

# ANALYTIC SECOND- AND THIRD-ORDER ACHROMAT DESIGNS

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## I. INTRODUCTION

An achromat is a transport system that carries a beam without distorting its transverse phase space distribution. In this study, we apply the Lie algebraic technique [1-6] to a repetitive FODO array to make it either a second-order or a third-order achromat. (Achromats based on reflection symmetries [7,8] are not studied here.) We will consider third-order achromats whose unit FODO cell layout is shown in Fig.1. The second-order achromat layout is the same except the octupoles are absent.

For the second-order achromats, correction terms (due to the finite bending of the dipoles) to the well-known formulae for the sextupole strengths are derived. For the third-order achromats, analytic expressions for the five octupole strengths are given. The quadrupole, sextupole and octupole magnets are assumed to be thin-lens elements. The dipoles are assumed to be sector magnets filling the drift spaces. More details of the analysis have been reported elsewhere.[9] We thank Y. Yan, H. Ye, J. Irwin and A. Dragt for their help.

## II. ANALYSIS

We first calculate the Lie maps of each of the magnet elements. The map for a magnet element of length  $L$  is given by  $e^{-L:H}$ , where  $H$  is the Hamiltonian of the element. For a particle with  $\delta = \Delta P/P_0$ , we use (we ignore the path-length dynamics)

$$\text{thin quadrupole : } HL = \frac{1}{2F_k}(x^2 - y^2)(1 - \delta + \delta^2)$$

$$\text{thin sextupole : } HL = \frac{S_k}{3}(x^3 - 3xy^2)(1 - \delta)$$

$$\text{thin octupole : } HL = \frac{O_k}{4}(x^4 - 6x^2y^2 + y^4)$$

$$\text{sector dipole : } H = \frac{P_x^2 + P_y^2}{2} + \frac{x^2}{2R^2} - \frac{x\delta}{R} + \frac{x(P_x^2 + P_y^2)}{2R} - \frac{x^2\delta}{2R^2} + \frac{x\delta^2}{R} + \frac{(P_x^2 + P_y^2)^2}{8} - \frac{x\delta^3}{R} + \frac{x^2\delta^2}{2R^2} \quad (1)$$

where  $R$  is the bending radius;  $F_k$  is the focal length of the  $k$ -th quadrupole;  $S_k$  and  $O_k$  are the  $k$ -th integrated sextupole and octupole strengths. Fringe fields are ignored.

Given the Hamiltonian  $H$  of an element, we factorize the element map as

$$e^{-L:H} = e^{H_2+H_3+H_4+\dots} = e^{f_2}e^{f_3}e^{f_4}e^{\mathcal{O}(X^5)} \quad (2)$$

where  $H_n$  and  $f_n$  are polynomials of order  $n$  in the variables  $X = (x, P_x, y, P_y, \delta)$ . We performed this factorization [3,5] and obtained

thin quadrupole :

$$f_3 = \frac{1}{2F_k}(x^2 - y^2)\delta, \quad f_4 = -\frac{1}{2F_k}(x^2 - y^2)\delta^2$$

thin sextupole :

$$f_3 = -\frac{S_k}{3}(x^3 - 3xy^2), \quad f_4 = \frac{S_k}{3}(x^3 - 3xy^2)\delta$$

thin octupole :  $f_3 = 0, \quad f_4 = -\frac{O_k}{4}(x^4 - 6x^2y^2 + y^4)$

sector dipole :

