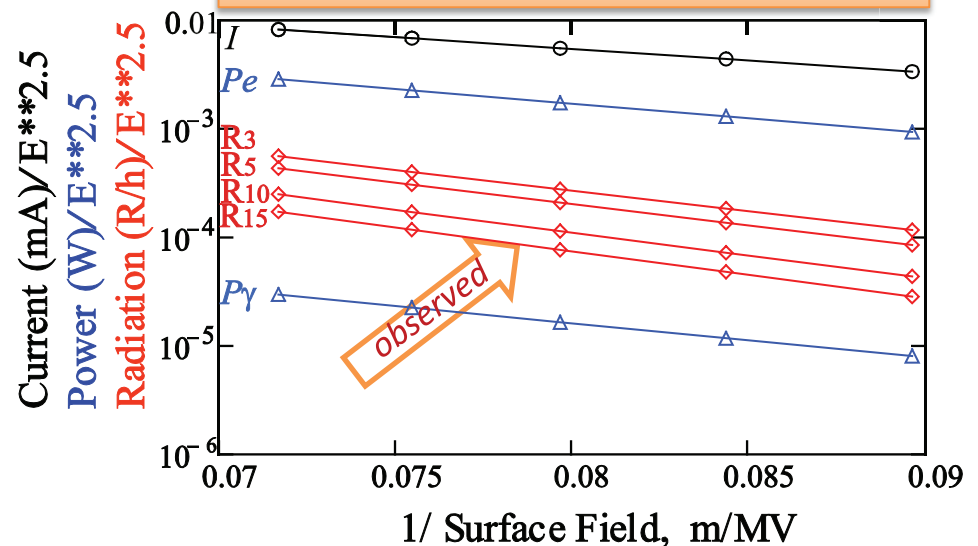
Fowler-Nordheim equation
 $\phi=4.5 \text{ eV}$, $B=6830$, $E \text{ (MV/m)}$

$$I \approx (\beta E)^{2.5} \exp\left(-\frac{B\phi^{1.5}}{\beta E}\right)$$

Enhancement factor (β) variance

Name		label	β
Dark Current of Field Emission		I	1264
Dark Current Power		Pe	1003
Bremsstrahlung Power		P_γ	865
Cu Shielded Dose Power	$d=3 \text{ mm}$	$R3$	721
	$d=5 \text{ mm}$	$R5$	695
	$d=10 \text{ mm}$	$R10$	649
	$d=15 \text{ mm}$	$R15$	628

All Calculated have F-N nature!



Thank you for your attention!