

## DESIGN FOR A SECOND-GENERATION PROTON STORAGE RING AT LAMPF

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### ABSTRACT

A conceptual design is presented for a second-generation proton storage ring complex at LAMPF. The facility would consist of two stacked racetrack-shaped machines. These machines would deliver a 1.2-mA beam of 1.6-GeV protons at 48 Hz. The pulse length would be 1.75  $\mu$ sec which represents a time compression of 570.

### 1. INTRODUCTION

There is some local interest for a 1.6-GeV proton storage ring (PSR) which will deliver nominally 2 MW of beam power at 48 Hz. The design for the present PSR is just 80 kW so the improvement is a factor of  $\sim 25$ . The 1.6-GeV kinetic energy would be obtained from an add-on linac to LAMPF. The flux requirement is  $1.5 \times 10^{14}$  ppp at 48 Hz; the beam would be sent alternately to neutron production, and neutrino production experiments, respectively. These facilities would each operate at 24 Hz.

This request can be met by using two stacked rings which are respectively fed with two successive LAMPF macropulses. Each ring would store  $7.5 \times 10^{13}$  protons. There are two constraints which must be met: (1) The slow losses which occur in the Los Alamos Proton Storage Ring (PSR) cannot take place in these rings.<sup>1</sup> (2) It is necessary to store beam in one of these rings for up to 8 msec, so the rings must be stable against coherent instability.

The machine requirements have been met in a first-order design which is the subject of the remainder of this report.<sup>2</sup> The design layout is shown in Fig. 1. The shape is that of a near racetrack. The four bend sections are 90° bend achromats. The two short straight sections each contain fast extraction systems. The rf cavity is located in a dispersion free zone. The long straight section containing the injection area includes a special injection chicane, the stripping foil, an H<sup>-</sup>/H<sup>0</sup> dump, two orbit bumpers, and two halo collimators. All of these are discussed below.

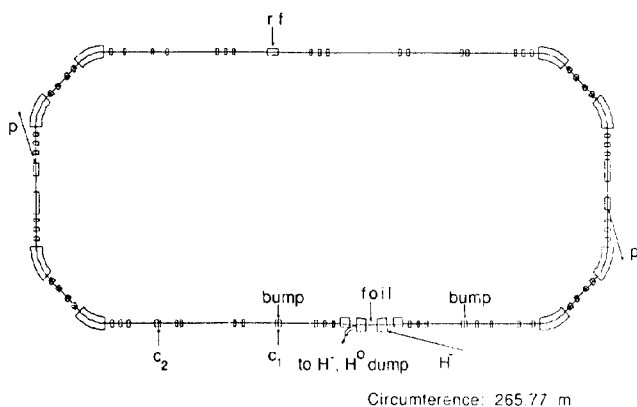


Fig. 1. Plan view layout of the new compressor rings.

Table I lists the parameters for the designed machines. In Section 2, I discuss the lattice design. In Section 3, I explain the mechanics of beam transfers. Collimation is briefly discussed in Section 4. Longitudinal simulations are treated in Section 5. The subject of coherent instabilities is addressed in Section 6. Concluding remarks are given in Section 7.

Table I. Machine Parameters

Circumference	265.77 m
Number of Rings/Superperiods	2/2
Circulating Current/Ring	12.6 A
Revolution Frequency	1.048 MHz
Number of Turns Injected	1048
Betatron Tunes $Q_x, Q_y$	5.23, 4.23
Chromaticity $Q'_x, Q'_y$	-7.32, -6.76
Transition Gamma $\gamma_t$	8.19

### 2. LATTICE DESIGN

The machine lattice functions across half the machine are depicted in Fig. 2(a). The beam halfwidths are shown in Fig. 2(b)—these sizes were calculated using the expressions

$$x = \sqrt{\beta_x \epsilon_x} + \left| \eta_x \frac{dp}{p} \right| \quad \text{and} \quad y = \sqrt{\beta_y \epsilon_y} \quad (2.1) \text{ and } (2.2)$$

with  $\epsilon_x = \epsilon_y = 100$  mm-mr and  $dp/p = \pm 0.003$ . These values were obtained from a study of the injection process. The maximum vertical beam size in the dipoles is of order  $\pm 35$  mm.

