

A LOW EMITTANCE LATTICE FOR THE CLIC DAMPING RING

J.P.Potier, CERN, CH-1211 Geneva 23, L.Rivkin, PSI, CH-5232 Villigen

Abstract

Damping rings with very small normalized equilibrium emittance and short damping times are required to deliver trains of bunches with a high repetition rate for the high-luminosity linear colliders. Using analytic expressions for the equilibrium emittance as a function of deflection angle per dipole, as well as the expression for the Twiss parameters providing the minimum emittance, a strategy to stay close to this minimum is described. In order to get as close as possible to the optimum Twiss parameters values, a quadruplet lattice with high horizontal phase advance is introduced. Finally, this approach is illustrated for the particular case of the CLIC damping ring and the resulting performance is described.

1 INTRODUCTION

The electron-positron linear colliders at high energy, requiring high luminosity, are all based on a high collision rate using beams of very small dimensions at the interaction point. These small beam dimensions require strong focusing in the final focus, as well as very small transverse emittance beams. Such small emittance will possibly be reached with high brightness electron guns presently under development, but is impossible to reach directly with the positron sources that have emittance three or more orders of magnitude higher. Therefore, for the positron beam, a damping ring facility will be necessary.

Most of the damping rings proposed nowadays are based on the Theoretical Minimum Emittance lattice (TME) in which the Twiss functions β_x and D_x are minimum in the middle of the bending magnet. The simplest example is a combined function bending magnet with a defocusing gradient and surrounding focusing quadrupoles to produce the appropriate Twiss functions. Such a lattice was proposed [1] for the CLIC damping ring. This ring was designed for the working energy of 3 GeV in order to get enough damping, but due to the strong chromaticity correction sextupoles, it suffered from a severe detuning versus emittance and from a great sensivity of the transverse dynamical acceptance to misalignment errors.

In this paper, using analytic expressions of the equilibrium emittance as a function of the deflecting angle per dipole, as well as the expression for the Twiss parameters corresponding to the minimum emittance, an expression for the emittance of the de-tuned lattice is proposed and a strategy to stay as close as possible to the minimum is developed, keeping the dispersion as high as possible, in order to limit the strength of the chromaticity

correction sextupoles. A main damping ring based on this approach is then derived providing beam characteristics fulfilling, without any wigglers, the 500 GeV/c CLIC injector complex requirements [2]. The corresponding parameter list for this damping ring is summarised in Table 2.

2 MINIMUM EMITTANCE LATTICE

The transverse equilibrium beam emittance of a ring working at an energy E , composed of dipole magnets of length L and deflection angle θ , can be expressed as a function of the optics parameters in the middle of the bending magnet α , β , D , D' . After integration of the synchrotron integrals, using the approximation of small bending angle, the emittance is [3].

$$\varepsilon_{x0} = \frac{C_q E^2}{J_x} \frac{I_5}{I_2} = \frac{C_q E^2}{J_x} \left[\frac{\gamma D^2 + 2\alpha \cdot D \cdot D' + \beta D'^2}{L} \cdot \theta - \left(\frac{\alpha \cdot D' + \gamma \cdot D}{12} \right) \cdot \theta^2 + \left(\frac{\beta}{12 \cdot L} + \frac{\gamma \cdot L}{320} \right) \cdot \theta^3 \right]$$

where $C_q = 1.468 \cdot 10^{-6} \left[\frac{\text{m}}{\text{GeV}^2} \right]$. As is well known, this

expression is minimum for $\alpha_{opt} = D'_{opt} = 0$ i.e. the optical and dispersion functions are symmetric with respect to the middle of the bending magnet and

$$\beta_{opt} = \frac{L}{2 \cdot \sqrt{15}}, \quad D_{opt} = \frac{L \cdot \theta}{24}, \quad \varepsilon_{x0} = \frac{C_q \cdot E^2}{J_x} \cdot \frac{\theta^3}{12 \sqrt{15}}$$

For the de-tuned lattice, still preserving the symmetry, the emittance blow-up $\varepsilon/\varepsilon_{opt}$ can be expressed using the normalised values $\beta_r = \beta/\beta_{opt}$ and $D_r = D/D_{opt}$

$$\varepsilon_r = \frac{5}{8} \cdot \left[\frac{D_r^2}{\beta_r} - \frac{2 \cdot D_r}{\beta_r} \right] + \frac{9}{2} \cdot \left[\frac{1}{4 \cdot \beta_r} + \frac{\beta_r}{9} \right].$$

The family of curves for different values of constant blow-up ranging from 2 to 128 in the β_r, D_r diagram is shown using logarithmic scales in Figure 1.

