

## TEST OF SUPERCONDUCTING ACCELERATOR STRUCTURES IN A CLOSED VACUUM SYSTEM

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### Abstract

During the installation of superconducting accelerator structures into the helium cryostat the evacuated cavities usually have to be let up to atmospheric pressure. This procedure represents a risk to the cavity performance and in many cases degradations have been observed.

An assembly scheme for superconducting accelerator structures has been devised, which avoids the exposure of the interior cavity surface to gases and minimizes the probability of accidental deposition of dust or debris on the cavity surface.

Two gate valves are mounted onto the cavity assembly at both beam - pipe ends and the rf - coupling port is closed with a vacuum tight rf - window. This assembly permits the pre - testing of accelerator sections in a laboratory test set - up and the evaluation of their performance prior to the installation into the cryostat. Tests on the CORNELL/CEBAF elliptical niobium cavity and the effects caused by actuating the gate valves are reported.

In an assembly of two 5 - cell cavities into a cavity pair of 1 m length an average accelerating gradient of  $E_{acc} = 10.4 \text{ MV/m}$  has been achieved.

### Introduction

Superconducting rf - cavities have in recent years shown significant improvements in their performance and several large scale applications are now under consideration<sup>1</sup>.

Nevertheless, the transfer of the technology from a laboratory scale to a large scale application as in an accelerator in a way, which avoids any degradation in performance of the cavities has not yet been fully demonstrated. The conditions of assembly of cavity units into cryostats are often more demanding than in a laboratory environment and challenge the sensitivity of the niobium rf - surface to long periods of exposure to atmosphere, to cleanliness and to accidental debris generation, which might result in Q - or field degradations or increased electron loading in these devices.

By hermetically sealing the cavities and keeping the inner surfaces under vacuum, one can avoid both multiple exposures and minimize the risk of contaminating the cavity during these operations.

### Sealed cavity concept

The experiments developing the sealed cavity concept have been carried out in two steps. In a first step a single 5 - cell elliptical, Cornell - type L - band cavity<sup>2</sup> is used and in a second step the concept is investigated with a cavity pair, which will eventually be the building bloc of the CEBAF accelerator<sup>4</sup>.

### Single 5 - cell cavity tests

Figure 1 shows the test set - up for the single 5 - cell cavity tests. The cavity is at both beam - pipe ends equipped with viton O - ring sealed gate valves, which in connection with an indium sealed Kapton rf -

window in the fundamental power coupler waveguide hermetically seal the cavity and allow its evacuation at room temperature. This is a highly desirable feature, because it allows after a cryogenic test, during which the gate valves are open and the cavity is continuously pumped via an ion getter pump, the detachment of the cavity from the test set - up without exposing the interior cavity surface to any gas at atmospheric pressure. The cavity can then further be handled for subsequent tests.