$$\begin{aligned} f_3 = & -\frac{1}{6R^2} \sin^3 \frac{L}{R} x^3 - \frac{1}{4R} \sin \frac{L}{R} \sin \frac{2L}{R} x^2 P_x \\ & - \frac{1}{4} \cos \frac{L}{R} \sin \frac{2L}{R} x P_x^2 + \frac{R}{6} (1 - \cos^3 \frac{L}{R}) P_x^3 \\ & - \frac{1}{2} \sin \frac{L}{R} x P_y^2 + \frac{x^2 \delta}{2R} \sin \frac{L}{R} (\cos \frac{L}{R} + \sin^2 \frac{L}{R}) \\ & + R \sin^2 \frac{L}{2R} P_x P_y^2 - 2 \sin^2 \frac{L}{2R} \sin^2 \frac{L}{R} x P_x \delta \\ & - \frac{R}{2} \sin^2 \frac{L}{2R} \sin \frac{2L}{R} P_x^2 \delta - \frac{1}{2} (L - R \sin \frac{L}{R}) P_y^2 \delta \\ & - \frac{x \delta^2}{2} (\sin^3 \frac{L}{R} + \sin \frac{2L}{R}) + \frac{R}{2} (2 - \cos \frac{L}{R}) \sin^2 \frac{L}{R} P_x \delta^2 \\ & + \frac{1}{12} (-6L + 2R \sin^3 \frac{L}{R} + 3R \sin \frac{2L}{R}) \delta^3 \\ f_4 = & \left[ -\frac{x^2}{8R} \sin^3 \frac{L}{R} - \frac{x P_x}{8} \sin \frac{L}{R} \sin \frac{2L}{R} \right. \\ & \left. - \frac{R}{8} \cos^2 \frac{L}{R} \sin \frac{L}{R} P_x^2 - \frac{R}{8} \sin \frac{L}{R} P_y^2 \right] (P_x^2 + P_y^2) \\ & + \frac{x^3 \delta}{12R^2} \sin^3 \frac{L}{R} + \left( \frac{1}{2} + \cos \frac{L}{R} \right) \sin^2 \frac{L}{2R} \sin \frac{L}{R} x P_x^2 \delta \\ & + \left[ \frac{R}{12} (3 + 4 \cos \frac{L}{R} + 5 \cos \frac{2L}{R}) P_x^3 \delta \right. \\ & \left. + \frac{x P_y^2 \delta}{4} \sin \frac{2L}{R} + \frac{R}{4} (3 + \cos \frac{2L}{R}) P_x P_y^2 \delta \right] \sin^2 \frac{L}{2R} \\ & - \frac{1}{4R} (\sin^3 \frac{L}{R} + \sin \frac{2L}{R}) x^2 \delta^2 + \frac{1}{2} \sin^2 \frac{L}{R} x P_x \delta^2 \\ & - \frac{R}{4} (1 + 3 \cos \frac{L}{R}) \sin^2 \frac{L}{2R} \sin \frac{L}{R} P_x^2 \delta^2 \\ & + \left[ \frac{R}{2} \sin^4 \frac{L}{2R} P_y^2 + (\cos \frac{L}{R} + \frac{1}{4} \sin^2 \frac{L}{R}) x \delta \right] \sin \frac{L}{R} \delta^2 \\ & - \frac{R}{2} \sin^2 \frac{L}{R} P_x \delta^3 + \frac{\delta^4}{12} (6L - R \sin^3 \frac{L}{R} - 3R \sin \frac{2L}{R}) \end{aligned} \quad (3)$$

Having factorized the maps of all magnets, the total map  $\mathcal{M}_{\text{cell}}$  of a cell is obtained by multiplying and concatenating the maps of the component elements:[3,9]

$$\mathcal{M}_{\text{cell}} = \prod_{i=1}^N (e^{i f_2^i} e^{i f_3^i} e^{i f_4^i}) = e^{i h_2} e^{i h_3} e^{i h_4} e^{i \mathcal{O}(X^5)} \quad (4)$$

where

$$\begin{aligned} \mathcal{R} &= e^{i h_2} = \prod_{i=1}^N e^{i f_2^i}, & h_3 &= \sum_{i=1}^N \tilde{f}_3^i \\ h_4 &= \sum_{i=1}^N \tilde{f}_4^i + \frac{1}{2} \sum_{j>i=1}^N [\tilde{f}_3^i, \tilde{f}_3^j] \end{aligned} \quad (5)$$

In Eq.(5),  $\tilde{f}^i$  means  $\tilde{f}^i(X) = f^i(R_{N \rightarrow i} X)$  with  $R_{N \rightarrow i}$  the linear map from the last element to the  $i$ -th element. The map of the  $N$ -cell achromat is  $\mathcal{M} = \mathcal{M}_{\text{cell}}^N$ . The number of cells  $N$  is so that  $\mu_{x,y}$  (the total phase advances in  $x$  are  $y$ ) are both multiples of  $2\pi$ , but avoiding resonances.

