



Magneto-optic Structure for Synchrotrons with Negative Momentum Compaction Factor

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In what cases the structure with such properties is necessary to us?

- To exclude the transition energy crossing
- To have the higher collective instability threshold
- To match in longitudinal plane the different accelerators
- To adjust the different local slip factor for the optimized stochastic cooling
- To avoid the sextupoles in the synchrotron light sources



The requirements to the absolute value of slip factor:

- I. For many collective instabilities the threshold is proportional **the slip factor**

$$\eta = 1/\gamma_{tr}^2 - 1/\gamma^2$$

For instance, from the Landau damping theory the stability requires a minimum spread in incoherent frequencies for longitudinal motion

$$\left(\frac{\delta\omega}{\omega}\right)^2 = \eta^2 \left(\frac{\sigma}{p}\right)^2 \geq \frac{eI_{peak} |\eta|}{2\pi m_0 c^2 \gamma \beta^2} \left| \frac{Z_L(n)}{n} \right|$$

So, **the absolute value of slip factor module** is desirable to have as large as possible.

- II. The transition energy crossing $\gamma = \gamma_{tr}$ ($\eta = 0$) has to be excluded, since the longitudinal stability disappears.



The requirements to the absolute value of slip factor:

III. The longitudinal beam size is determined by the ratio

$$\Delta\phi_{\max} = \pm W \sqrt{\frac{2\pi h |\eta| \Omega_{rev}}{eV p_s R \cos\phi_s}}$$

and **the absolute value of slip factor** can be used as additional factor for the matching between two accelerators or/and control of beam sizes during acceleration.



The requirements to the sign of slip factor:

IY. Many investigations devoted to the beam stability declare that the beam is more stable below the transition energy

$$\gamma < \gamma_{tr} \quad \rightarrow \quad \eta < 0$$

Besides, in the synchrotron light sources the natural chromaticity accords to the transverse stability criteria for the negative slip factor. So, if the lattice has the imaginary gamma transition

$$\eta = 1/(iG_{tr})^2 - 1/\gamma^2 < 0$$

all requirements can be fulfilled!!!



History of lattice with imaginary gamma-transition

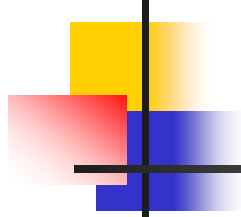
- **in 1955 Vladimirsky and Tarasov** suggested method to get the imaginary γ_{tr} and did it by increasing number of “compensating magnets” with a reversed field but the same gradients, as would be called for in a design with no compensating magnets and where ω is slightly more than the tune.
- **In 1958 Courant and Snyder** quantitatively described this idea of the negative momentum compaction factor.
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- Later many authors tried to realize this idea of imaginary transition energy in different lattices:
 - In 1972 Lee Teng** suggested the modular method;
 - In 1974 Bruck** developed the regular focusing structure with the “missing” magnet cell in **Saturne II**;
 - In 1983 Franczak, Blasche, Reich** excited superperiodically the quadrupoles for the **SIS-18**;
 - In 1985 Gupta, Botman, Craddock** at an initial design stage of the **TRIUMF KF** used missing magnet;



History of lattice with imaginary gamma-transition

- In **1989** **Senichev, Golubeva, Iliev** suggested the “resonant” lattice for **Moscow Kaon Factory**;
- In **1992** **Ng, Trbojevic, Lee** applied the modular method of Lee Teng for MB (**FNAL**);
- In **1992** **U.Wienands, N.Golubeva, A.Iliev, Yu.Senichev, R.Servranckx** adopted the “resonant” lattice for Kaon Factory (**TRIUMF**);
- In **1993** **E. Courant, A. Garen and U. Wienands** took the “resonant” lattice for **LEB (SSC)**;
- In **1995** **Y. Senichev** wrote the “resonant” lattice theory and applied it for Main Ring (**JPARC**);
- In **2000** **H. Schönauer, Yu. Senichev** et al., The “resonant” lattice for Proton driver for a **Neutrino Factory (CERN)**
- In **2007** **Y.Senichev** et al., The “resonant” lattice for **Super-Conducting option of HESR (FAIR)**
- In **2008** The “resonant” lattice is one of the candidate for **PS2 (CERN)**

Regular and Irregular lattices



Momentum Compaction factor (MCF):

$$\alpha = \frac{1}{2\pi} \int_0^C \frac{D(\mathcal{G})}{\rho(\mathcal{G})} d\mathcal{G}$$

where the dispersion $D(\theta)$ is:

$$D'' + K(\mathcal{G})D = \frac{1}{\rho(\mathcal{G})}$$

If in the optics with eigen frequency ν the curvature $\sigma(\theta)$ is modulated with frequency ω

$$\sigma(\mathcal{G}) = 1/\rho(\mathcal{G}) \sim \boxed{Be^{i\omega\mathcal{G}}} + 1/\bar{R}$$

the dispersion solution and Momentum Compaction Factor are:

$$D(\mathcal{G}) \sim Ae^{i\nu\mathcal{G}} + \boxed{\frac{B}{\nu^2 - \omega^2} e^{i\omega\mathcal{G}}} + \bar{D}$$

$$\alpha = \frac{\bar{D}}{\bar{R}} + \frac{\overline{\tilde{D}(\mathcal{G}) \cdot \tilde{r}(\mathcal{G})}}{\bar{R}}$$



Regular lattice

In conventional regular FODO lattice $\omega \gg v$.

Therefore the dispersion oscillates with eigen frequency (tune) ν :

$$D(\mathcal{G}) \approx Ae^{i\nu\mathcal{G}} + \bar{D}$$

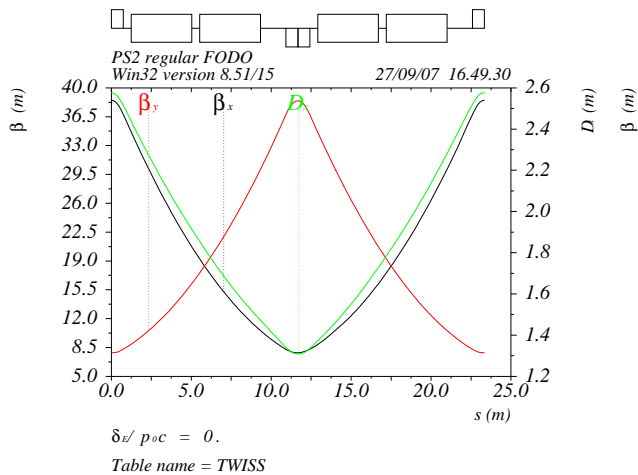
Then Momentum Compaction Factor (MCF) is determined by average values ratio:

$$\alpha = \frac{\langle D(\mathcal{G}) \rangle}{\langle \rho(\mathcal{G}) \rangle} = \frac{\bar{D}}{\bar{R}} \approx \frac{1}{\nu^2}$$