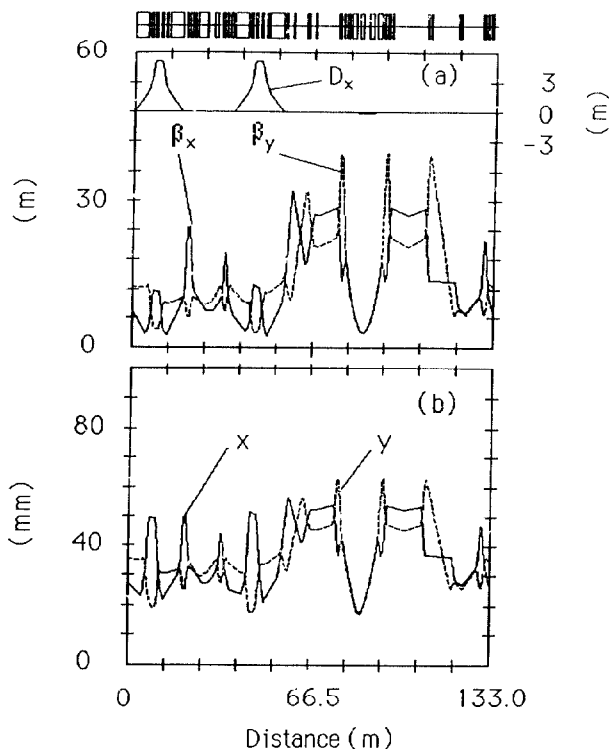


Fig. 2. (a) Machine lattice functions for 1 superperiod; (b) half beamwidths calculated using Eqs. (2.1) and (2.2). The emittances  $\epsilon_x$  and  $\epsilon_y$  are both 100 mm-mr and  $dp/p = 0.003$ .

### 3. BEAM TRANSFERS

#### A. $H^-$ Injection

The ring injection takes place via the process  $H^- \rightarrow H^+$  in a  $250\text{-}\mu\text{g}/\text{cm}^2$  carbon stripping foil. Figure 3 shows a closeup plan view of the circulating proton and injected  $H^-$  beams in the region of the four-dipole chicane. The four dipoles translate the proton beam  $171.5\text{ mm}$  to beam left of centerline at the stripping foil location (call this the center). The two orbit bumpers (see Fig. 1) are separated by  $180^\circ$  in horizontal betatron phase—they serve to further displace the translated proton beam at the foil. The bump starts out at  $20\text{ mm}$  left of center and reduces to  $10\text{ mm}$  during the  $1\text{-msec}$  injection period (this time corresponds to  $\sim 1050$  turns). After the injection the bumps are rapidly reduced to zero. Referring to Fig. 3, the  $H^-$  are injected into the second dipole and are nominally placed at  $25\text{ mm}$  beam left of center, and on-axis vertically. Unstripped  $H^-$  (or partially stripped  $H^0$ ) will exit the third dipole displaced to the outside of the proton beam; they will pass through another stripping foil, so as to convert to protons, and then be conducted away to a dump. The injected  $H^-$  beam should be matched to the machine in 6-D phase space.