For a given emittance blow-up, the maximum of $D_r = f(\beta_r)$ curve is chosen, where

$$\beta_{rmx} = \varepsilon_r \quad \text{and} \quad D_{rmx} = 1 + \frac{2}{\sqrt{5}} \cdot \sqrt{\varepsilon_r^2 - 1}.$$

The curve representing the position of these maxima is also shown in Figure 1.

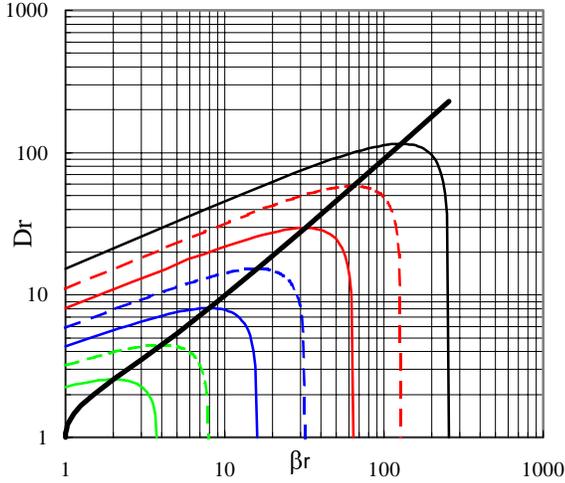


Figure 1 Dispersion versus beta function for a given emittance detuning and dispersion versus emittance for a maximum dispersion and a given emittance detuning

3 CHOICE OF THE LATTICE PARAMETERS

3.1 Bending field and design energy

In the CLIC injector complex [2], one train of 1 to 10 bunches is injected and extracted at a repetition rate, f_r from 1210 to 2400, but a number of trains k , are concurrently circulating in the damping ring in order to leave a larger time for damping $T = k/f_r$. The present design is based on trains of 10 bunches, spaced by 20 cm, at a repetition frequency f_r of 1800 Hz.

The damping ring circumference C is chosen to accommodate the k trains, with enough separation between them to allow for the rise and fall of the injection and extraction system l_k . In the case of a fast kicker, l_k is 7.5 m (25 ns). Using a particular combination of fast kickers and RF kickers, the time separation between the bunch trains, l_s can be reduced down to $l_k/2$ (12.5 ns) [4]. If n is the number of damping time necessary to damp the incoming emittance the reduced damping time

$$\tau_r = \frac{\tau_{x,y}}{C} \quad \text{has to satisfy the condition } \tau_r \leq \frac{1}{n \cdot l_s \cdot f_r}$$

As shown in [5], the round beam produced by the positron injector is first pre-damped in a collector ring with large transverse and longitudinal acceptances during $5 \tau_{x,y}$ and then damped in the main damping ring (MDR) during $4 \tau_{x,y}$. Under these conditions, with $\tau_r \leq 37 \mu\text{s/m}$, the beam emittance at extraction will not be larger than the equilibrium emittance by more than 10%. This value, which depends on the bending field and on the design energy, can be written as

$$\tau_r = \frac{2.54 \cdot 10^{14}}{J_x \cdot B \cdot E^2}$$

with $J_x = 1$ as the bending magnet will have no gradient. In order to maximise the damping, keeping the normalised emittance low, the highest possible field in the bending magnet is chosen while staying far from saturation, B around 1.5 T, and then E from the above equations is $E = 2.15 \text{ GeV}/c$.

3.2 Twiss functions in the middle of the bending magnets needed to produce the design emittances

Taking into account the emittance blow-up between the ring exit and the interaction point, the normalised transverse emittances at the output of the main damping ring have to be $\gamma \epsilon_x = 2.5 \cdot 10^{-6} \text{ radm}$, $\gamma \epsilon_y = 0.04 \cdot 10^{-6} \text{ radm}$ with a bunch length $\sigma_z = 18 \text{ mm}$. We have chosen to use a low emittance detuning value $\epsilon_r = 3.7$ to use the TME lattice efficiently with $D_r = 4.2$ close to the maximum on the detuning curve and $\beta_r = 4.4$ (see figure 1). The number n_b of cells can be worked out from the optimum equilibrium emittance and the emittance detuning, resulting in $n_b = 60$ and a dipole magnet length $L = .5 \text{ m}$.

4 QUADRUPLLET TME LATTICE

In order to provide the low dispersion and beta values in the middle of the dipole magnet, it will be flanked on each side by a defocusing quadrupole followed by a focusing quadrupole. The corresponding lattice is shown in Figure 2.

