© 1983 IEEE. Personal use of this material is permitted. However, permission to reprint/republish this material for advertising or promotional purposes or for creating new collective works for resale or redistribution to servers or lists, or to reuse any copyrighted component of this work in other works must be obtained from the IEEE.

IEEE Transactions on Nuclear Science, Vol. NS-30, No. 4, August 1983

EXPERIMENTAL COMPARISON OF BEAM EXCITED MODES IN BIPERIODIC STRUCTURES

K.C.D. Chan, H. Euteneuer*, J.-P. Labrie and J. McKeown

Atomic Energy of Canada Limited, Research Company Chalk River Nuclear Laboratories Chalk River, Ontario, Canada KOJ 1JO

Summary

An experiment to study excitations of higher order modes in a coaxial coupled structure and an onaxis coupled structure is in progress. The tuning and assembly of these structures is complete. Calculations have shown that a coaxial coupled structure is 5% less sensitive to beam excitation of its axially symmetric modes than an on-axis coupled structure. Low power tests have identified mode frequencies above the accelerating mode passband showing that higher order modes propagate in an on-axis coupled structure and not in a coaxial coupled structure. High power beam tests are scheduled for later this year.

Introduction

Excitations of higher order modes in accelerating structures are important in considering beam loading, beam energy loss and beam breakup¹,². These excitations are being studied in an on-axis coupled structure and a coaxial coupled structure in order to obtain information on efficiency and beam stability, information that could lead to a preferred biperiodic structure for applications in storage rings and microtrons. The on-axis coupled structure was chosen because it has been used in the University of Mainz microtron² and the Electron Test Accelerator (ETA)³ at the Chalk River Nuclear Laboratories (CRNL). The coaxial coupled structure was chosen because recently reported work showed promising results in reducing beam breakup effects⁴. The fundamental modes of these structures are the $\pi/2$ modes of the TM₀₁₀ passbands.

In the proposed beam tests, the structures will be initially studied with a low duty cycle pulsed beam (4 MeV electrons from ETA) that has high enough charge per bunch (10^{11} electrons) to provide sufficient single bunch excitation in the rf cavities. This allows the energy loss parameters to be measured without the complication of an enhancement effect from closely spaced multiple bunches. The structures will then be studied with a cw beam from ETA. With their fundamental frequencies chosen to be the third harmonic of the ETA frequency (804.78 MHz) and with their TM₁₁₀-like mode frequencies at approximately 1.7 times that of the fundamental frequencies, the frequencies of the ${\rm TM}_{110}$ modes are in the vicinity of the fifth harmonic of the ETA frequency. This choice of frequencies provides an opportunity of resonantly exciting both the fundamental and the $\rm TM_{110}\mbox{-}like$ modes and, as a consequence, of studying the exci-tation of the fundamental mode and a typical beam breakup mode with enhanced sensitivities.

For simple cavity geometries, energy loss parameters and excitation levels of higher order modes can be calculated with computer programs like BCI⁵ and $100E^6$. Results from the proposed beam tests when compared to these calculations can provide insight to the beam excitation process and validation for the computer programs.

This experiment is now in progress. The results of low power tests of structures and results from

calculations are reported in this paper. High power beam tests are scheduled for later this year.

Calculation Method

The beam energy loss and excitation levels of higher order modes can be well described if the energy loss parameters of the cavities are known. The energy loss parameter is defined as the proportionality constant between the energy lost by a single bunch to an empty cavity and the square of the total bunch charge.

The total energy loss to exciting the axially symmetric modes can be calculated using the computer code BCI^5 . This code computes the induced axially symmetric electromagnetic fields, when a charge bunch traverses a cavity, by numerically integrating Maxwell's equations in the time domain. Another code, TBCI⁷, which calculates the nonaxially symmetric electromagnetic fields has recently become available. With this code, the total energy loss parameter for the non-axially symmetric modes can be similarly calculated.

The above codes do not provide the energy loss in individual modes of the structure. The energy loss $p_m^{2}U_m$ of a single bunch to the mth mode is calculated with data from low power tests and by integrating the following differential equation:

$$\frac{d^2 p_m}{dt^2} + \frac{\omega_m}{Q_m} \frac{d p_m}{dt} + \omega_m^2 p_m \approx \frac{\omega_m}{2U_m} \int \vec{J} \cdot \vec{E}_m d^3 r$$

where p_{ff} = eigenmode expansion coefficients

 $\omega_m = \text{mode frequency}$ $E_m = \text{mode electric field}$ J = beam current density $Q_m = \text{mode quality factor}$ $U_m = \text{mode stored energy} = 1/2 \epsilon_0 \int \vec{F}_m \cdot \vec{E}_m d^3 r$

This equation is a modified version of the well known formula by Condon⁹ that expands the vector potential in terms of eigenmodes using coefficients p_m . In this equation, the vector potential, \overline{A}_m , is replaced by the electric field, \overline{E}_m , using the fact that they are simply related in the Coulomb Gauge, i.e., $\overline{E}_m = (1/c)(\partial \overline{A}_m/\partial t)$ for $\nabla\cdot\overline{A}_m = 0$. The integration of the above differential equation with values for ω_m , Q, U_m and \overline{E}_m obtained from low power tests is performed with a computer program, MODE, developed at CRNL.