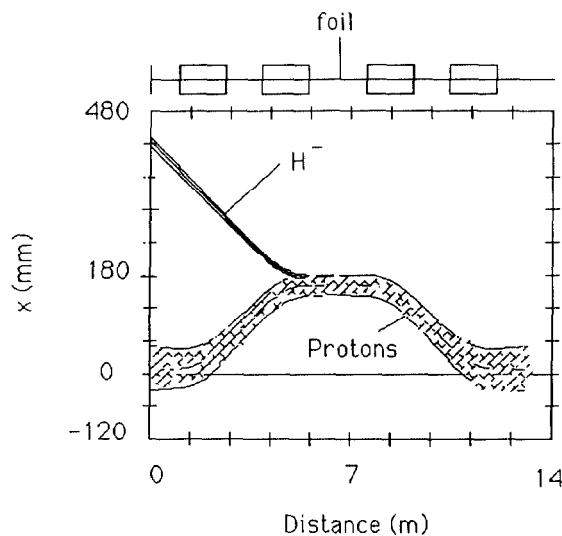


Fig. 3. Circulating proton and injected  $H^-$  beam envelopes within the four-dipole injection chicane. The  $H^-$  pass on the outside of the first dipole. The proton beam geometric emittance is  $100\text{ mm}\cdot\text{mr}$ . The  $H^-$  injected emittance is of order  $2\text{--}3\text{ mm}\cdot\text{mr}$ .

#### B. Fast Extraction

Beam is extracted from each ring in a single turn and sent in box-car fashion to the experimental targets. Timewise, first one ring is filled in  $1\text{ msec}$  and the second ring is filled  $1/120\text{ sec}$  later. They are fast extracted together (separated by one revolution time). These processes are repeated  $48$  times per sec. The extracted pulse length would be  $1.75\text{ }\mu\text{sec}$ , so the time compression is  $\sim 570$ . A  $3.5\text{-m}$  ferrite kicker displaces the protons into the field region of a  $1.5\text{-m}$  d.c. septum magnet from which they are conducted to the appropriate experimental area (see Fig. 1).

### 4. COLLIMATION

The injection foil is positioned offset to the outside of the machine to reduce the number of repeat proton traversals. These traversals cause the rms transverse emittance to grow by an amount  $\beta^* \theta^2 fN(t)/2$  where  $\beta^*$  is the beta function at the foil,  $\theta$

is the rms scattering angle for a single traversal, and  $fN(t)$  is the number of foil traversals in  $N$  turns up to time  $t$ . To minimize the emittance growth I designed for  $\beta^* = 3.0\text{ m}$  at the foil; we try to reduce the probability for a traversal ( $f$ ) by locating the foil edge close to the injected  $H^-$  beam spot. Simulations indicate a value of  $0.055$  for  $f$ . In fact, rms emittance growth due to foil scattering is only a few percent. Of more concern are the large angle scatters due to nuclear or single coulomb scattering in the thin stripping foil. The largest angle we can reasonably expect to contain is about  $2\text{ mr}$ . The probability for even larger scatters is  $\sim 7 \times 10^{-6}$ . If we roughly take  $25$  traversals for the average proton, then we would expect a loss of  $105\text{ nA}$  for  $600\text{ }\mu\text{A}$ . This loss would activate each machine downstream of the foil. We plan to quickly absorb these large angle scatters in the downstream collimators  $C_1$  and  $C_2$  (see Fig. 1). The collimators are strategically placed  $90^\circ$  and  $180^\circ$  in betatron phase downstream of the stripping foil, respectively. Some adjustment to the actual design would be necessary since an orbit bump magnet is coincident with  $C_1$ .

### 5. LONGITUDINAL SIMULATIONS

The function of the rf system is to (i) maintain a longitudinal gap in the beam for lossless extraction and (ii) to produce enough relative momentum spread to keep the circulating protons coherently stable. The average circulating current is  $12.6$  amperes in each ring at full intensity. With a fundamental rf system, bunching will occur and the peak currents can be expected to rise to over  $40$  amperes; this will surely result in coherent instability and beam loss. For these rings I suggest use of the rf waveform given by Eq. (5.1). The rf voltage is composed of the fundamental plus four harmonics

$$V(\phi) = V_0 \sum_{i=1}^5 V_i \sin(i\phi) \quad (5.1)$$

with  $V_1 = 0.2067$ ,  $V_2 = -0.331$ ,  $V_3 = 0.333$ ,  $V_4 = -0.236$ , and  $V_5 = 0.103$ . This waveform should maintain a gap in the beam. However, little or no increase in the  $dp/p$  occurs. We obtain larger  $dp/p$  values by just sweeping the energy of the injected beam in the last linac module. This sweeping is done sinusoidally with two oscillations over the  $1\text{ msec}$  injection period.