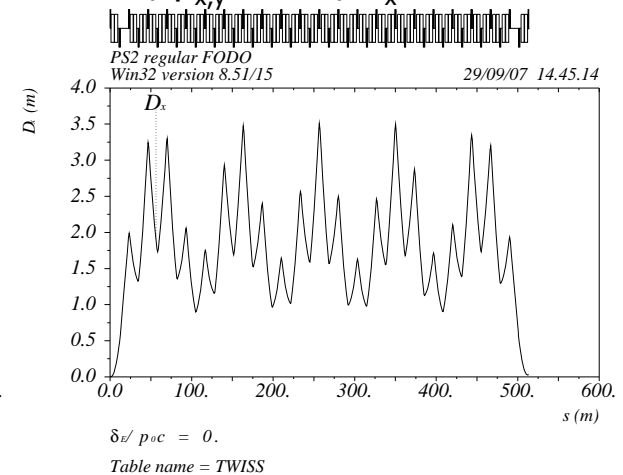
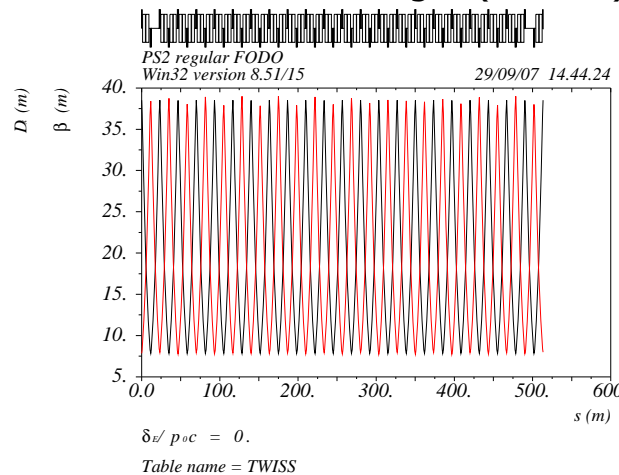
and the maximum energy of accelerator without the transition energy crossing is determined by $\gamma_{\max} \approx \nu$ or for the $\pi/2$ phase advance FODO lattice $\gamma_{\max} \approx N_{\text{cell}}/4$

Regular lattice for PS2 (3-50 GeV) based on FODO cells with real transition energy $\gamma_{tr} \sim 10$ (parameters taken from PS2 report by Wolfgang Bartman)

FODO cell with magnet length
 $L=3.79\text{m}$ and drift 1.6m



Arc based on FODO lattice with tune per cell $\sim 84^0$
The total length (22 cells) 513.5 m ; $\beta_{x,y} \sim 39\text{ m}$, $D_x \sim 3.5\text{m}$



To make higher γ_{tr} than 50 the total number of FODO cells has to be increased up to 110 per arc

Conclusion:

The only possible solution is the imaginary gamma transition with the wide control of its absolute value



Irregular lattice with curvature modulation (missing magnet lattice)

In case of eigen frequency ν is enough close to the curvature oscillation with the superperiodicity frequency $S = \nu + \delta$, the dispersion oscillates with the forced frequency $\omega = S$:

$$D(\mathcal{G}) \sim \frac{B}{\nu^2 - S^2} e^{i\mathcal{G}S} + \bar{D}$$

In irregular structure MCF depends on the curvature modulation B and detuning $\delta = S - \nu \ll \nu$:

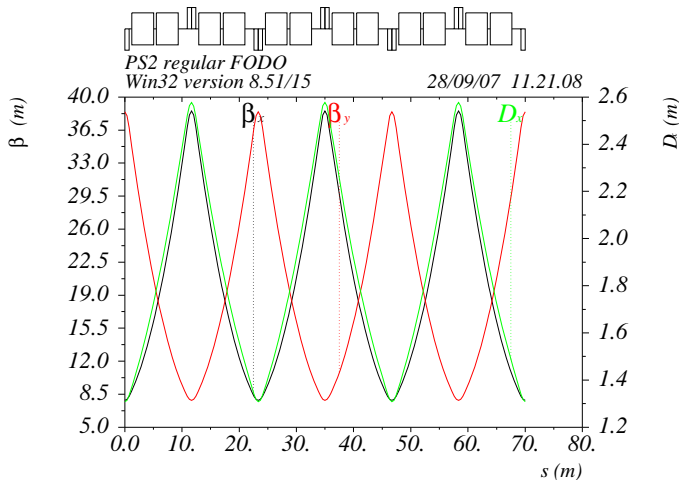
$$\alpha \approx \frac{1}{\nu^2} - \frac{B^2}{2\delta\nu}$$

Irregular PS2 lattice with curvature modulation ("missing" magnet lattice)

3 regular FODO cells with total length

$$3 \times 23.21 \text{ m} = 69.63$$

$$L_{\text{mag}} = 3.7 \text{ m}$$

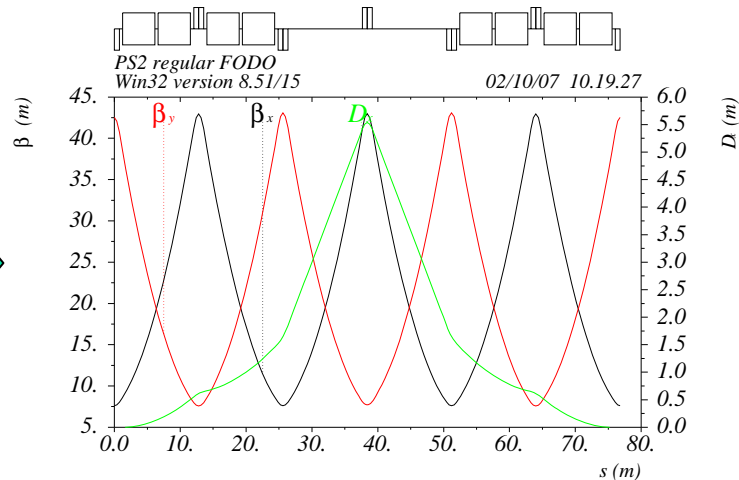


$$\delta\varepsilon/p_{oc} = 0.$$

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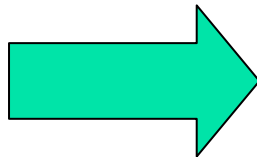
3 irregular FODO missing magnet cells
with total length 76.8 m

$$L_{\text{mag}} = 4.9 \text{ m}$$



$$\delta\varepsilon/p_{oc} = 0.$$

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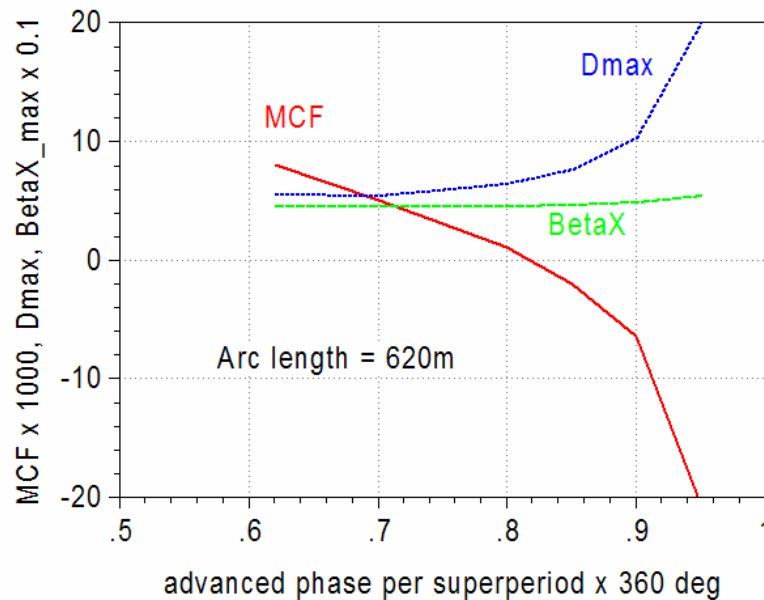


Zero momentum compaction factor in the “missing” magnet lattice

In arc length ~ 620 m $MCF < 0$ at $v > 0.82$

In arc length ~ 600 m $MCF < 0$ at $v > 0.875$

In arc length ~ 580 m $MCF < 0$ is not reached



Conclusion

“Missing magnet” lattices has

advantages:

- practically does not perturb β -functions;

disadvantages:

- requires the large phase advance value,
- significantly increases the arc length.