We now make a canonical coordinate transformation from  $(x, P_x, y, P_y)$  to  $(\phi_x, A_x, \phi_y, A_y)$  by  $x = \sqrt{2A_x \beta_x} \sin \phi_x + \eta \delta$ ,  $P_x = \sqrt{\frac{2A_x}{\beta_x}} (\cos \phi_x - \alpha_x \sin \phi_x) + \eta' \delta$ , and similarly for  $y$  and  $P_y$  without the  $\eta$  and  $\eta'$  terms, where  $\beta_{x,y}$ ,  $\alpha_{x,y}$  and  $\eta, \eta'$  are the Courant-Snyder and the dispersion functions.[10] The linear map generator  $h_2$  becomes  $h_2 = -\mu_x A_x - \mu_y A_y - \frac{1}{2} \bar{\alpha}_c \delta^2$  where and  $\bar{\alpha}_c$  is the momentum compaction factor. We then decompose  $h_n$  in terms of the eigenmodes of  $h_2$ : as[5]

$$\begin{aligned} h_n &= \sum_{a+b+c+d+e=n} C_{abcd,e}^n |abcd, e\rangle \\ |abcd, e\rangle &\equiv A_x^{(a+b)/2} A_y^{(c+d)/2} e^{i(a-b)\phi_x} e^{i(c-d)\phi_y} \delta^e \end{aligned} \quad (6)$$

To reduce a nonlinear map to its normal form, it can be shown[11] that (in the absence of resonances)[2] all the non-secular terms can be transformed away via a symplectic similarity transformation leaving only terms with  $a = b$  and  $c = d$ , i.e., terms depending on  $A_x, A_y$  and  $\delta$  only. In particular, we have

$$\begin{aligned} h_3 &= C_{1100,1}^3 A_x \delta + C_{0011,1}^3 A_y \delta + C_{0000,3}^3 \delta^3 \\ h_4 &= C_{2200,0}^4 A_x^2 + C_{0022,0}^4 A_y^2 + C_{1111,0}^4 A_x A_y \\ &\quad + C_{1100,2}^4 A_x \delta^2 + C_{0011,2}^4 A_y \delta^2 + C_{0000,4}^4 \delta^4 \end{aligned} \quad (7)$$

### III. SECOND-ORDER ACHROMATS

For a second-order achromat, we follow Eqs.(6-7) and find the normal form of the unit cell is given by  $h_3$  of Eq.(7) where

$$\begin{aligned} C_{1100,1}^3 &= \sum_{k=1,2}^{\text{quads}} \left[ \frac{1}{2F_k} - \lambda_k \eta(k) \right] \beta_x(k) + w_x \\ C_{0011,1}^3 &= - \sum_{k=1,2}^{\text{quads}} \left[ \frac{1}{2F_k} - \lambda_k \eta(k) \right] \beta_y(k) + w_y \end{aligned} \quad (8)$$

and

$$\begin{aligned} w_x &= \sum_{k=1,2}^{\text{dipoles}} \frac{1}{2} \sin^2 \left( \frac{L}{R} \right) \left\{ \frac{\beta_x(k)}{R} \left[ \sin \frac{L}{R} + \cot \frac{L}{R} \right. \right. \\ &\quad \left. \left. - \frac{\eta(k)}{R} \sin \frac{L}{R} - \eta'(k) \cos \frac{L}{R} \right] + 2\alpha_x(k) \left[ 1 - \cos \frac{L}{R} \right. \right. \\ &\quad \left. \left. + \frac{\eta(k)}{R} \cos \frac{L}{R} + \eta'(s) \cos \frac{L}{R} \cot \frac{L}{R} \right] \right\} \end{aligned}$$

$$\begin{aligned} &+ \gamma_x(k) R \left[ -\cos \frac{L}{R} \tan \frac{L}{2R} - \frac{\eta(k)}{R} \cos \frac{L}{R} \cot \frac{L}{R} \right. \\ &\quad \left. + \left( \cos \frac{L}{R} + \frac{1}{2} \sec^2 \frac{L}{2R} \right) \eta'(k) \right] \} \end{aligned}$$

$$\begin{aligned} w_y &= \sum_{k=1,2}^{\text{dipoles}} \frac{1}{2} \gamma_y(k) R \left[ \sin \frac{L}{R} - \frac{L}{R} - \eta(k) \sin \frac{L}{R} \right. \\ &\quad \left. + \eta'(k) \left( 1 - \cos \frac{L}{R} \right) \right] \end{aligned} \quad (9)$$

The lattice functions are evaluated at the two quadrupoles in Eq.(8) and at the ends of the two dipoles in Eq.(9). In the limit of weak bending with  $\epsilon_1 = \frac{L}{R} \ll 1$ , we have

$$\begin{aligned} w_x &\simeq \epsilon_1 \sum_s^D \alpha_x(s) \eta'(s) + \frac{1}{4} \gamma_x(s) (3L \eta'(s) - 2\eta(s)) \\ w_y &\simeq \epsilon_1 \sum_s^D \frac{1}{4} \gamma_y(s) (L \eta'(s) - 2\eta(s)) \end{aligned} \quad (10)$$

