

Fabrication and Tests of Prototype Quadrupole Magnets for the Storage Ring of the Advanced Photon Source*

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Abstract

Prototype quadrupole magnets for the APS storage ring have been fabricated and tested. Mechanical stability of the magnet poles and acceptable field quality have been achieved. Geometries of the pole-end bevels have been studied in order to simplify the design of the magnet end-plate. The field saturation at different segments of the magnet has been measured to evaluate the magnet efficiency.

I. INTRODUCTION

The magnetic lattice of the positron storage ring for the 7-GeV Advanced Photon Source (APS) requires 400 quadrupole magnets [1]. The quadrupoles are of the conventional resistive type, and have three different magnetic lengths and five families as shown in Table 1. The required beam stay-clear aperture is $x=\pm 35$ mm and $y=\pm 20$ mm. Each magnet is excited by an independent power supply. The design of the magnets is the same except for the length of the magnet.

Figure 1 shows the current-lead end of a 0.8-m length prototype quadrupole along with a section of the vacuum chamber. The magnet design is restricted by the requirements of the vacuum chamber geometry for the photon beam ports and antechamber. Consequently, the magnet does not have the flux return yoke between the top and bottom halves of the magnet, and has relatively long and narrow magnet poles [2-3]. Two prototype magnets have been fabricated and tested using a rotating coil method.

The normal and skew multipole field coefficients, b_n and a_n , for a 2-D magnetic field, $B = B_y + i B_x$, are defined

$$B = B_0 \sum_{n=0}^{\infty} (b_n + i a_n) (x + i y)^n \quad (1)$$

where the coefficients are in cm^{-n} units, and $b_1=1.0 \text{ cm}^{-1}$ and $a_1=0$. Relative values of the coefficients with respect to the main quadrupole field component at radius $r_0=2.5$ cm are used:

$$b_n(\text{at } r_0) = b_n r_0^n / b_1 r_0, \quad a_n(\text{at } r_0) = a_n r_0^n / b_1 r_0. \quad (2)$$

II. MAGNET DESIGN AND FABRICATION

Figure 2 shows the end-view of a one-half section of the magnet. The magnet pole has 45° symmetry and is tapered to

reduce the flux saturation. In order to minimize the physical length of the magnet for a given length of the core, which is 0.765m long, the magnet end-plates have chamfers of 19.1-mm/45°-cut as shown in Fig. 2 so that the magnet coil fits snugly around the magnet pole.

Table 1
Parameters of the storage ring quadrupole magnets for the 7-GeV operation.

	<u>Q1</u>	<u>Q2</u>	<u>Q3</u>	<u>Q4</u>	<u>Q5</u>
L (m)	0.50	0.80	0.50	0.50	0.60
B' (T/m)	-10.843	15.792	-10.585	-18.902	18.248
B'L (T)	-5.421	12.634	-5.293	-9.451	10.949
I (A) ^a	215	320	210	415	390
ε (%) ^a	99	97.5	99	89	92

^a Measured data for the prototype magnets.

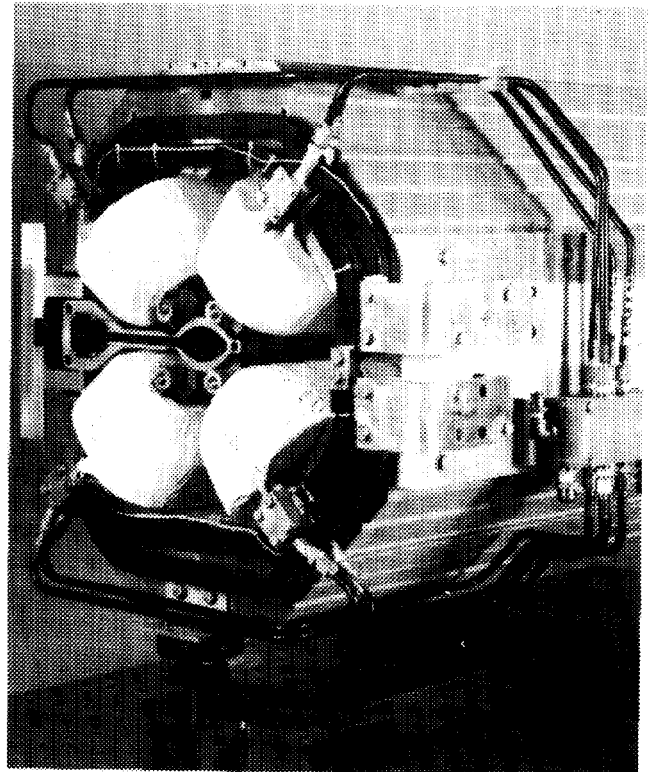


Fig. 1. Photograph of the current-lead end of a 0.8-m prototype quadrupole magnet.

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The end plates are designed to have a removable pole-tip. The removable pole-tip does not have the 45°-cut chamfers. This requires the attachment of the pole-tips after the installation of the magnet coils.