Parameter	Sym- bol	Units	TME lattice
Momentum	E	GeV/ c	2.15
Deflection per cell	θ	dg	6.0
Momentum compaction	α_p	10^{-3}	0.29
Normalised equilibrium emittance	$\gamma \epsilon_n$	10^{-6} radm	2.56
Normalised damping time	τ_r	10^{-6} s	37
Horizontal phase advance per cell	μ_x	2π	0.445
Vertical phase advance per cell	μ_y	2π	0.217
Emittance detuning ϵ/ϵ_{opt}	ϵ_r	-	3.7
Dispersion in the middle of the bending	D	mm	9.4
β in the middle of the bending	β	m	0.292
β detuning	β_r	-	4.42
Dispersion detuning	D_r	-	4.19

Table 1: Main characteristics of the CLIC TME lattice

The main characteristics of a ring built of 60 cells are shown in Table 1. The values found are in good agreement with the analytical calculation made above.

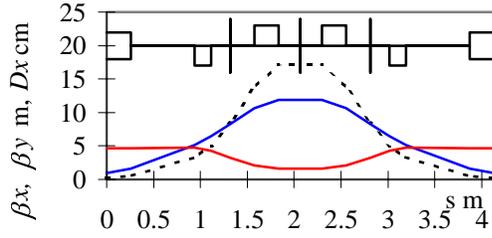


Figure 2: Twiss functions for the TME lattice providing an emittance detuning of 3.7

5 MAIN DAMPING RING DESIGN

Each damping ring arc consists of five TME quadruplet cells and two dispersion suppressors, that utilise half of a regular bending magnet. The arcs are separated by short straight sections equipped with quadrupole triplets to get $\alpha_{xy} = 0$ and a small β_x in the middle. These short straight sections can house a damping wiggler. An arc is represented in Figure 3.

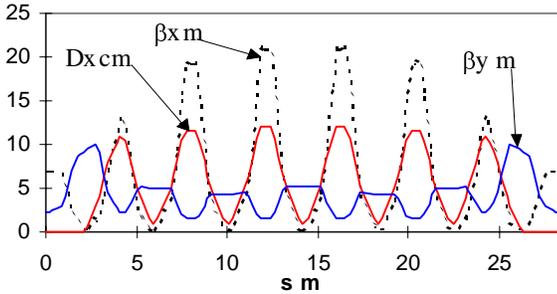


Figure 3: Arc of the CLIC main damping ring including short straight sections

The ring is made up of two halves, 5 arcs each, and two long straight sections with π phase advance in each plane. These straight sections are inserted symmetrically, one for the RF cavities the other for the injection and extraction systems. The chromaticity is corrected by two families of sextupoles in the regular cells, and the 4 other families in the dispersion suppressor and in the straight sections.

The dynamic acceptance has been studied in the ring without the long straight sections. The closed orbit is corrected to $50\mu\text{m}$, using position monitors (assumed resolution $25\mu\text{m}$) located at each sextupole, with the correcting dipoles located at the same positions. The dynamic acceptance is more than $6.5 \cdot 10^{-6}$ radm without errors. In this case, de-tuning versus the emittance in the aperture is less than 0.005 in the horizontal plane and 0.003 in the vertical plane at 10 % coupling. In presence of errors, at full coupling, with dP/P within $\pm 0.5\%$ and position errors up to $50\mu\text{m}$, the dynamic acceptance is $4.0 \cdot 10^{-6}$ radm.

As the bunch distance is a multiple of 0.2 m the RF frequency of the accelerating cavity will be 1.5 GHz with

a voltage of 1 MV providing enough Touschek life-time. The parameters of the main damping ring are in Table 2.

Parameter	Sym- bol	Units	MDR ring
Momentum	E	GeV/c	2.15
Number of cells	-	-	60
Ring length (without straight sections)	L	m	283
Normalised equilibrium emittance	$\gamma\epsilon_n$	10^{-6} radm	2.5
Emittance detuning $\epsilon/\epsilon_{\text{opt}}$	ϵ_r	-	3.8
Damping partition numbers	$J_{x,y,z}$		1,1, 2
β detuning	βr		4.4
Dispersion detuning	Dr		4.2
Normalised damping time	τ_r	10^{-6} s	37
Bending magnet field	B	T	1.47
Horizontal / vertical tunes	$\mu_{x,y}$	2π	31.2/1 3.3
Horizontal/vertical chromaticities	μ_y		-107 / -21
Momentum compaction	α_p	10^{-3}	0.24
Dynamical acceptance in +/- 1%	A_{dyn}	10^{-6} radm	4.0
Rms displacement errors	σ_{misal}	μm	50
RF frequency	f_{rf}	GHz	1.5
RF voltage	V_{RF}	MV	1.0
Energy loss per turn	U_0	MV	0.39
Bunch length	σ_c	mm	1.8

Table 2: Characteristics, of the main damping ring adapted to the CLIC requirements using the TME lattice

CONCLUSIONS

Using an analytic approach, a damping ring working close to the theoretical minimum emittance has been designed fulfilling CLIC's requirements. As the CLIC bunch train length and repetition rate are evolving, this approach will be used to adapt the parameters and possibly introduce wigglers, to adapt to the new requests.

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