Results of "Resonant" lattice theory:

From the article: Yu. Senichev, A "resonant" lattice for a synchrotron with a low or negative compaction factor, KEK Preprint 9740, 1997 and JETP, v. 132, n. 5, p.1127

The solution of equation

$$\frac{d^2 D}{ds^2} + [K(s) + \varepsilon k(s)]D = \frac{1}{\rho(s)}$$

with modulation of gradient and curvature:

$$\varepsilon k(\phi) = \sum_{k=0}^{\infty} g_k \cos k\phi; \quad \frac{1}{\rho(\phi)} = \frac{1}{R} \left(1 + \sum_{n=1}^{\infty} r_n \cos n\phi \right)$$

gives the expression for MCF:

$$\alpha_s = \frac{1}{\nu^2} \left\{ 1 + \frac{1}{4 \cdot (1 - kS/\nu)} \cdot \left[\left(\frac{\bar{R}}{\nu} \right)^2 \frac{g_k}{[1 - (1 - kS/\nu)^2]} - r_k \right]^2 \right\}$$

1. Negative momentum compaction factor with minimum circumference and control of gamma transition in a wide region

The lattice has the remarkable feature:

The gradient and the curvature modulation amplify each by other if they have opposite signs,

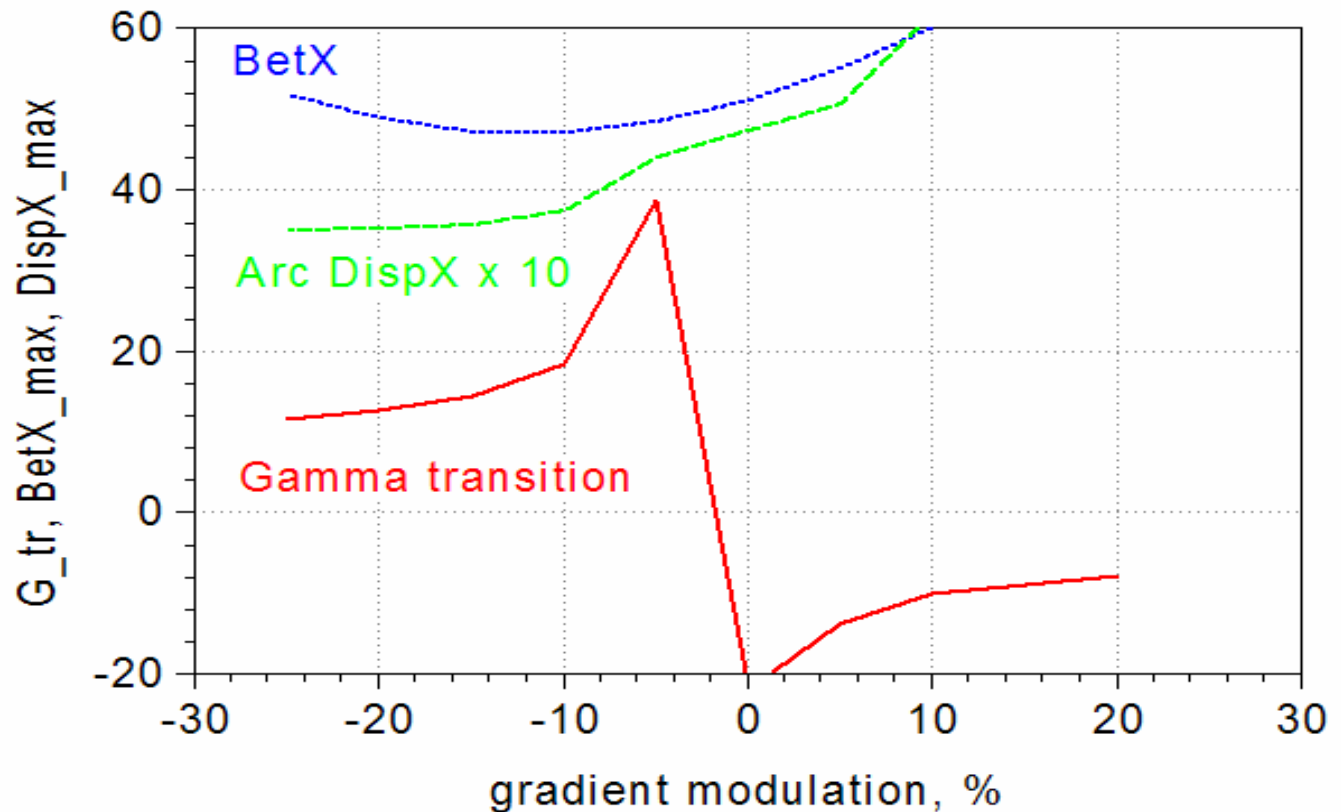
$$g_k \cdot r_k < 0$$

The ratio between them is desirable to have:

$$|r_k| \leq \left(\frac{\bar{R}}{\nu} \right)^2 \left| \frac{g_k}{1 - (1 - kS)^2} \right| \quad \text{and} \quad \frac{1}{4(kS/\nu - 1)} \cdot \left(\frac{g_k}{[1 - (1 - kS/\nu)^2]} - r_k \right)^2 \approx 2$$

On the contrary they can compensate each other when they have the same sign.

Then gamma transition varies in a wide region
from $\gamma_{tr} \sim v_x$ to $\gamma_{tr} \sim iv_x$
with quadrupole strength variation only!!!





2. Dispersion-free straight section without special suppressor;

3. Low sensitivity to multipole errors and sufficiently large dynamic aperture

First condition:

To provide a **dispersion-free straight section**, the arc consisting of S_{arc} superperiods must have a 2π integer phase advance.

Second condition:

In order to drive the momentum compaction factor, the horizontal betatron tune ν_{arc} must be less than the resonant harmonic of perturbation kS_{arc} , and the difference between them has to be of a minimum integer value. We take $\nu_{arc} - kS_{arc} = -1$

Third condition:

The arc superperiodicity S_{arc} has to be even and ν_{arc} is odd.