A simulation has been performed in order to demonstrate the viability of the method. Beam was injected uniformly in rf phase  $\phi$  for  $|\phi| \leq 2.4$  radians—this corresponds to populating  $\sim 146$  microbunches of the  $192$  possible. The  $dp/p$  were generated in a Gaussian fashion with  $\sigma_p/p = 0.05\%$ . During injection, the central value of the  $dp/p$  was varied sinusoidally with turn number  $t$  as  $0.002 \sin(2\pi t/525)$  (in absolute units). The rf voltage of the fundamental  $V_0 * V_1 = 3.5\text{ kV}$ , so the peak voltage of the waveform given by Eq. (5.1) is  $16.9\text{ kV}$ . The projections of  $\phi$  and  $dp/p$  are given in Figs. 4(a) and 4(b), respectively. The gap is maintained in Fig. 4(a) and the rms  $\phi$  width is unchanged from the injected value. The FWHM of the  $dp/p$  distribution is of order  $0.5\%$ .

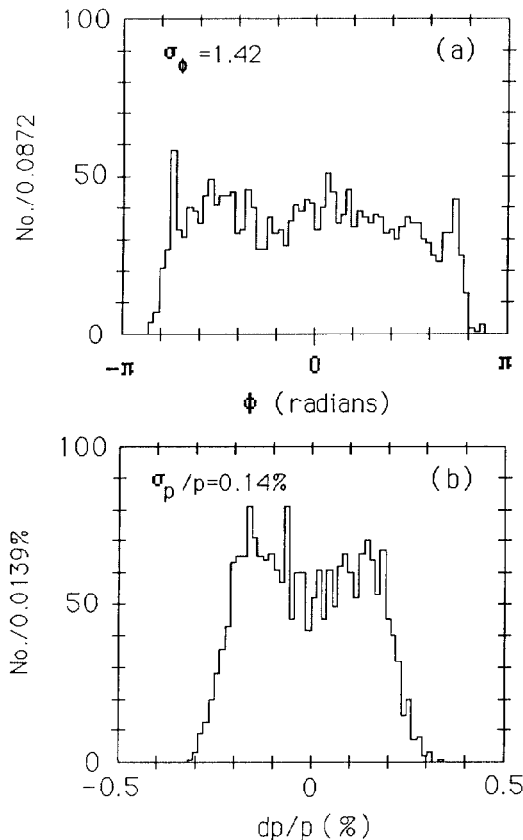


Fig. 4. Rf simulation results for 1050 turns of injection.

## 6. BEAM STABILITY

### A. Space-Charge Tune Shift

The space-charge tune shift is given by<sup>3</sup>

$$|\Delta Q_y| = G_y \frac{2.4 \text{ mm-mr}}{\epsilon_N} \frac{N}{10^{13}} \frac{F_y}{B\beta\gamma^2} \quad (6.1)$$

where  $G_y$  is a form factor depending upon the  $x$ - $y$  spatial distribution,  $\epsilon_N$  is the normalized vertical emittance which contains 87% of the beam, and  $N$  is the number of circulating protons. The remaining term is approximated by

$$\frac{F_y}{B\beta\gamma^2} \sim \frac{1.02}{B\beta\gamma^2} + 0.045\beta \quad (6.2)$$

where  $B$  is the bunching factor,  $\beta = pc/E$ , and  $\gamma = E/moc^2$ .

We pessimistically take  $G_y = 2$  corresponding to a 2D Gaussian distribution. Next,  $\epsilon_N$  is given by  $\epsilon_y\beta\gamma$  and we use  $\epsilon_y = 40 \text{ mm-mr}$  as determined from injection simulations. I assume  $N = 7.5 \times 10^{13}$  and a bunching factor  $B = 0.65$ . With these choices the space-charge tune shift is computed to be  $|\Delta Q_y| = 0.098$ .

