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Summary and Introduction

In a large synchrotron or a storage ring, the random closed orbit distortions are generally large. When combined with the sextupole magnets for chromaticity correction, they produce linear stopbands because effective gradient errors appear. Further, the vertical closed orbit distortion produces a vertical dispersion because there appears a vertical bend in the quadrupole and sextupole magnets. These effects are studied by an analytical method.

It is shown that the tune  $\nu$ , which is close to  $\nu = mNs$  and  $3\nu = mNs$  (where  $Ns$  is the number of super-periods and  $m$  is an arbitrary integer) should be avoided to have a small stopband width. In order to have a small vertical dispersion, the tune close to  $2\nu = mNs$  should be avoided. The present theory also indicates a preferable method of chromaticity correction to avoid an excessive vertical dispersion. The effect of closed orbit correction is not considered in this paper.

Equation of Motion

The Hamiltonian of particle motion in a machine with sextupole magnets, a momentum error  $\Delta p/p$  and horizontal and vertical kick errors  $\theta_{xi}$  and  $\theta_{yi}$  is given as<sup>1,2)</sup>

$$\begin{aligned}
 H &= H_0 + V \\
 H_0 &= \frac{1}{2}(p_x^2 + p_y^2) + \frac{1}{2}K(x^2 - y^2) \\
 V &= \sum_{i=1}^M \theta_{xi} \delta(z-z_i) (1 - \frac{\Delta p}{p}) x - \frac{1}{\rho} \frac{\Delta p}{p} x \\
 &\quad - \sum_{i=1}^M \theta_{yi} \delta(z-z_i) (1 - \frac{\Delta p}{p}) y \\
 &\quad - \frac{1}{2} K \frac{\Delta p}{p} (x^2 - y^2) + \frac{1}{6} K' (1 - \frac{\Delta p}{p}) (x^3 - 3xy^2),
 \end{aligned} \tag{1}$$

where

$$\begin{aligned}
 K &= \frac{1}{B\rho} \frac{\partial B}{\partial x} \\
 K' &= \frac{1}{B\rho} \frac{\partial^2 B}{\partial x^2}
 \end{aligned}$$

- $x$  = horizontal deviation
- $y$  = vertical deviation
- $z$  = orbit length (independent variable)
- $p_x, p_y$  = canonical momentum
- $z_i$  = orbit position of a kick
- $M$  = number of kick elements

The kicks  $\theta_{xi}$  and  $\theta_{yi}$  are given by

$$\theta_{xi} = \frac{\Delta B}{B\rho} \frac{\ell_i}{y_i}, \quad \theta_{yi} = \frac{\Delta B}{B\rho} \frac{\ell_i}{x_i}, \tag{2}$$

where  $\Delta B$  denotes a random field error and  $\ell_i$  is the length of the kick element. We assumed a thin lens ( $\delta$ -function) for a kick.

The closed orbits (including dispersion functions)  $x_{eq}$  and  $y_{eq}$  are periodic solutions of the Hamiltonian equations and thus are described by the equations

$$\begin{aligned}
 x_{eq}'' + Kx_{eq} &= \frac{1}{\rho} \frac{\Delta p}{p} - \sum_{i=1}^M \theta_{xi} \delta(z-z_i) (1 - \frac{\Delta p}{p}) \\
 &\quad + K \frac{\Delta p}{p} x_{eq} - \frac{1}{2} K' (1 - \frac{\Delta p}{p}) (x_{eq}^2 - y_{eq}^2), \tag{3}
 \end{aligned}$$

$$\begin{aligned}
 y_{eq}'' - Ky_{eq} &= \sum_{i=1}^M \theta_{yi} \delta(z-z_i) (1 - \frac{\Delta p}{p}) \\
 &\quad - K \frac{\Delta p}{p} y_{eq} + K' (1 - \frac{\Delta p}{p}) x_{eq} y_{eq}, \tag{4}
 \end{aligned}$$

where primes on  $x_{eq}$  and  $y_{eq}$  denote differentiation with respect to  $z$ .

