

Reduction of Energy Sweep of the ETA-II Beam*

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Abstract

The ETA-II electron beam will be used to drive a high power microwave frequency FEL for plasma heating experiments. For maximum FEL output power the beam energy at the entrance to the wiggler should be within $\pm 1\%$ of the wiggler resonance value. In initial operations the ETA-II beam energy stayed within this range for a maximum time of less than 13 ns. Much of the energy variation was due to the design of the pulsed power feeds to the accelerator induction cells. A new multicable pulsed power feed design was tested in a shortened version of ETA-II where it extended the time during which the beam energy stayed within the $\pm 1\%$ limits to greater than 40 ns. These design changes are now being incorporated into the full accelerator.

I. INTRODUCTION

The Experimental Test Accelerator II (ETA-II) facility is funded to develop and demonstrate the electron induction linac technology necessary for driving FELs at high average power [1]. The facility consists of the ETA-II accelerator, (the first induction linac designed specifically to drive an FEL), and several test stands for studying cathode brightness and poisoning, ferrite response, pulse-power feeds, and the operation of magnetic switches at high repetition frequency (prf). The design changes described in this report, which were tested on a shortened version of the accelerator, are now being incorporated in the full machine. When completed ETA-II will be able to supply 70 ns full-width-half-maximum pulses of 2-3 kA beam current, 6-7 Mev energy, in fifty pulse bursts at 5 kHz prf with a burst repetition rate of 0.5 Hz. As a technology demonstration we intend to use ETA-II to drive a 140 GHz FEL, the Intense Microwave Prototype (IMP) amplifier system [2], whose output will be used for plasma heating experiments on the LLNL Microwave Tokamak Experiment (MTX).

The IMP system consists of a microwave oscillator, a quasi-optic coupler which injects the oscillator output coaxially with the beam and a wiggler which couples beam energy to the electromagnetic field. The high magnetic field and wide tunability capabilities required for the FEL are provided by a permanent magnet-laced electromagnetic wiggler with a 10-cm period and an overall length of 5.5 m.

II. ENERGY SWEEP TOLERANCES

Variation of beam energy will affect the FEL output power by two different mechanisms: through gain change as the beam energy deviates from resonance with the wiggler, and through energy sensitivity of the alignment of the beam with the axis of the wiggler. Sensitivity of beam power to off resonance operation has been calculated using the free electron laser simulation code, FRED [3,4]. For code input parameters in the expected operating range FRED predicts a 1% deviation from resonance energy reduces output power by $\sim 6\%$, a 2% deviation by $\sim 25\%$.

Initial misalignment of the beam with respect to the solenoidal guide field of the accelerator will result in the beam centroid following a helical path through the accelerator. Localized field errors will introduce jumps in the guiding-center radius and position along the way. If the energy is constant the beam path will be fixed in space but energy variation will modulate the cyclotron wavelength and produce a complicated sweeping in time of the beam centroid position and angle at any point including the entrance to the wiggler. This behavior, called beam "corkscrew" motion [5]-[8], imposes stringent requirements on magnetic alignment and energy sweep.

In earlier operation two beam position monitors separated by a field free region were used to measure the spatial and angular sweep at the exit of the accelerator as the energy varied. A beam transport code was used to calculate the corresponding motion at the entrance to the wiggler and these values were used as input into FRED to determine their effect on the microwave power. For the measured corkscrew motion we estimated that a $\pm 1\%$ energy variation could decrease the output power by 30%, a much larger effect than merely being off resonance. Considerable improvement in magnetic alignment and reduction of corkscrew amplitude have been made since the above measurements [7] but the goal of keeping the energy variation within $\pm 1\%$ is still desirable. Maximizing the average FEL output power requires that the beam energy stay within these limits for a large fraction of the current pulse length. As a technology demonstration our immediate milestone has been to maintain the energy sweep within $\pm 1\%$ for at least 30 ns.

III. ENERGY SWEEP STUDIES

A. Beam energy measurement

Our primary beam energy diagnostic has been a magnetic spectrometer [1]. A bending magnet, located in the transport

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section between the accelerator and the wiggler, when energized, deflects the beam into a 45° side arm. Two pairs of beam position monitors, one on the input side and the other coaxial with the side arm are used to measure the variation of the deflection angle of the beam centroid in the bending plane around the 45° central angle. The system can detect angular variations due to energy changes of ~0.1% and has a 500 MHz bandwidth. The absolute energy calibration is derived from the mapping of the bending magnet's field.