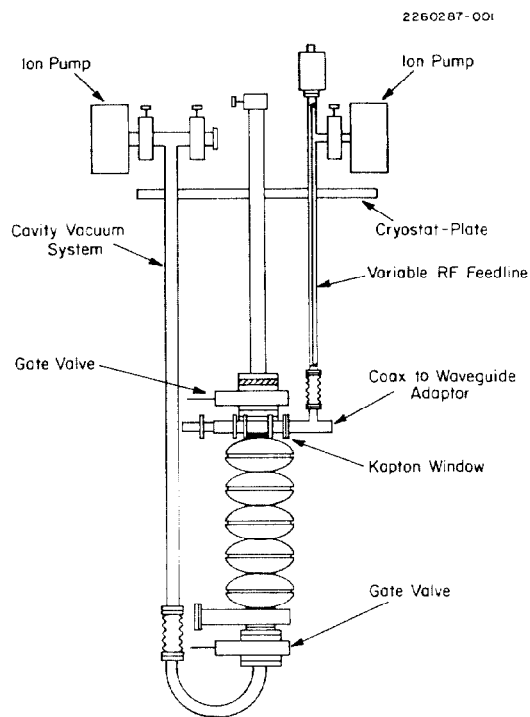


Figure 1: Experimental Test Set - up for 5 - Cell Cavity Test

The excitation of the rf - fields in the cavity is accomplished by means of a variable coaxial rf - feedline connected to a waveguide - to - coax - transition piece attached to the fundamental coupler of the cavity ( detail of assembly in figure 2 ). The coupling hole is located at a distance of 128 mm from the beam line in a field of about 30% of the field maximum on center<sup>3</sup>, which permits a comfortable variation of the external Q - value between  $3 \times 10^9$  and  $6 \times 10^{10}$  by moving the feedline in the cut - off tube of figure 2. 5 - cell cavity LE 5 - 4, which was last used in the Cornell beam - test<sup>5</sup>, was chosen for this experiment. In the beam - test the cavity exhibited a Q - value of  $Q = 1.6 \times 10^9$  and break - down occurred at an accelerating gradient of  $E_{acc} = 6.5 \text{ MV/m}$ .

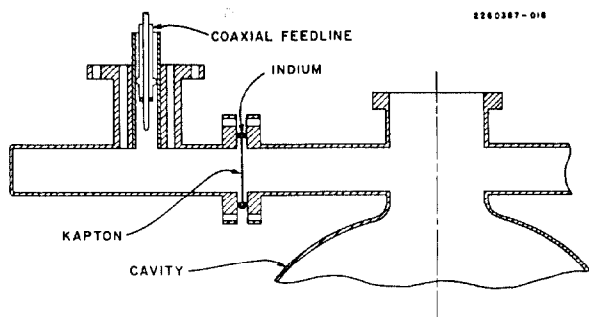


Figure 2 : Detail of Coax - to - Waveguide Assembly

Prior to the gate valve test the external  $Q$  - value of the fundamental power coupler was adjusted from

120 000 to  $1.1 \times 10^6$  and the field profile on axis was adjusted to be flat within 3 % .

The cavity was first retested after 30 sec of buffered chemical polishing and assembly in the clean room with the Kapton rf - window and the coax - to - waveguide adaptor attached . The Kapton film ( Type "H" , 5 mil thickness ) had been baked for 12 hrs at a temperature

of  $150^{\circ}\text{C}$  in a vacuum of about  $10^{-6}$  torr . At the end of the baking cycle the vacuum in the baking system had improved by at least one order of magnitude .

Unfortunately , when attempting to install the assembled cavity to the test stand , we encountered mechanical problems with the fit - up of the cut - off tube in the coax - to - waveguide adaptor and the outer conductor of the feedline . This required additional machining of the niobium tube . Therefore the cavity had to be placed back in the clean room , the Kapton window/waveguide assembly was removed , the cavity was filled with methanol and left in the clean room for 12 hrs . A freshly baked Kapton window was assembled to the coax - to - waveguide transition before being attached to the cavity .

Even though the Kapton foil was exposed for less than 3 hrs to room air - after the baking Kapton is quite hydrolytic - it took several days to achieve a vacuum in the low  $10^{-7}$  torr range both inside the cavity and the rf - feedline at room temperature .

The results of this test are listed in table 1 .

TEST #/ T [K]	$Q_0$ (LOW FIELD)	$Q_0$ (AT BD)	$E_{\text{ACC}}$ [MV/m]	SURFACE TREATMENT	COMMENTS
1 / 1.9	$8 \times 10^9$	$5.8 \times 10^9$	6.4	30 SEC BCP	KAPTON WINDOW + COAX-WAVEGUIDE TRANSITION
2				DISASSEMBLY METHANOL RINSE	GATE VALVES ATTACHED FEEDLINE PROBLEMS
3 / 2.0	$5.6 \times 10^9$	$3 \times 10^9$	6.6	CAVITY VACUUM MAINTAINED	DISASSEMBLY FROM TEST STAND, GATE VALVE 6x CYCLED
4 / 2.0	$5.6 \times 10^9$	$1.8 \times 10^9$	6.7	CAVITY VACUUM MAINTAINED	GATE VALVES 10x CYCLED ON TEST STAND

Table 1 : Summary of Test Results on 5 - Cell Cavity

At 2 K a  $Q$  - value of  $7.5 \times 10^9$  was measured and the field level could continuously be raised to the break down level of  $E_{\text{acc}} = 6.4 \text{ MV/m}$  except for a

very light multipacting level around  $4.2 \text{ MV/m}$  , which processed rapidly within 2 min . No field emission loading was observed .