To calculate the excitations in the cw case, the induced fields of the single bunch are multiplied by the resonance function F to account for the contributions from multiple bunches. The resonance function is given by:

$$F = F_R + jF_I \qquad \phi = \tan^{-1}(F_I/F_R)$$

$$F_R = \frac{1 - e^{-2T}}{2(1 - 2e^{-T}\cos \delta + e^{-2T})}$$

Summer visitor from University of Mainz.

$$F_{I} = \frac{e^{-2T} \sin \delta}{2(1-2e^{-T} \cos \delta + e^{-2T})}$$

here $\delta = 2\pi (f_{m} - f_{b})/f_{b}$ f_{m} = mode frequency
 $T = (f_{m}/f_{b})(\pi/Q)$ f_{b} = beam frequency

The cw synchronous field will be |F| times that of the single bunch value in magnitude and at a phase lag $_{\varphi}$ referring to the phase of the beam bunch.

Experimental Setup

A schematic of the experimental arrangement for testing beam excitations in rf structures is shown in Fig. 1. ETA will deliver electrons in cw or pulsed mode at energies between 1.5 MeV to 4 MeV. The beam will traverse the two structures at displacements from the structure axis controlled by steering magnets and measured by beam position monitors.

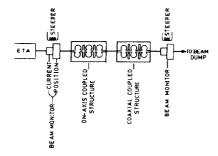


Fig. 1. Experimental arrangement.

ŧ

The ETA pulsed electron gun is presently being commissioned. It is similar to the Collider Injector Gun employed on the Stanford Linear Collider⁹. It can produce electron pulses of 5 ns length which contain up to 10^{11} electrons (5 A peak current). Cavity excitation from this gun operating at low duty cycle (5 kHz) can be considered as that from a single bunch, and the energy loss parameters can be extracted without considering cw enhancement.

The ETA cw electron gun can provide accelerated currents up to 20 mA. With the energy loss parameters obtained from the pulsed beam and the measured excitations with the cw beam, the enhancement factors in cw operation can be determined.

Accelerating Structures and Low Power Testing

The structures have been tuned and assembled (Fig. 2). Dimensions for the unit cells are shown in Fig. 3. Table 1 lists the rf parameters for the copper structures made up of 3 accelerating cells and 2 coupling cells.

Table 1. Summary of parameters of the on-axis and coaxial structures.

	On-axis	Coaxial
<pre>#/2 Mode Frequency (MHz)</pre>	2415.0	2415.0
Q, Quality Factor	15800	18000
First Neighbour Coupling	38	2.4%
Stopband (kHz)	60	2150
Estimated ZT ² (MiJ/m)	74	74

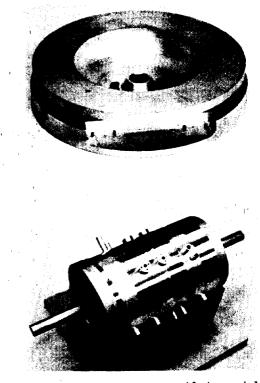


Fig. 2. A half cell and the assembled coaxial coupled structure.

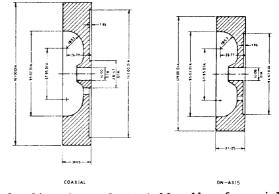


Fig. 3. Dimensions of the half cells of coaxial and on-axis coupled structures. All dimensions are in mm.

Low power testing of the structures is underway. Table 2 lists the mode frequencies in the coaxial and on-axis coupled structures measured to the TM_{110} passband. The assignments of structure and cavity modes are tentative. Cavity mode is assigned if the mode is excited in one cavity and the excitation is not detected by probe insertion in other cavities. Data show that the higher order modes in the coaxial coupled structure, unlike those in the on-axis coupled structure, do not propagate because the coaxial coupled structure and the accelerating cavities have relatively different frequency spectra.

Results of Calculations

Beam bunches were assumed to be Gaussian with σ_{TMS} 's of 0.0155 m or 15°. An average current of 2 mA was assumed for the cw beam and total charge of 1.6 x 10^{-8} C per pulse for the pulsed beam.