Further simplification can be made by putting

$$\begin{aligned}
 x_{eq} &= x_{co} + \eta_x \frac{\Delta p}{p}, \\
 y_{eq} &= y_{co} + \eta_y \frac{\Delta p}{p},
 \end{aligned} \tag{5}$$

where "co" denotes random closed orbit distortions and  $\eta_x$  and  $\eta_y$  are horizontal and vertical dispersions. Keeping terms of zeroth and first orders in  $\Delta p/p$ , neglecting nonlinear terms and assuming that  $\eta_y \ll \eta_x$  and  $\eta_x$  is given by the  $1/\rho$  term in eq.(3), we obtain

$$y_{co}'' - Ky_{co} = \sum_{i=1}^M \theta_{yi} \delta(z-z_i) \tag{6}$$

$$\eta_y'' - K\eta_y = \sum_{i=1}^M \theta_{yi} \delta(z-z_i) - (K-K'\eta_x)y_{co}. \tag{7}$$

Eq.(6) is well-known<sup>3)</sup> and eq.(7) has been derived by several authors.<sup>4,5)</sup>

We then consider a betatron oscillation around the closed orbits  $x_{eq}$  and  $y_{eq}$ . By putting

$$x = x_{eq} + u, \quad y = y_{eq} + v, \tag{8}$$

where  $u$  and  $v$  denote the amplitudes of betatron oscillation, the perturbation Hamiltonian  $V$  is transformed to<sup>1)</sup>

$$\begin{aligned}
 V &= \frac{1}{2} \frac{\Delta p}{p} K(u^2 - v^2) - \frac{1}{2} K' x_{eq} (1 - \frac{\Delta p}{p}) (u^2 - v^2) \\
 &\quad + K' y_{eq} (1 - \frac{\Delta p}{p}) uv, \tag{9}
 \end{aligned}$$

where we have neglected nonlinear terms since we consider only linear stopbands.

### Vertical Dispersion

Solutions of eqs. (6) and (7) are given in terms of Fourier series<sup>2)</sup>

$$y_{co} = \sqrt{\beta_y} \sum_{k=-\infty}^{\infty} \frac{v^2 f_k}{v^2 - k^2} e^{ik\phi_y} \quad (10)$$

with

$$f_k = \frac{1}{2\pi v_y} \sum_{i=1}^M \beta_{yi}^{1/2} \theta_{yi} e^{-ik\phi_{yi}} \quad (11)$$

and

$$\eta_y = \sqrt{\beta_y} \sum_{n=-\infty}^{\infty} \frac{v^2 f_n e^{in\phi_y}}{v^2 - n^2} - \frac{\sqrt{\beta_y}}{2\pi} \sum_{k,n=-\infty}^{\infty} \frac{v^3 f_k J_{n-k}}{(v^2 - k^2)(v^2 - n^2)} e^{in\phi_y} \quad (12)$$

with

$$J_m = \int_0^c \beta_y (K - K' \eta_x) e^{-im\phi_y} dz. \quad (13)$$

Notations are familiar ones of Courant and Snyder.<sup>3)</sup> The first term in eq.(12) is equal to  $y_{co}$  and small. The function  $J_m$  is related to  $\Delta\beta/\beta$  and chromaticity in the way

$$\frac{(\Delta\beta/\beta)_y}{\Delta p/p} = \frac{v_y}{4\pi} \sum_{m=-\infty}^{\infty} \frac{J_m e^{im\phi}}{v^2 - (m/2)^2} \quad (14)$$

$$\frac{\Delta v_y}{\Delta p/p} = \frac{1}{4\pi} J_0. \quad (15)$$

Looking at eq.(12), we see that the largest contribution to  $\eta_y$  comes from the terms  $n \sim \pm v$  and  $k \sim \pm v$ . Since  $n v k$  should be an integer multiple of superperiodicity  $N_s$ , we see that the tune around  $2v_y$  ( $N n$  ( $n =$  arbitrary integer) should be avoided to have a small vertical dispersion. Even then, the largest contribution to  $\eta_y$  comes from  $J_0$  and  $J_m$  where  $m \sim \pm 2v$ . Thus, it is important in chromaticity correction to make these terms small. It is to be noted here that Close et al.<sup>6)</sup> has pointed out by a computational method that the vertical dispersion at the half-integral structure resonance described above is rather easily corrected by closed orbit correction.