B. Sources of energy variation

Energy variation may have either operational causes or be intrinsic to the design. Operational causes are those which affect shot reproducibility such as input voltage variation, timing jitter, variation of ferrite reset condition, and insulator breakdown. Such uncontrolled variation can make the accelerator almost impossible to tune and virtually useless. Two important additions were made to the ETA-II control system for the experiments described here, the first being a computer controlled feedback timing compensation system that corrects for timing drifts due to power supply variations and the second an arc and overvoltage protection system which interrupts accelerator operation when a fault occurs. The latter along with the multicable feed system modification, described below, limit the energy available for driving an arc and causing insulator damage. These changes greatly reduced uncontrolled variations and improved our ability to tune the machine. Remaining as problems are the intrinsic causes of energy variation within a shot -- time varying beam loading and cell impedance, and mismatches in the pulse-power feeds to the accelerator cells.

Measurements of beam energy variation at the output of ETA-II in its original configuration showed that the energy was within the $\pm 1\%$ limits for at most 13 ns [1], less than half of the period we could accept as a minimum. The source of most of this variation was traced to the cell pulse-power feeds. As originally configured, each ten-cell set was fed from its magnetic pulse compressor (MAG-1D) by a single 4 Ω water dielectric cable which connected to the input ends of a pair of busbars running parallel to the axis on opposite sides of the cell block. These provided a symmetrical power feed to the individual cells which tapped into the bars along the way. The far ends of the bars were terminated to reduce reflections. Although this design provided a neat mechanical solution to the problem of pulse-power distribution, measurement and analysis soon showed that electrically it was not satisfactory. The busbars form a slow wave structure, consequently the phase of the voltage pulse with respect to the beam pulse ($\beta=1$) varies with distance along the busbar. Since the beam loading modifies the applied voltage pulse, phase variation results in each gap seeing a different resultant voltage variation with time and since the final beam energy is the sum of the contributions of all of the gaps, it is not surprising that a large energy sweep was encountered.

C. Modeling the power feed.

A computer model of the pulse power feed was used to help understand its operation [9]. Experimental measurements of the injector current pulse shape, the MAG-1D voltage pulse shape and the variation of the cell leakage current with time were combined with a model of the busbar slow wave structure to calculate the time variation of each gap's voltage relative to the current pulse. The voltages were summed to give an estimate of the energy sweep of the output. The results of such a simulation are shown in Figure 1. We see that there is good agreement between the model's predictions and the experimental measurements of $\pm 1\%$ energy sweep for a

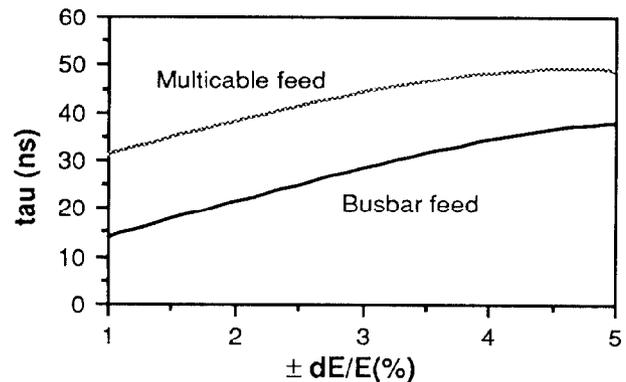


Figure 1. Time that beam energy stays within regulation range versus range (Simulation, 60 cells, $E=6$ Mev, $I=2$ kA)

maximum of 13ns with the old busbar feed.

Both experiment and modeling having shown that there was very little chance of meeting our milestone with the busbar power feed, the design of a new, multicable feed was undertaken. Such a feed system for the cells, while mechanically much more complex, allows transit time isolation from the other cells while proper choice of cable lengths insures constant phase between current pulse and gap voltages. Since it is best to feed the gaps symmetrically at two points, 180° apart, our approach was to use two 40 Ω solid dielectric cables to feed two cells in parallel. A short busbar on each side connects the high voltage electrodes of the cell pair and a cable connects to each busbar center. With this design there is ~1 ns phase difference between the two cells relative to the current pulse and some sloshing around of energy between the cell pairs during the current rise and fall when the load is not matched. Modeling of this system, detailed in reference [9], showed that this new design should enable us to meet our energy sweep milestone for the full machine for certain conditions of current, MAG-1D voltage, and timing. (Figure 1).