### B. Coherent Stability

The major coupling impedances are imaginary and due to space charge. They are

$$\frac{Z_\ell}{n} = \frac{i}{2} \frac{Z_0}{\beta\gamma^2} \left( 1 + 2\ell n \frac{b}{a} \right) \quad (6.3)$$

where  $Z_0$  is the impedance of free space,  $Z_0 = 377 \text{ ohms}$ , and  $b/a$  is the ratio of beam pipe to beam radius  $b/a \sim 2.67$ . We obtain  $Z_\ell/n = i82\Omega$ . The transverse impedance

$$Z_\perp = \frac{iRZ_0}{\beta^2\gamma^2} \left( \frac{1}{a^2} - \frac{1}{b^2} \right) = i2.4 \times 10^6 \Omega/\text{m} \quad (6.4)$$

I chose  $a = 0.03 \text{ m}$  and  $b = 0.08 \text{ m}$ . The average circulating current  $I = 12.6 \text{ amperes}$  and the peak  $\hat{I} = 19.4 \text{ amperes}$  for the rf system contemplated.

The test for longitudinal stability

$$\left( \frac{dp}{p} \right) \geq \left[ \frac{\hat{I}}{\beta^2|\eta|E} \left| \frac{Z_\ell}{n} \right| \right]^{1/2} \quad (6.5)$$

where  $\eta = \gamma_i^{-2} - \gamma^{-2} = -0.1218$ .

I find  $(dp/p)_{\text{FWHM}} \geq 0.24\%$ . This requirement is easily satisfied by our beam with  $(dp/p)_{\text{FWHM}} \sim 0.5\%$  so the beam will be longitudinally stable.

The test for transverse stability

$$|Z_\perp| \leq 4 \frac{\beta E}{\hat{I}} \frac{Q_y}{R} \left[ (n - Q_y)\eta + \frac{dQ_y}{dp/p} \right] \left( \frac{dp}{p} \right)_{\text{FWHM}} \quad (6.6)$$

results in

$$|Z_\perp| \leq 0.2395 \times 10^6 [(n - 4.23) \times 0.12 + 6.75]$$

If we use  $|Z_\perp| = 2.4 \times 10^6 \Omega/\text{m}$ , then we find the machine is stable for  $n > 31$  or frequencies  $f > 32.5 \text{ MHz}$ . Below this frequency the machine is unstable with a growth rate given by

$$\frac{1}{\tau} = \frac{Ic}{4\pi Q_y E} (Re Z_\perp) = 2.8 \times 10^{-2} Re(Z_\perp) \text{ sec}^{-1} .$$

For  $\tau > 500 \mu\text{sec}$  we need  $Re(Z_\perp) \leq 71 \text{ k}\Omega/\text{m}$ . This requirement may be difficult to meet. However, the beam can be stabilized by simply increasing the chromaticity  $dQ_y/(dp/p)$  to  $-10$  from its nominal value of  $-6.75$ .

## 7. CONCLUSION

These high-intensity machines do look feasible. If constructed, they would supply 12 times more beam power for producing spallation neutrons than the PSR design. A number of subjects still need to be addressed: collimator calculation, tracking, optimization, and a cost estimate. The present  $H^-$  source would have to be upgraded by a factor of 2.

## REFERENCES

1. R. J. Macek, D. H. Fitzgerald, R. L. Hutson, M. A. Plum, and H. A. Thiessen, Los Alamos National Laboratory Report LA-UR-88-1682 (1988).
2. For a detailed design, see, e.g., E. Colton, Los Alamos National Laboratory Technical Note AHF 88-025.
3. See e.g. J. Crawford et al., Feasibility Study for a European Hadron Facility, Report EHF-86-33 (1986, unpublished).