Horizontal dispersion is also affected by random closed orbit distortions. The additional horizontal dispersion  $\Delta\eta_x$  is given in a similar way by

$$\Delta\eta_x = \sqrt{\beta_x} \sum_{n=-\infty}^{\infty} \frac{v^2 f_n}{v^2 - n^2} e^{in\phi_x} + \frac{\sqrt{\beta_x}}{2\pi} \sum_{n,k=-\infty}^{\infty} \frac{v^3 f_k J_{n-k}^x}{(v^2 - k^2)(v^2 - n^2)} e^{in\phi_x} \quad (16)$$

with

$$f_k^x = \frac{1}{2\pi v_x} \sum_{i=1}^M \beta_{xi}^{1/2} \theta_{xi} e^{-ik\phi_{xi}} \quad (17)$$

$$J_m^x = \int_0^c \beta_x (K - K' \eta_x) e^{-im\phi_x} dz. \quad (18)$$

### Half-Integral Resonance

As seen from the Hamiltonian (9), the horizontal closed orbit distortion gives rise to half-integral

resonance and the effective gradient error is equal to  $-K' x_{eq}$ . We consider a case for a right momentum or  $\Delta p/p \ll 0$ . The stopband width for half-integral resonance is given by<sup>3)</sup>

$$\delta v_{x,y} = \frac{1}{2\pi} \left| \int_0^c \beta_{x,y} x_{eq} K' \exp(ip\phi_{x,y}) dz \right| \quad (19)$$

for  $v \sim p/2$  ( $p$ : integer).

The rms estimate is expressed as

$$(\delta v_{x,y})_{rms}^2 = \frac{1}{4\pi^2} \int_0^c dz \int_0^c dz' \beta_{x,y}(z) \beta_{x,y}(z') K'(z) K'(z') \overline{\beta_x(z) \beta_x(z')} \overline{H(z) H(z')} \cos p(\phi - \phi'), \quad (20)$$

where we put

$$x_{eq} = \sqrt{\beta_x} H. \quad (21)$$

To proceed further, we should evaluate the function  $\overline{H(z) H(z')}$ . If we assume a thin lens for a kick  $\theta_i$ ,  $H(\phi)$  is expressed as

$$H(\phi) = \frac{1}{2\sin\pi v} \left[ \sum_{i=1}^M \beta_i^{1/2} \theta_i \cos v(\pi + \phi - \psi_i) + 2\sin\pi v \sum_{i=1}^M \beta_i^{1/2} \theta_i \sin v(\phi - \psi_i) \right], \quad (22)$$

where  $M$  is the total number of kick elements and  $M(\phi)$  is the number of kick elements located at the azimuthal points from 0 to  $\phi$ .

We now assume that the kicks  $\theta_i$ 's are "uncorrelated", i.e.  $\overline{\theta_i \theta_j} = \overline{\theta_i} \overline{\theta_j} \delta_{ij}$ , where the bar indicates an ensemble average. This assumption is reasonable when we consider random closed orbit distortions. When an orbit correction is taken into account, the corrector kick will be correlated in some way to the random kicks. We neglect this case in this paper. Then,

$$\overline{H(\phi) H(\phi')} = \frac{1}{4\sin^2\pi v} \left[ \sum_{i=1}^M \beta_i \overline{\theta_i^2} \cos v(\pi + \phi - \psi_i) \cos v(\pi + \phi' - \psi_i) + 2\sin\pi v \sum_{i=1}^M \beta_i \overline{\theta_i^2} \sin v(\phi - \psi_i) \cos v(\pi + \phi' - \psi_i) + 2\sin\pi v \sum_{i=1}^M \beta_i \overline{\theta_i^2} \sin v(\phi' - \psi_i) \cos(\pi + \phi - \psi_i) + 4\sin^2\pi v \sum_{i=1}^M \beta_i \overline{\theta_i^2} \sin v(\phi - \psi_i) \sin v(\phi' - \psi_i) \right], \quad (23)$$

where  $M(\phi, \phi')$  denotes the minimum of  $M(\phi)$  and  $M(\phi')$ .