Compensation of sextupole non-linearity

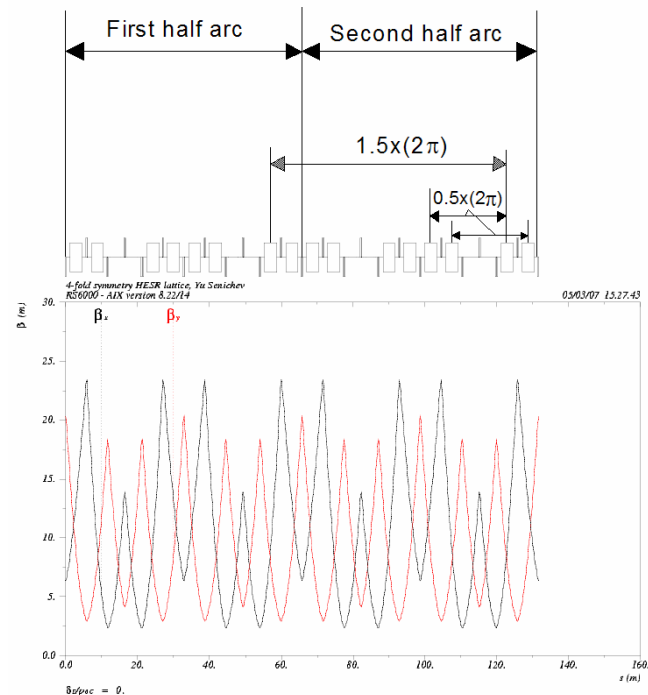
- In that case the phase advance between any two cells located in the different half arcs and separated by $\frac{S_{arc}}{2}$ number of

superperiods is then equal to

$$\frac{v_{arc}}{S_{arc}} \cdot \frac{S_{arc}}{2} = \frac{v_{arc}}{2} = \pi + 2\pi n$$

- the total multipole of third order is canceled:

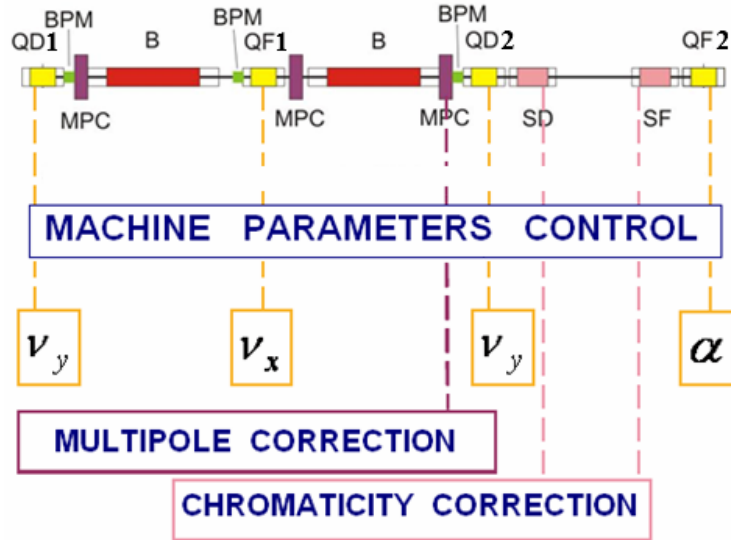
$$M_3^{total} = \sum_{n=0}^N S_{x,xy} \beta_x^{l/2} \beta_y^{m/2} \exp(in(l\mu_x + m\mu_y)) = 0$$



4. Minimum families of focusing and defocusing quadrupoles and separated adjustment of gamma transition, horizontal and vertical tunes

1/2 SUPERPERIOD

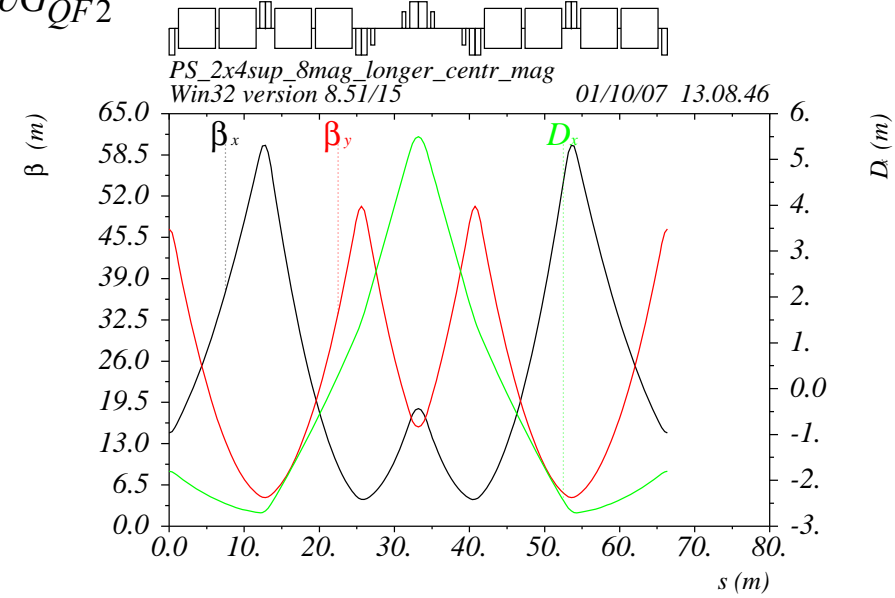
- B bending magnet
- QD defocussing quadrupole
- QF focussing quadrupole
- SD defocussing sextupole
- SF focussing sextupole
- MPC multipole corrector (steerer, trim quadrupole etc)
- BPM beam position monitor



$$1. \frac{\partial v_x}{\partial G_{QF1}} > \frac{\partial v_x}{\partial G_{QF2}} \gg \frac{\partial v_x}{\partial G_{QD}}$$

$$2. \frac{\partial v_y}{\partial G_{QD}} \gg \frac{\partial v_y}{\partial G_{QF1}} \approx \frac{\partial v_y}{\partial G_{QF2}}$$

$$3. \frac{\partial \alpha}{\partial G_{QF2}} \gg \frac{\partial \alpha}{\partial G_{QF1}} \approx \frac{\partial \alpha}{\partial G_{QD1}}$$



$\delta_E / p_{oc} = 0.$
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5. Convenient sextupole chromaticity correction scheme

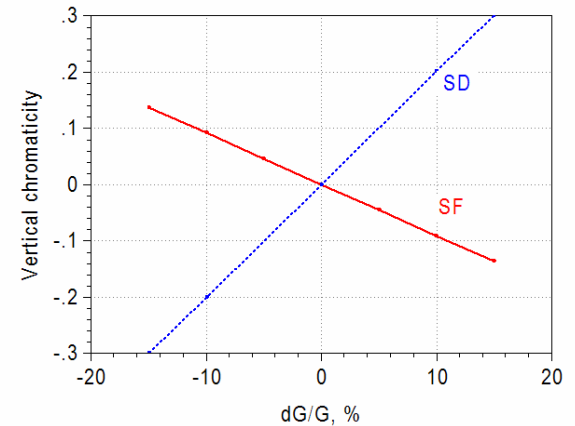
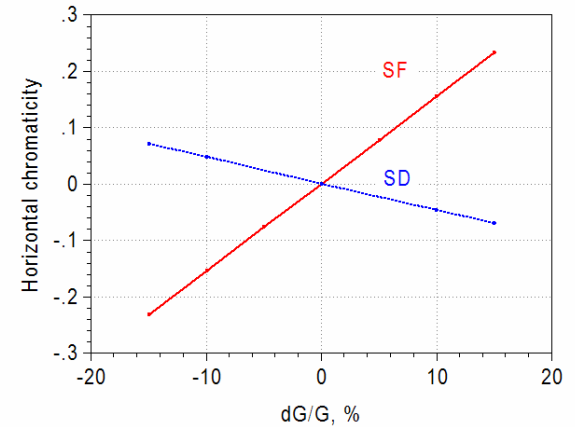
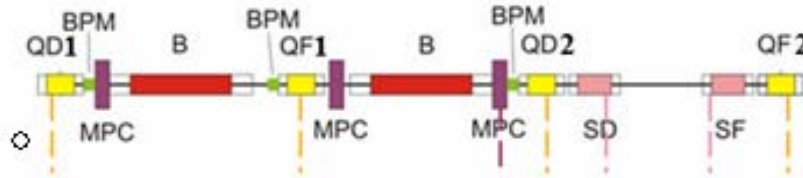
Total chromaticity

$$\frac{\partial \nu_{x,y}}{\partial \delta} = -\frac{1}{4\pi} \int_0^C \beta_{x,y}(s) K_{x,y}(s) ds$$

■ Sextupole compensation

$$\frac{\partial \nu_{x,y}}{\partial \delta} = \pm \frac{1}{4\pi} \int_0^C \beta_{x,y}(s) \cdot D(s) \cdot S(s) ds$$

Half-superperiod





6. Independent optics parameters of arcs and straight sections

- Tune arc does not depend on the transition energy and is kept constant;
- Special insertion on the straight section allows to match the $\beta_{x,y}$ -functions between arcs and straight sections;
- Dispersion-function on the straight sections always equal zero;
- All high order non-linearities are compensated inside each arc.