The Kapton window itself does not seem to have introduced additional losses in the high  $Q$  system .

In preparation for the subsequent test with the gate valves the cavity as well as the coupling system was slowly let up to nitrogen gas through a  $0.2 \mu\text{m}$  filter . The cavity was detached from the test stand and the indium sealed adaptor pieces were disassembled from the cavity in the clean room . During this operation it was made sure that always the pieces to be detached were located below the cavity to avoid accidental debris deposition in the cavity . After the removal of the indium gaskets from the flanges the cavity was carefully rinsed in methanol and any immersion of the Kapton foil into the methanol was avoided . The gate valve subassemblies , which had been ultrasonically cleaned in methanol , were attached to the cavity as shown in figure 1 and subsequently the cavity was mounted to the test stand . The upper gate valve was blanked off as indicated in figure 1 . Cavity and feedline system were evacuated separately . Even after several days of pumping the cavity vacuum did not improve significant -

ly and remained in the high  $10^{-7}$  torr range - about a factor of 10 worse than usually . This behaviour is probably caused in part by outgassing of the viton O - rings in the gate valves exposed for a short time to methanol <sup>6</sup> .

Because of a short in the feedline , the cavity had to be warmed up again after initial cool - down ; the gate valves were closed after the gate mechanism had been exercised 6 times and the cavity was detached from the test stand . After the feedline problems had been corrected , the cavity was reattached and test # 3 as indicated in table 1 was carried out . In a forth test the cavity remained on the test stand after warm up and both gate valves were completely closed and opened 10 times . With the gate valves closed for more than 1 hour the vacuum in the cavity did not degrade .

Up to a gradient of  $E_{\text{acc}} = 4$  to  $5 \text{ MV/m}$  the  $Q$  - value was nearly independent of field level . Above  $5 \text{ MV/m}$  field emission loading was observed , which was in test # 4 significantly reduced within 30 min of rf - processing . In addition , the break - down field level increased to  $7.4 \text{ MV/m}$  indicating that the quench might have been initiated by field emission .

#### Cavity pair test

To further investigate the feasibility of the sealed cavity concept in a more complex system , we have assembled two 5 - cell cavities - Cornell cavity LE 5 - 5 and Cornell type cavity Dornier I manufactured by Dornier Company - to a cavity pair as shown in figure 3 .

5 - 5 had been used in the Cornell beam test and LE exhibited a field of only  $2.4 \text{ MV/m}$  ; the low break - down field was probably caused by debris deposition during installation into the CESR storage ring .

This cavity was recovered to a field level of  $E_{\text{acc}} = 11.9 \text{ MV/m}$  just by rinsing the surface with methanol - a further indication of contamination . Cavity Dornier I had originally an accelerating gradient of  $E_{\text{acc}} = 7.9 \text{ MV/m}$  and a resonant frequency ,

which was 15 MHz too low . By solid state gettering in the presence of  $\text{Ti}^7$  at  $1300^{\circ}\text{C}$  the interstitial