3646

On-Axis		Coaxial		Mode Assignment
Frequency	Q	Frequency	Q	
2374 2391 2415 2439 2457	5300 4700 15800 4700 6200	2391 2401 2415 2431 2442	5100 5500 18000 6800 5100	™ ₀₁₀ structure passband
		2733 2737	3500	TM ₁₁₀ coupling cavity mode
		3408	3600	TM ₂₁₀ coupling cavity mode
3908 3912 3914 3933 3942	9600 9500 9100 9200 9200			TE ₁₁₁ structure passband
		3966 3973	16000	TE ₁₁₁ accelerating cavity mode
4033 4035 4046 4047 4047	~ 600 0			TM OL1 structure passband
		4117 4118	20300	${\rm TM}_{110}$ accelerating cavity mode
4123.1 4124.6 4125 4125.3 4127.4 4132.5 4134.7 4135.4 4139.7 4139.7	18000 20000 18000 17000 5000 5000 16000 5000 5000 5000			^{IM} 110 Structure passband

Table 2. Modes observed between frequencies 2300 and 4200 MHz for the on-axis and coaxial structures. The mode assignments are tentative.

The energy loss parameter calculated by MODE for the $\pi/2$ mode was $1.73 \ V \cdot pC^{-1}$ for the entire structure (i.e., $9.44 \ V \cdot pC^{-1} \cdot m^{-1}$ which is in agreement with the fields calculated by SUPER-FISH10. The synchronous field induced by the cw beam was 70 kV·m⁻¹ and the maximum field by the pulsed beam was 300 kV·m⁻¹. The resonance function calculated for the cw beam was 1500 by using a Q value of 14200 and resonant excitation at the third harmonic of the beam frequency. Energy loss parameters for 0 and π modes were only 3.91×10^{-3} and $1.11 \times 10^{-3} \ V \cdot pC^{-1}$ for the entire structure. They are small compared to that of the $\pi/2$ mode because of the effects of transit time factors and field level differences in various cells in the structure. These results are applicable to both the coaxial and on-axis coupled structures because the differences calculated with SUPERFISH¹⁰ are approximately 5%, which is comparable to the error of the bead pull data used.

The total energy loss parameter of all axially symmetric modes for the on-axis coupled structure was calculated to be 2.04 V·pC⁻¹ over the entire structure with the computer code BCI. The parameter calculated for the coaxial coupled structure was 5% lower. Since the energy loss parameter for the $\pi/2$ mode is 1.73 V·pC⁻¹, it accounts for more than 80% of the beam bunch excitations of the axially symmetric modes.

The excitation of the $\rm TM_{110}$ mode was estimated for a shaped cavity by using MODE and fields of an equivalent cylindrical cavity. The energy loss parameter was found to be one order of magnitude smaller than that of the $\pi/2$ mode when the beam traversed the cavity 4.7 mm off axis.

The magnitude and phase of the resonance function, F, for the TM_{110} mode excitation by the fifth harmonic of the ETA beam are shown in Fig. 4, indicating that the TM_{110} mode frequency has to be within 10 MHz of the fifth harmonic of beam frequency to obtain significant enhancement. This condition can be satisfied during future beam experiments by either adjusting the beam frequency or adjusting the mode frequency by means of the temperature of the water in the cooling channel. The latter has a sensitivity of \sim 70 kHz/°C.

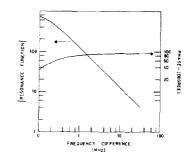


Fig. 4. The magnitude of the resonance function and its phase with respect to the beam is shown as a function of the frequency difference between the TM_{110} -like mode frequency and the frequency of the fifth harmonic.

Acknowledgement

This work is partly supported by the Nuclear Physics Laboratory of the University of Illinois at Urbana-Campaign, USA.

References

- R.H. Helm and G.A. Loew, "Beam Breakup" in Linear Accelerators, eds., P.M. Lapostolle and A.L. Septier, North Holland Publ. Co., Amsterdam, (1970) 173.
- H. Herminghaus and H. Euteneuer, "Beam Blowup in Race Track Microtron", Nucl. Inst. Meth. <u>163</u> (1979) 299-308.
- J. McKeown, R.T.F. Bird, K.C.D. Chan, S.H. Kidner and J.-P. Labrie, "High Power, On-Axis Coupled Linac Structure", Proc. 1981 Linac Conf., Los Alamos Laboratory Report No. LA-9234-C, 334.
- J.-P. Labrie and J. McKeown, "The Coaxial Coupled Linac Structure", Nucl. Inst. Meth. 193 (1982) 437-444.
- T. Weiland, "On the Computation of Electromagnetic Fields Excited by Relativistic Bunches of Charged Particles in Accelerating Structures", CERN Laboratory Report No. CERN/ISR-TH/80-07 (1980).
- 6. K.C.D. Chan, Internal CRNL report, to be published.
- T. Weiland, "TBCI and URMEL New Computer Codes for Wake Field and Cavity Mode Calculations", proceedings of this conference.
- E.V. Condon, "Forced Oscillations in Cavity Resonators", J. Appl. Phys. <u>12</u> (1941) 129.
- R.F. Koontz, "CID Thermionic Gun System", Proc. 1981 Linac Conf., Los Alamos Laboratory Report No. LA-9234-C, 62.
- K. Halbach and R.F. Holsinger, "SUPERFISH, A Computer Program for Evaluation of rf Cavities with Cylindrical Asymmetry", Particle Accelerators <u>7</u> (1976) 213.