The "golden" ratio between S_{arc} and v_{arc}

To fulfill all mentioned conditions we have to have the strictly fixed sets of S_{arc} and v_{arc} :

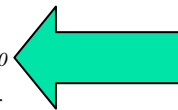
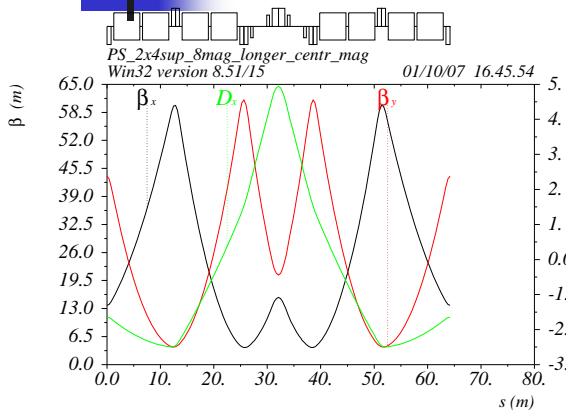
4:3; 6:5; 8:6; 8:7,.... and so on.

↓

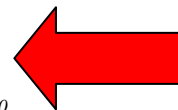
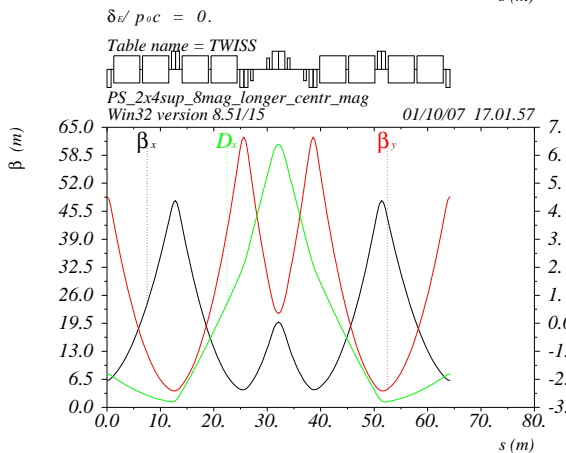
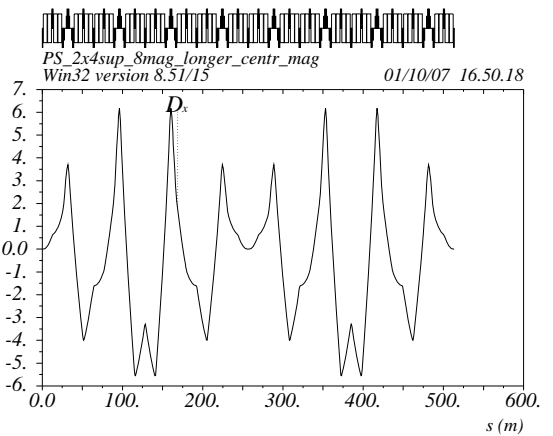
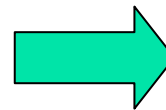
4:3 + 4:3

8 superperiodical lattices (for PS2)

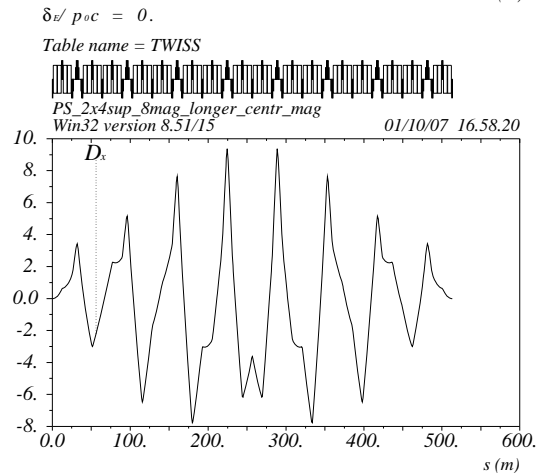
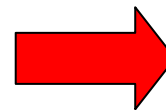
with $\nu_{arc}=6$ and $\nu_{arc}=7$



$\nu_{arc}=6$:



$\nu_{arc}=7$:



$\delta_z/p_{oc} = 0$.

Table name = TWISS



The second order non-linearity

- After some canonical transformation we can get the second order approach of Hamiltonian in the next view:

$$H(J_x, \mathcal{G}_x, \theta_x, J_y, \mathcal{G}_y, \theta_y) =$$

$$v_x J_x + v_y J_y + \sum g(M, N, n_1, n_2, p) J_x^{M/2} J_y^{N/2} \exp i(n_1 \mathcal{G}_x + n_2 \mathcal{G}_y - p\theta)$$

- Now let us suppose that we are some where around of the third order resonance:

$$3\bar{v}_x = p_0,$$

$$\bar{v}_x = v_x + \Delta$$

- the Hamiltonian takes a view

$$H_1(J, \psi, \theta) = v_x J_x + v_y J_y + \frac{1}{2} J_x^{3/2} \{h_{3030p_0} \exp i(3\psi_x - p_0\theta) + c.c.\} +$$

$$\zeta_x J_x^2 + \zeta_{xy} J_x J_y + \zeta_y J_y^2$$



The higher order resonance excitation and non-linear tune shifts

- the coefficients $\zeta_x, \zeta_y, \zeta_{xy}$ are the non-linear tune shifts:

$$\zeta_x = \zeta_x^{sex} + \zeta_x^{oct}$$

$$\zeta_{xy} = \zeta_{xy}^{sex} + \zeta_{xy}^{oct}$$

$$\zeta_y = \zeta_y^{sex} + \zeta_y^{oct}$$

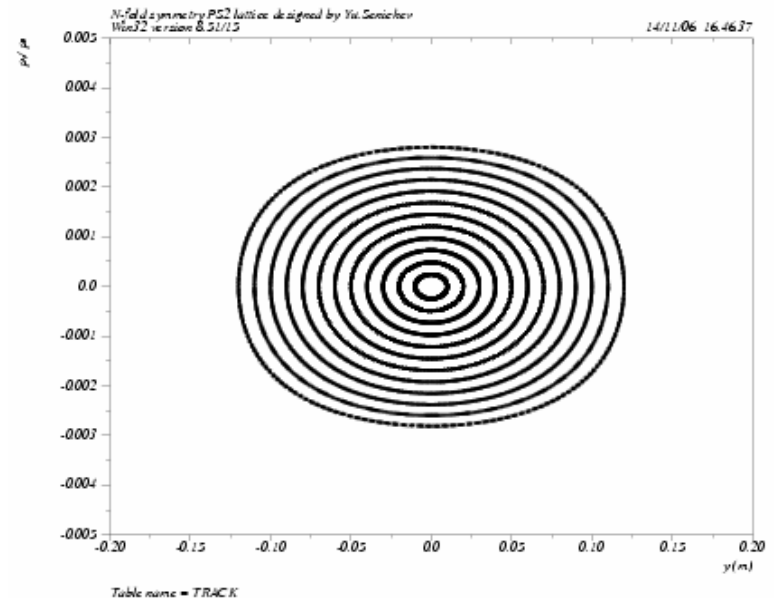
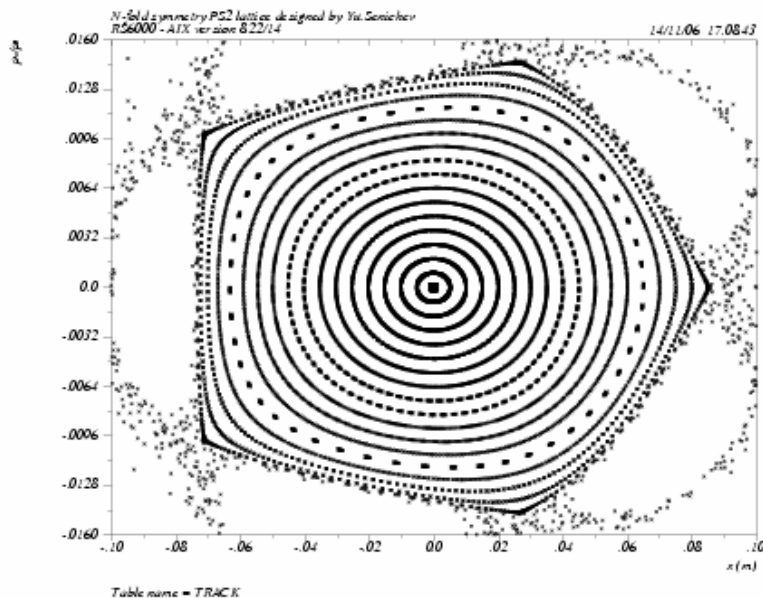
- as example

$$\zeta_x^{sex} = -\frac{3}{4} \left[\sum_{p=-\infty}^{\infty} \frac{|h_{3010p}|^2}{v_x - p} + \sum_{\substack{p=-\infty \\ p \neq p_0}}^{\infty} \frac{3|h_{3030p}|^2}{3v_x - p} \right]$$

$$\zeta_x^{oct} = \frac{1}{32\pi\Delta^2} \int_0^{2\pi} \beta_x^2 O_x R d\theta$$

Dynamic aperture after chromaticity compensation (for PS2)

- We calculated the dynamic aperture by the numerical tracking for one of options using MAD. It is \sim Hor.=600 mm mrad and Ver.=400 mm mrad



Pro and Con for two types of lattices: "resonant" and regular FODO (for PS2)

	Resonant lattice with ρ and gradient modulation		Regular FODO lattice with suppressors	
	Advantages	disadvantages	advantages	disadvantages
Crossing W_{transit}	No			Yes, at $\gamma \sim 10$
Variability and controll of W_{transit}	Yes			No
Necessity of dispers. suppressor	No			Yes
Decoupling between arc and str. section	Yes			No
Free space on arcs	$\sim 16 \times 3 \text{ m}$			$2 \times 8 \text{ m}$
Sextupole comp. on arc	Yes			No

Pro and Con for two types of lattices: "resonant" and regular FODO (PS2)

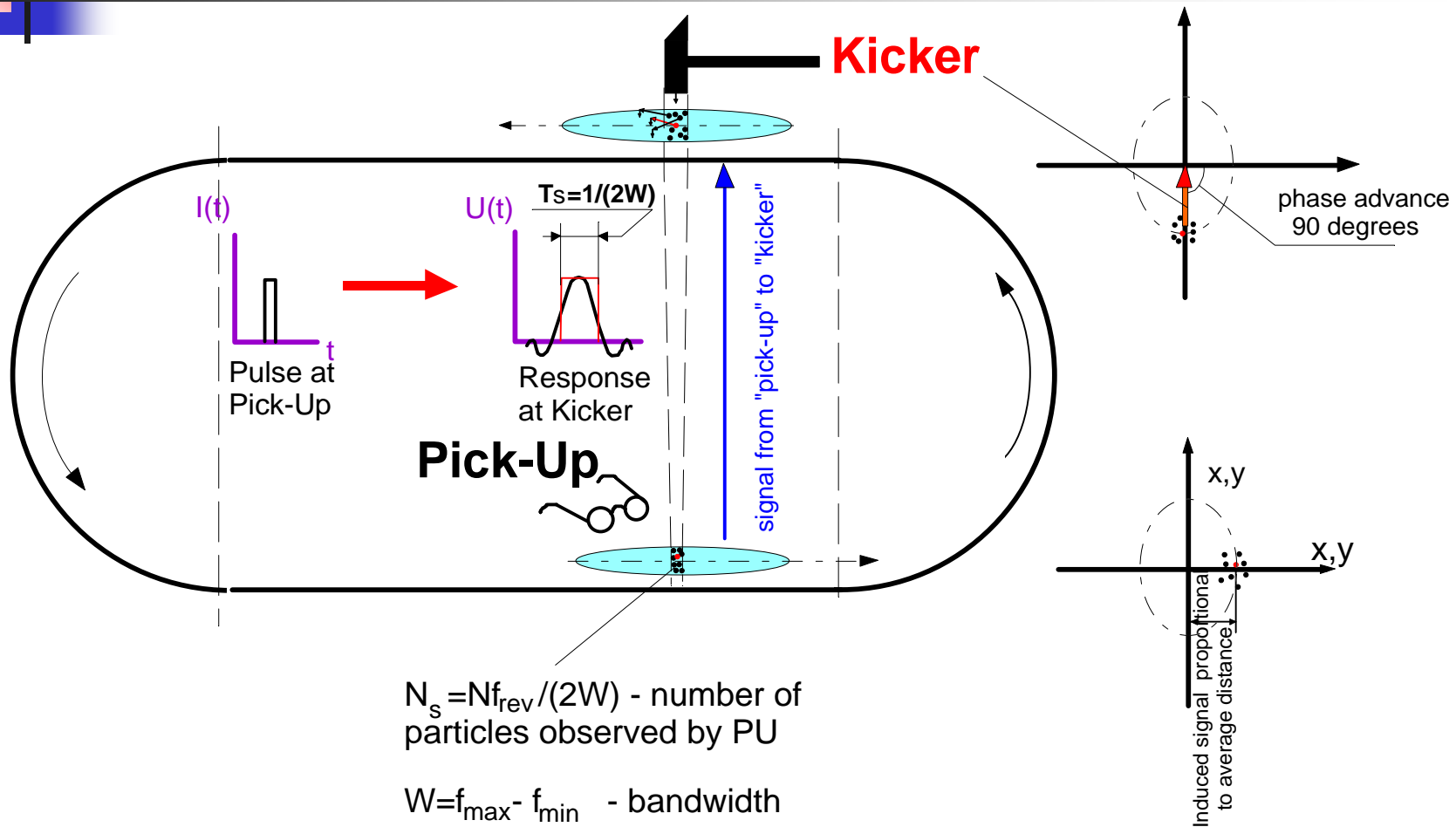
	Resonant lattice with ρ and gradient modulation		Regular FODO lattice with suppressors	
	Advantages	disadvantages	advantages	disadvantages
Sensitivity to high multipoles	Low			High
Sextupoles on str. section	Yes			No
Quadr. families number		3	2	
Max dispersion		$\sim 6 \div 10$ m, depends on var.	~ 3.5 m	
Max $\beta_{x,y}$ function		$48 \div 70 / 40 \div 70$ depends on var.	40/40	
$3\sqrt{\beta_x \epsilon_{rms} + (D_x \Delta p/p)^2}$ at $\epsilon_{rms} = 0.68$; $\Delta p/p_{rms} = 1 \times 10^{-3}$	$\sim 40 \div 50$ mm, depends on var.		~ 45 mm	