To form a second-order achromat, we set the two  $C$ -coefficients to zero, and obtain

$$\begin{aligned} S_1 &= \frac{1}{2\eta(1)F_1} + \frac{\beta_y(2)w_x + \beta_x(2)w_y}{\eta(1)[\beta_x(1)\beta_y(2) - \beta_x(2)\beta_y(1)]} \\ S_2 &= \frac{1}{2\eta(2)F_2} - \frac{\beta_y(1)w_x + \beta_x(1)w_y}{\eta(2)[\beta_x(1)\beta_y(2) - \beta_x(2)\beta_y(1)]} \end{aligned} \quad (11)$$

The first terms usually dominate and give the well-known results. The correction terms with  $w_x$  and  $w_y$  are normally but not always small.

### IV. THIRD-ORDER ACHROMATS

We also studied the case of a third-order achromat. An algebraic program using Mathematica was developed to do the analysis. Here we only report our results. The normal form of the third-order generator for a unit cell is given by Eq.(9) with

$$\begin{aligned} C_{2200,0}^4 &= -\frac{3}{8} \sum_{k=1}^5 \beta_x(k)^2 O_k + w_{xx} \\ C_{1111,0}^4 &= \frac{3}{2} \sum_{k=1}^5 \beta_x(k) \beta_y(k) O_k + w_{xy} \\ C_{0022,0}^4 &= -\frac{3}{8} \sum_{k=1}^5 \beta_y(k)^2 O_k + w_{yy} \\ C_{1100,2}^4 &= -\frac{3}{2} \sum_{k=1}^5 \beta_x(k) \eta(k) O_k + w_{xd} \\ C_{0011,2}^4 &= \frac{3}{2} \sum_{k=1}^5 \beta_y(k) \eta(k) O_k + w_{yd} \end{aligned} \quad (12)$$

and (when  $\epsilon_1 = \frac{L}{R} \ll 1$ )

$$\begin{aligned} w_{xx} &\simeq \csc \frac{3\mu_x}{2} (2 + 3 \cos \mu_x) \prod_s^S \frac{S_s}{4} \beta_x(s)^{\frac{3}{2}} - \frac{3L}{16} \sum_s^D \gamma_x(s)^2 \\ &\quad + \frac{1}{8} \csc \frac{3\mu_x}{2} (3 \cos \frac{\mu_x}{2} + 2 \cos \frac{3\mu_x}{2}) \sum_s^S S_s^2 \beta_x(s)^3 \end{aligned}$$

$$\begin{aligned}
w_{xy} \simeq & -\frac{L}{4} \sum_s^D \gamma_x(s) \gamma_y(s) - \frac{1}{2} \cot \frac{\mu_x}{2} \sum_s^S S_s^2 \beta_x(s)^2 \beta_y(s) \\
& - \csc\left(\frac{\mu_x}{2} + \mu_y\right) \csc\left(\frac{\mu_x}{2} - \mu_y\right) \sin 2\mu_y \sum_s^S \frac{S_s^2}{4} \beta_x(s) \beta_y(s)^2 \\
& + \left[ \csc\left(\frac{\mu_x}{2} + \mu_y\right) - \csc\left(\frac{\mu_x}{2} - \mu_y\right) - \csc \frac{\mu_x}{2} \sum_s^S \frac{\beta_x(s)}{\beta_y(s)} \right] \\
& \times \frac{1}{2} \prod_s^S S_s \sqrt{\beta_x(s)} \beta_y(s)
\end{aligned}$$

$$\begin{aligned}
w_{yy} \simeq & -\frac{3L}{16} \sum_s^D \gamma_y^2(s) + \frac{1}{16} \sum_s^S S_s^2 \beta_x(s) \beta_y(s)^2 \\
& \times \left[ 4 \cot \frac{\mu_x}{2} + \sin \mu_x \csc\left(\frac{\mu_x}{2} + \mu_y\right) \csc\left(\frac{\mu_x}{2} - \mu_y\right) \right] \\
& + \frac{1}{8} \left[ 4 \csc \frac{\mu_x}{2} + \csc\left(\frac{\mu_x}{2} + \mu_y\right) + \csc\left(\frac{\mu_x}{2} - \mu_y\right) \right] \\
& \times \prod_s^S S_s \sqrt{\beta_x(s)} \beta_y(s)
\end{aligned}$$