The two quadrants of the assembled laminations are welded at joints "A" and "B" as shown in Fig. 2. The weld joints have welding-relief grooves to reduce the effects of weld shrinkage. The laminations are 1.52-mm thick low carbon steel. The laminations have alignment notches as shown in Fig. 2 used for the attachment of a removable alignment fixture used for the measurements of the magnetic axis and for the survey of the magnets in the storage ring.

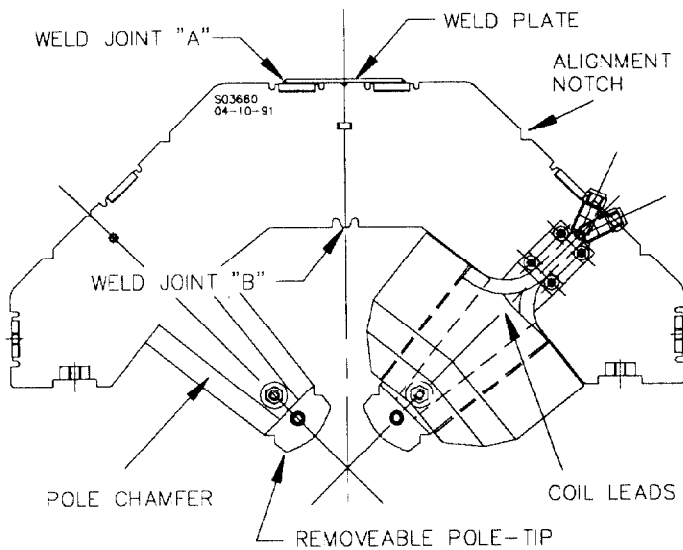


Fig.2. End-view of the top-half section of the magnet.

III. MAGNET MEASUREMENTS

A. Mechanical Stability

For the first prototype magnet the two quadrants of each half-magnet were welded only at joint "A" in Fig. 2. That left a gap at "B" allowing magnet pole movements of approximately 0.15 mm at high field. Additional welds applied at "B" between the two quadrants for both prototype magnets prevented pole movements and achieved the required mechanical stability of the magnets. The magnet pole movements before and after the additional welds were reflected in the measurements of the skew sextupole and normal octapole field coefficients.

B. Multipole Field Coefficients

Shown in Fig. 3 are the normal and skew multipole field coefficients for the second prototype magnet at a beam aperture radius of 2.5 cm. The magnet excitation currents listed in Table 1 for the five families of the quadrupoles are within the measurement currents in Fig. 3.

After the main quadrupole field component, the first two allowable terms are b_5 (duodecapole) and b_9 (20-pole) and the corresponding skew coefficients. The values of the two coefficients are obtained with a pole end-bevel geometry of 12.8 mm x 12.8 mm-cut. Two-dimensional calculations of the two coefficients at a high excitation current are $b_5 = -0.34 \times 10^{-4}$ and $b_9 = 0.69 \times 10^{-4}$. The "body" measurements of the two coefficients agree with these calculations within 1×10^{-4} .

In Fig. 3 the two largest unallowed coefficients are sextupole and octapole terms, $b_2 = 2.5 \times 10^{-4}$ and $b_3 = 3.5 \times 10^{-4}$. They are due to the imperfections in the stacking of the laminations, welding of the two quadrants and assembly of the top and bottom half-magnet. All these multipole coefficients are within acceptable levels for the required dynamic aperture of the positron beam in the storage ring.

C. Pole-End Bevels

The pole-end bevels in the removable pole-tips for the reference design have a geometry of 12.8 mm x 12.8 mm-cut. The bevels increased b_5 by 5.5×10^{-4} and reduced b_9 by 0.1×10^{-4} compared to those two allowable terms for the pole-tips without any bevels.

In Table 2, the values of b_5 and b_9 for five different pole-bevels and chamfers are listed. It shows that b_9 is relatively insensitive to the bevel and chamfer geometries compared to b_5 . For the bevels 9.6 mm x 17.4 mm with a chamfer up to 16.5 mm, the coefficients are within 2×10^{-4} units.

Table 2
Pole-end bevels on the removable pole-tips and integrated b_5 and b_9 coefficients at 2.5 cm in 10^{-4} unit.

Bevels (r x z) with chamfers [mm]	250.7 A		450.6 A	
	b_5	b_9	b_5	b_9
a. 12.8x12.8	0.19	-0.53	-1.14	-0.59
b. 9.6x17.4	2.67	-0.62	1.13	-0.68
c. 9.6x17.4 with 12.8 ^a	0.09	-0.74	-1.09	-0.78
d. 9.6x17.4 with 16.5	-0.64	-0.80	-2.01	-0.83
e. 9.6x17.4 with 19.1	-1.42	-0.83	-3.88	-0.88

^a Chamfers are in the same direction with the chamfers of the magnet end-plates.

D. Excitation Efficiency

Plotted in Fig. 4 are the measured data of the field gradient integrals normalized to the excitation currents. The gradient integrals of the two prototypes differed by less than 5×10^{-3} for the currents higher than 250 A.