Thus, the “Resonant” structure has the features:

1. Ability to achieve the negative momentum compaction factor with minimum circumference and control of gamma transition in a wide region;
2. Dispersion-free straight section without special suppressor;
3. Low sensitivity to multipole errors and sufficiently large dynamic aperture.
4. Minimum families of focusing and defocusing quadrupoles and separated adjustment of gamma transition, horizontal and vertical tunes;
5. Convenient sextupole chromaticity correction scheme;
6. Independent optics parameters of arcs and straight sections

Stochastic cooling principle and requirements to the optics



$N_s = Nf_{rev}/(2W)$ - number of particles observed by PU

$W = f_{max} - f_{min}$ - bandwidth

28 September-3 October, RuPAC



Real and Imaginary arcs for Stochastic Cooling:

- The momentum compaction factor in imaginary and real arcs takes the meaning:

$$\alpha_{kp} = -\frac{1}{4v_{arc}^2} \qquad \alpha_{pk} = \frac{1}{4v_{arc}^2}$$

- and slip factors:

$$\eta_{pk} = \frac{1}{\gamma^2} - \frac{1}{4v_{arc}^2}$$
$$\eta_{kp} = \frac{1}{\gamma^2} + \frac{1}{4v_{arc}^2}$$

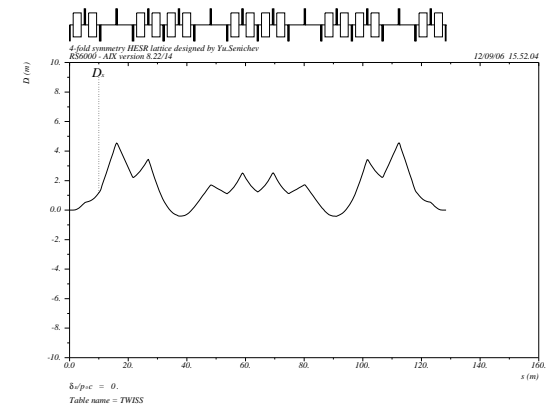
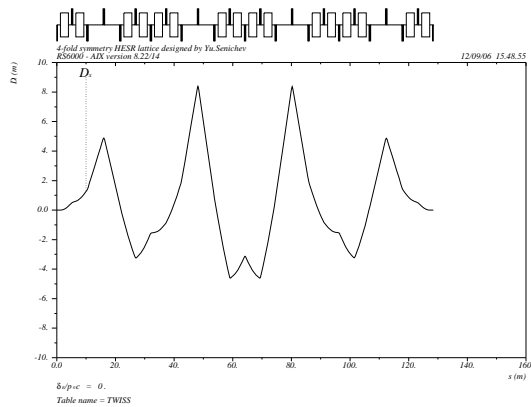
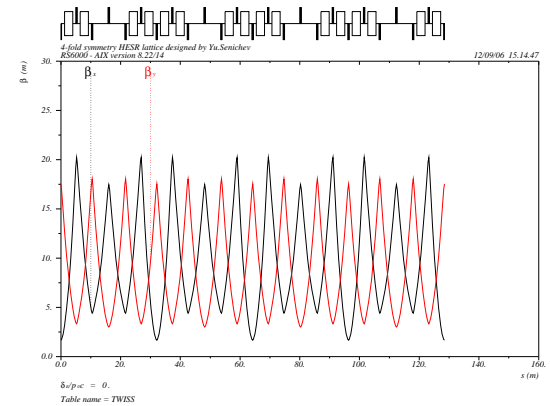
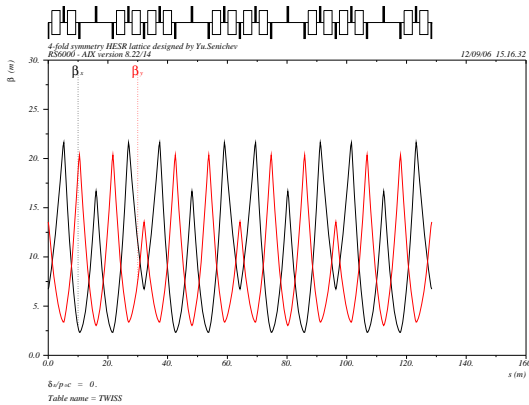
In case $\gamma \approx 2v_{arc}$:

the real arc is isochronous $\eta_{pk} \approx 0$

the imaginary arc has a slip factor $\eta_{kp} \approx 1/2v_{arc}^2$

Twiss parameters of the real and imaginary arcs of SC option for HESR (FAIR)

- The β -function and dispersion on the imaginary, the real 4-fold symmetry arcs



28 September-3 October, RuPAC
2008



What can we do for Synchrotron Light Source Optics?

- Almost all **Synchrotron Light Sources** work higher of the transition energy, therefore chromaticity must be $\xi > 0$
- Since the horizontal emittance depends upon the horizontal dispersion function,

as $\varepsilon_x \propto \langle H \rangle_{dipole}$, where $H = \gamma_x \eta_x^2 + 2\alpha_x \eta_x \eta'_x + \beta_x \eta_x'^2$ to get $\varepsilon_{x, min}$