$$\begin{aligned}
w_{xd} \simeq & -\frac{3L}{4} \sum_s^D \gamma_x(s) \eta'(s)^2 - \sum_s^S \beta_x(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \\
& + \frac{1}{2} \cot \mu_x \sum_s^S \left[ \beta_x(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \right]^2 \\
& + \csc \mu_x \prod_s^S \beta_x(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \\
& + \csc \frac{\mu_x}{2} \sum_{1,2}^S \frac{S_2}{2} \beta_x(2) \eta(1) (S_1 \eta(1) - \frac{1}{F_1}) \sqrt{\beta_x(1) \beta_x(2)} \\
& + \frac{1}{2} \cot \frac{\mu_x}{2} \sum_s^S S_s \eta(s) (S_s \eta(s) - \frac{1}{F_s}) \beta_x(s)^2
\end{aligned}$$

$$\begin{aligned}
w_{yd} \simeq & -\frac{L}{4} \sum_s^D \gamma_y(s) \eta'(s)^2 + \sum_s^S \beta_y(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \\
& + \frac{1}{2} \cot \mu_y \sum_s^S \left[ \beta_y(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \right]^2 \\
& + \csc \mu_y \prod_s^S \beta_y(s) \left( \frac{1}{2F_s} - S_s \beta_x(s) \right) \\
& - \csc \frac{\mu_x}{2} \sum_{1,2}^S \frac{S_2}{2} \beta_y(2) \eta(1) (S_1 \eta(1) - \frac{1}{F_1}) \sqrt{\beta_x(1) \beta(2)} \\
& - \frac{1}{2} \cot \frac{\mu_x}{2} \sum_s^S S_s \eta(s) (S_s \eta(s) - \frac{1}{F_s}) \beta_x(s) \beta_y(s)
\end{aligned} \tag{13}$$

Exact expressions of the  $w$ -coefficients are too lengthy to be included here.

The required octupole strengths are such that the five  $C$ -coefficients in Eq.(12) are equal to zero. For the case when two of the octupoles are located next to the two sextupoles and the

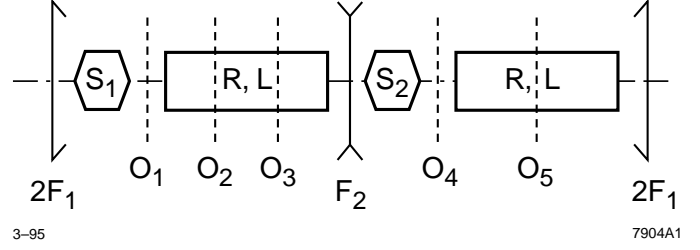


Figure 1. Unit cell of an achromat layout.

other three are at the  $\frac{1}{3}$ ,  $\frac{2}{3}$ , and the  $\frac{1}{2}$  locations of the two bending magnets, we find

$$O_1 \simeq \frac{a+b}{6f^3D}, \quad O_2 \simeq \frac{81(c+d)}{2fD}, \quad O_3 \simeq \frac{81(c-d)}{2fD}$$

$$O_4 \simeq \frac{a-b}{6f^3D}, \quad O_5 \simeq \frac{128\epsilon}{3(2f^2-1)D}$$

$$a = 2f(1360 - 22846f^2 - 74476f^4 + 695809f^6 - 1438146f^8 + 1200096f^{10} - 326592f^{12})$$

$$b = -352 - 3360f^2 + 233290f^4 - 1070910f^6 + 1917603f^8 - 1364850f^{10} + 361584f^{12}$$

$$c = 6f(-42 + 1076f^2 - 7409f^4 + 16306f^6 - 14368f^8 + 4032f^{10})$$

$$d = 8 - 394f^2 + 5322f^4 - 16907f^6 + 14866f^8 - 4464f^{10}$$

$$e = -368 + 10536f^2 - 92342f^4 + 307222f^6 - 470547f^8 + 330642f^{10} - 81648f^{12}$$

$$D = (4f^2 - 1)^2(3f^2 - 4)(10 - 173f^2 - 261f^4 + 324f^6)L^3\epsilon_1^2 \tag{14}$$

We have defined the dimensionless parameter  $f = \frac{2F_1}{L}$  and have assumed that  $\epsilon_1 = \frac{L}{R} \ll 1$  and  $|\frac{F_1+F_2}{L}| \ll 1$ .

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