Normalized field gradients, B'/I , for different segments of the magnet were measured at two currents and listed in Table 3. For an infinite permeability of the lamination steel, calculated gradient is $B'/I = 5.18363 \times 10^{-2}$ T/m·A. A two-

dimensional calculation of the efficiency of the excitation at 450A (7.3Gev) is 88.5% compared to the measured value of 87.2%.

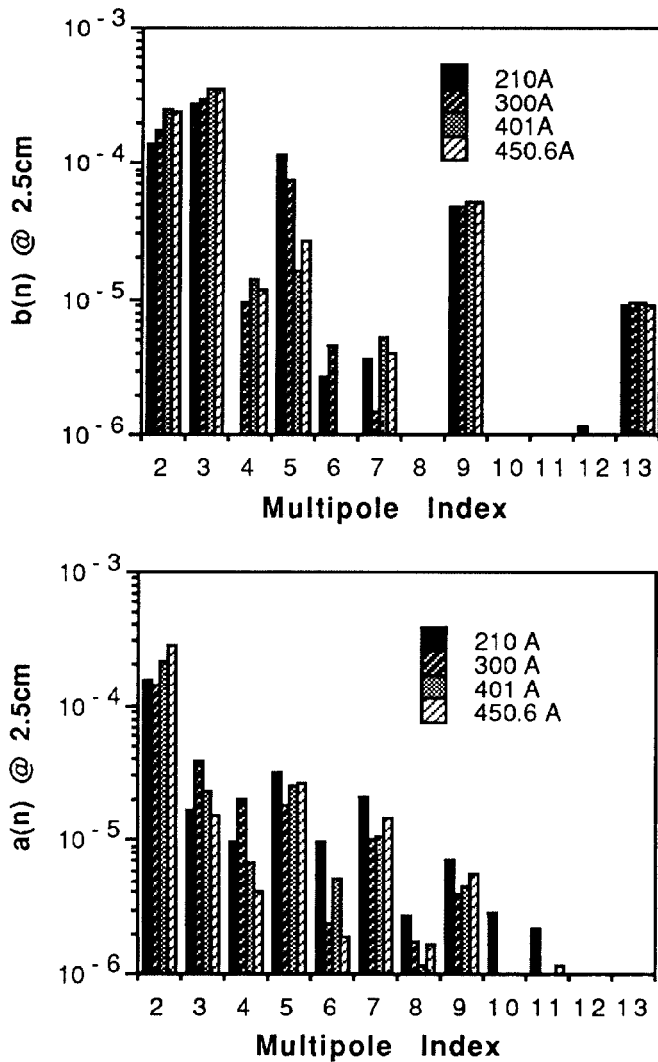


Fig. 3. Magnitudes of the relative multipole field coefficients at $r_0=2.5$ cm. The following coefficients have negative values: b_5 at 450.6A, b_6 , b_9 , b_{13} , a_3 , a_4 except at 210A, a_6 , a_8 at 410A and 450.6A, a_9 at 450.6A, and a_{10} .

IV. CONCLUSION

From the fabrication and measurements of two prototype quadrupoles for the storage ring, the mechanical stability of the magnet poles and routine assembly procedure for the fabrication of production magnets have been achieved. The measured magnetic fields in terms of multipole coefficients for the prototypes meet the requirements for the positron beam dynamics. Use of removable pole-tip geometries of pole-end bevels has been investigated in order to design the magnet end-plate. In order to improve the excitation efficiency for the

operation above 7-GeV, the pole geometry has been modified for the production magnets.

Table 3
Averaged field gradients at different sections in the longitudinal direction normalized to the magnet excitation currents

z (m)	B'/I (10^{-2} T/m·A)	
	at 250.79A	at 450.75A
0 - 0.215	5.122	4.518
0.215 - 0.270	5.101	4.485
0.270 - 0.325	4.993	4.208

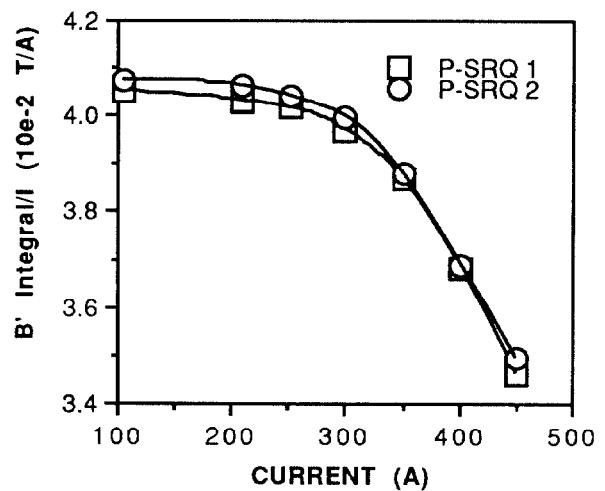


Fig. 4. Magnet excitations of the two prototype quadrupoles.

V. ACKNOWLEDGMENTS

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VI. REFERENCES

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