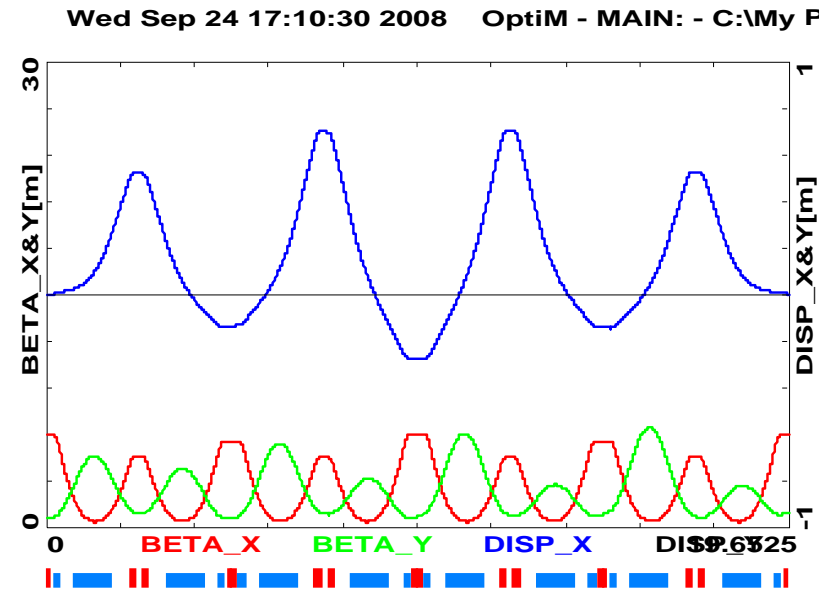
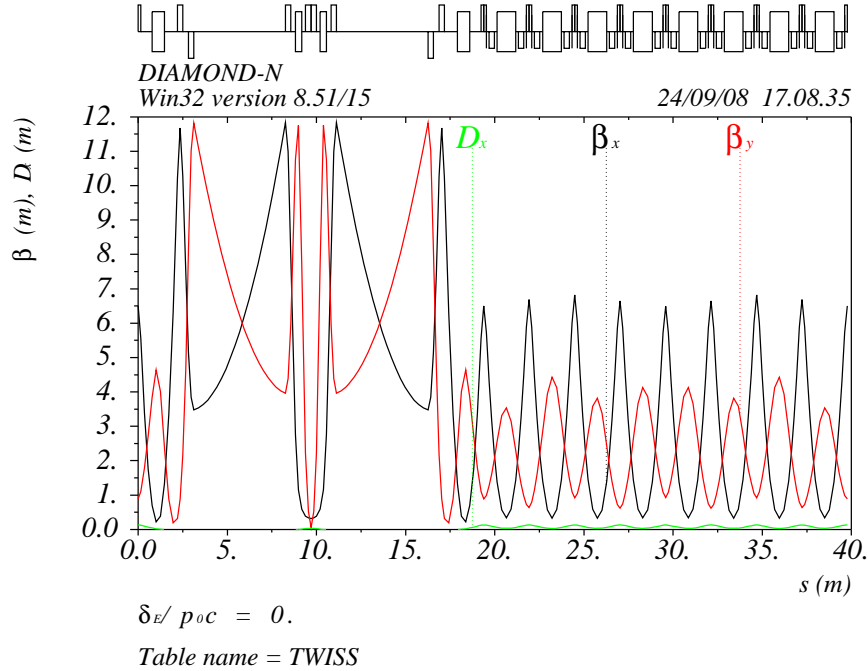
the dispersion \rightarrow minimum value

- Stronger sextupoles are required \rightarrow the dramatic decreasing of DA
- There are two methods:
 - Sextupoles have to be compensated
 - Lattice w/o sextupole with imaginary γ_{tr}

SLS Lattices:

with sextupoles N-bend achromat with $\alpha > 0$

w/o sextupoles with $\alpha < 0$





Sextupole compensation in SLS optic

- under strong influence of (k_x+k_y) -th Integer resonance

$$H(I_x, I_y, \varphi_x, \varphi_y) = \frac{(k_x^2 + k_y^2)^{1/2}}{k_x} \Delta_x I_x + \frac{(k_x^2 + k_y^2)^{1/2}}{k_y} \Delta_y I_y +$$

$$2 \langle h_{k_x, k_y, p} \rangle I_x^{k_x/2} I_y^{k_y/2} \cos(k_x \varphi_x + k_y \varphi_y) +$$

$$\zeta_x I_x^2 + \zeta_y I_y^2 + \zeta_{xy} I_x I_y$$

- For 3-d integer resonance the influence of the non-linearity is specified by the discriminant in the expression:

$$I_x^{1/2} = -\frac{3h_{30p} \cos 3\varphi_x}{8\zeta_x} \pm \frac{1}{4\zeta_x} \sqrt{\frac{9}{4} h_{30p}^2 - 8\zeta_x (\Delta + \zeta_{xy} I_y)}$$

Nekhoroshev's criterium:

the non-linearity in both planes have to have the same sign and $4\zeta_x \zeta_y \geq \zeta_{xy}^2$

- The lattices with $\zeta_x \gg h_{30p}$ have to be classified as a special lattice, since it is a case, when the value of h_{30p} is effectively suppressed, but the non-linearity remain to be under control and strong.
- If the sign of the detuning Δ coincides with the sign of the tune shift ζ_x , the discriminant is negative and the system has only one centre at $I_x = 0$
- The quasi-isochronism condition by Nekhoroshev is fulfilled, when

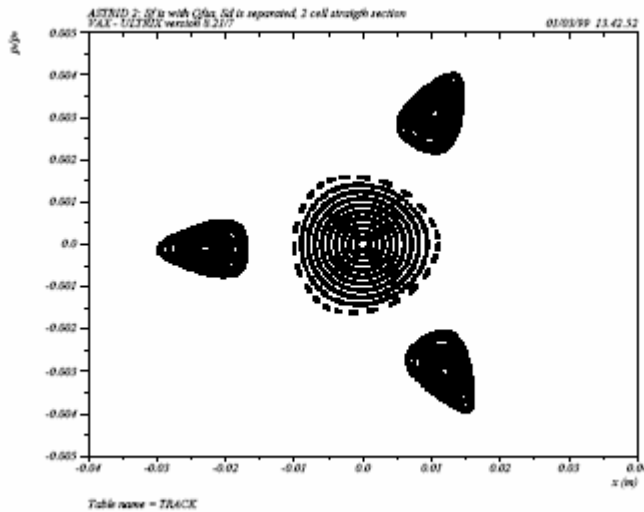
$$k_x (2\zeta_x I_x^r + \zeta_{xy} I_y^r) + k_y (2\zeta_y I_y^r + \zeta_{xy} I_x^r) = 0$$
$$\zeta_x k_x^2 + \zeta_{xy} k_x k_y + \zeta_y k_y^2 = 0$$

Convex or concave
resonant surface with
maximum stable region

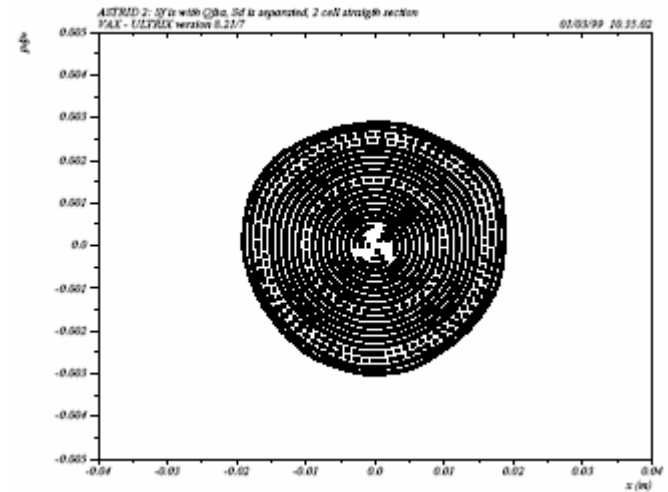
Dynamic aperture tracking

- negative and positive detune

$$\zeta > 0; \Delta < 0$$



$$\zeta > 0; \Delta > 0$$





Conclusion

“Resonant” lattice was developed with features:

- ability to achieve the negative momentum compaction factor using the resonantly correlated curvature and gradient modulations;
- gamma transition variation in a wide region from $\gamma_{tr}=v_x$ to $\gamma_{tr}=iv_x$ with quadrupole strength variation only;
- integer odd 2π phase advance per arc with even number of superperiod and dispersion-free straight section;
- independent optics parameters of arcs and straight sections;
- two families of focusing and one of defocusing quadrupoles;
- separated adjustment of gamma transition, horizontal and vertical tunes;
- convenient chromaticity correction method using sextupoles;
- first-order self-compensating scheme of multipoles and as consequence low sensitivity to multipole errors and a large dynamic aperture



Conclusion

“Resonant” lattice can be used:

- In the heavy ion and proton synchrotron lattice without the transition energy crossing
- In the lattice with high efficiency of stochastic cooling
- In the Synchrotron Light Source lattices w/o sextupoles or with selfcompensated sextupoles