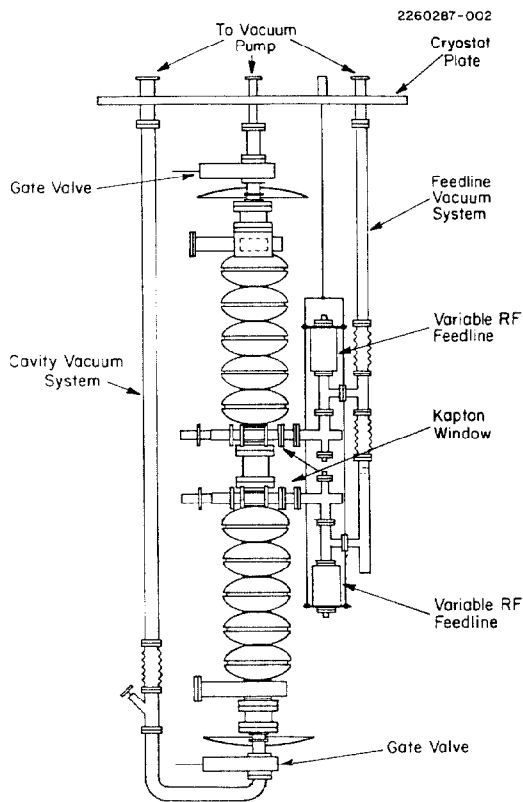


Figure 3 : Cavity Pair Test Set - Up

impurities in the niobium were partially removed resulting in a softer material with higher thermal conductivity. After tuning the cavity to the right frequency and surface preparation by buffered chemical polishing the cavity exhibited in a subsequent test an accelerating gradient of  $E_{acc} = 10.4$  MV/m. No

quench was observed as in the original test, but the achievable gradient was limited by a high level of field emission loading.

After buffered chemical polishing for 1 min both cavities were assembled in the clean room into a pair and then transferred to the test set - up. Cavity and feedline system were simultaneously evacuated by means of a turbomolecular pump before being switched to separate ion getter pumps. After several days of pumping the vacua did not improve beyond  $10^{-6}$  torr. Test results are shown in figure 4.

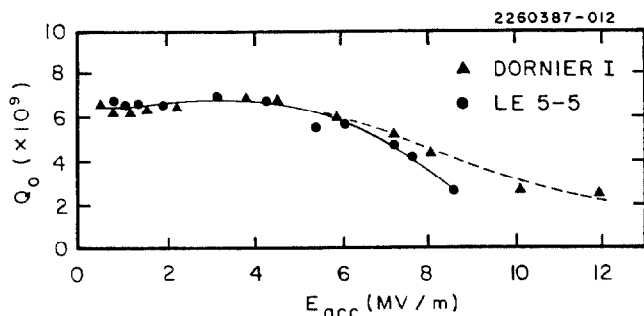


Figure 4 : Test Results on Cavity Pair

Both cavities had a  $Q$  - value of  $Q = 6.5 \times 10^9$  at 2 K and at low field levels. In both cavities some multipacting was observed, which processed in less than 30 min and allowed the field levels to be raised continuously. In cavity LE 5 - 5 - this cavity was mounted below cavity Dornier I and probably absorbed most of the residual gas in the assembly on its surface when cooled down first - a field level of  $E_{acc} = 8.9$  MV/m was reached before strong field emission loading prevented a further increase in gradient. No break - down was observed as was also the case with Dornier I, in which the gradient could be raised up to  $E_{acc} = 11.9$  MV/m, before limitation by field emission loading was setting in. At this field level the  $Q$  - value had dropped to  $Q = 2.4 \times 10^9$ .

### Conclusion

The experiments demonstrate the feasibility of the sealed cavity concept, even though in some of the tests a somewhat increased level of field emission loading has been observed. It is conceivable that this behaviour is partially caused by the mediocre room temperature vacuum in the cavity due to out - gassing of the viton O - rings in the gate valves and by poorly vented O - ring grooves in the present design. Improved pre - baking or the selection of a different O - ring material as well as the proper groove design should correct this problem. The experiments indicate that very likely degradations in cavity performance can be avoided. This sealed cavity concept will be implemented in the CEBAF accelerator. With a 1 m long cavity pair, which will be the building bloc of this accelerator, an average accelerating gradient of  $E_{acc} = 10.4$  MV/m has been obtained, a value, which is well above the design value of  $E_{acc} = 5$  MV/m.

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