D. ETA-II tests.

On a test stand we developed a multicable feed system which would require minimum modification of the existing system. Each MAG-1D has two 4 Ω output cables and can

feed two ten-cell blocks. Rather than adapting the MAG-1D to the multicable feed, which would have been a major task, we installed a high voltage distribution box where transition was made from the two 4 Ω cables to twenty 40 Ω cables in parallel. The old busbar structure was replaced with the cell feed structure described above. After initial tests the new feed system was installed on the first two ten-cell blocks of ETA-II for evaluation before modifying the remainder of the accelerator. The remaining four ten-cell blocks were removed and replaced with a transport section, and the injector, whose design concentrates its voltage across the A-K gap, was left unchanged. This shortened version of ETA-II was capable of producing a 2.5-3 Mev beam.

The model was used to predict optimum values of MAG-1D voltage and relative timing between the injector and the accelerator for minimizing the energy sweep of a ~ 1.5 kA beam from the accelerator. Experimental measurements agreed well with predictions of the model. If we define τ as the time the beam energy has a maximum peak to peak variation of 2%, then we were able to find conditions of voltage and timing delay near the model values for which τ exceeded 40 ns. The best recorded shot is shown in Figure 2. While this shot is on the upper edge of the τ distribution the probability of

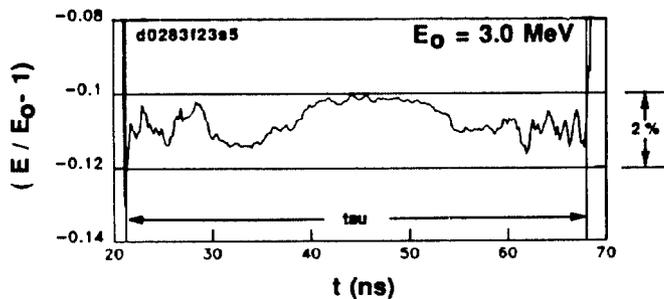


Figure 2. Beam energy variation versus time ($I \sim 1.5$ kA)

exceeding the 30 ns milestone for these operating conditions was very high. Figure 3 is a histogram of the τ distribution for a set of 50 shots with the same input conditions. This data

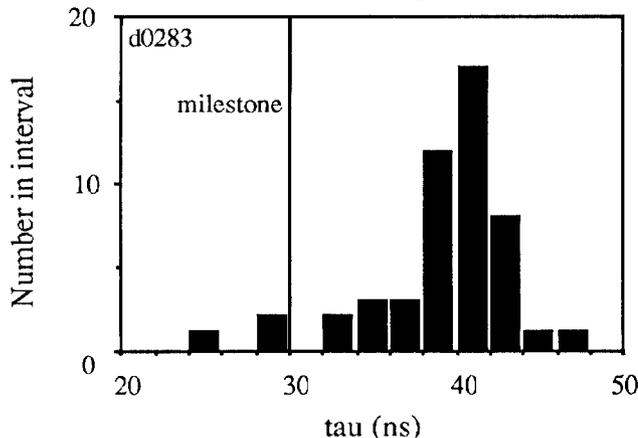


Figure 3. Histogram of τ distribution for a set of 50 shots.

was recorded as 10 shot sets at various times during a days operation. Over this period of operation the drift of the central energy value was less than 1% (Figure 4)

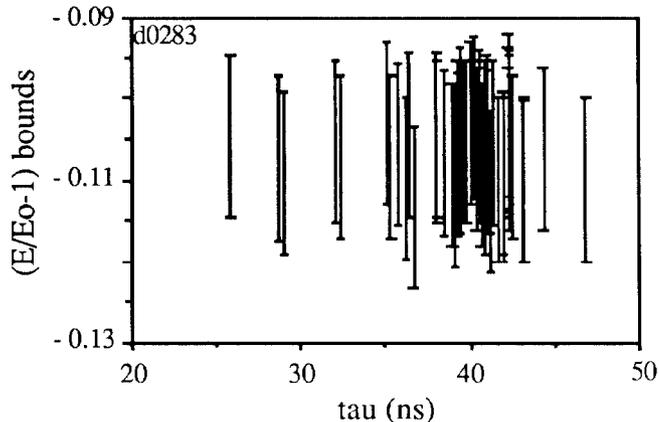


Figure 4. Energy bounds versus τ for data set.

IV. SUMMARY

In recent operation of a shortened version of ETA-II with only the injector and the first two ten-cell blocks we have been able to keep the energy sweep of the output beam to less than 2% for periods greater than 40 ns. The key ingredient of this achievement was the retrofit of a new multicable pulse power feed to the 20 cells and the development of a model for predicting optimum operating parameters. This success was perhaps a necessary but not a sufficient condition to guarantee that we will be able to maintain the same degree of regulation at higher current and with the addition of the remaining four ten-cell blocks; however, the model predicts that a retrofit of the remaining ten-cell blocks with the new feeds will lead to the desired energy regulation at full energy and higher currents.

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