Another form of  $\overline{H(\phi) H(\phi')}$  is obtained from the Fourier series form of closed orbit distortion given by eqs.(10) and (11). In this case,

$$\overline{H(\phi) H(\phi')} = \sum_{k,k'=-\infty}^{\infty} \frac{v^4 \overline{f_k f_{k'}}}{(v^2 - k^2)(v^2 - k'^2)} e^{ik\phi + ik'\phi'} \quad (24)$$

The ensemble mean  $\overline{f_k f_{k'}}$ , is given for "uncorrelated" thin lens kicks in the form

$$\overline{f_{k+k'}} = \frac{1}{4\pi^2 v^2} \sum_{i=1}^M \beta_i \theta_i^2 e^{-i(k+k')\psi_i} \quad (25)$$

$$= F_{k+k'}$$

If  $\overline{\theta_i^2}$  is equal to  $\overline{\theta^2}$  for all kicks, the function is non-zero only when  $k+k' = mN_s$  ( $m$ : arbitrary integer). We consider this case.

If we insert eq.(23) or (24) into eq.(20), we obtain the rms stopband width for half-integral resonance.

#### Linear Stopbands

We give the formulae<sup>7)</sup> of rms linear stopband widths and linear tune shifts. The expressions are given in terms of Fourier series because qualitative features of the present theory are more manifest. For half-integral resonance, the stopband widths are given as ( $v \sim p/2$ )

$$(\delta v_x)_{\text{rms}}^2 = \sum_{m,m'} B_m B_{m'} \frac{v^4 F_{(m+m')}}{\{v^2 - (p+m)^2\} \{v^2 - (p-m')^2\}}, \quad (26)$$

$$(\delta v_y)_{\text{rms}}^2 \approx \sum_{m,m'} B'_m B'_{m'} \frac{v^4 F_{(m+m')}}{\{v^2 - (p+m)^2\} \{v^2 - (p-m')^2\}}. \quad (27)$$

The linear tune shifts  $\Delta v_x$ ,  $\Delta v_y$  are given as

$$(\Delta v_x)_{\text{rms}}^2 = \frac{1}{4} \sum_{m,m'} B_m B_{m'} \frac{v^4 F_{(m+m')}}{\{v^2 - m^2\} \{v^2 - m'^2\}}, \quad (28)$$

$$(\Delta v_y)_{\text{rms}}^2 = \frac{1}{4} \sum_{m,m'} B'_m B'_{m'} \frac{v^4 F_{(m+m')}}{\{v^2 - m^2\} \{v^2 - m'^2\}}, \quad (29)$$

The stopband width for the sum resonance ( $v_x + v_y \sim p$ ) is given as

$$(\delta v_{\text{sum}})_{\text{rms}}^2 \approx \sum_{m,m'} B'_m B'_{m'} \frac{v^4 F'_{(m+m')}}{\{v^2 - (p+m)^2\} \{v^2 - (p-m')^2\}}, \quad (30)$$

The width for difference resonance ( $v_x - v_y \sim 0$ ) is

$$(\delta v_{\text{dif}})_{\text{rms}}^2 \approx \sum_{m,m'} B'_m B'_{m'} \frac{v^4 F'_{(m+m')}}{\{v^2 - m^2\} \{v^2 - m'^2\}}. \quad (31)$$

In the above formulae

$$B_m = \frac{1}{2\pi} \sum_i \beta_{xi}^{3/2} K'_i l_i \cos(m\phi_i)$$

$$B'_m = \frac{1}{2\pi} \sum_i \beta_{xi}^{1/2} \beta_{yi} K'_i l_i \cos(m\phi_i) \quad (32)$$

$$F_m = \frac{\overline{\theta^2}}{4\pi^2 v^2} \sum_i \beta_{xi} \cos(m\psi_{xi})$$

$$F'_m = \frac{\overline{\theta^2}}{4\pi^2 v^2} \sum_i \beta_{yi} \cos(m\psi_{yi}).$$

We have assumed that the lattice is symmetric and  $v_x = v_y = v$ .  $m, m'$  in the summation takes values which are integer multiples of  $N_s$ . Suffix  $x$  or  $y$  is attached to  $\phi_i$  depending on the case.

The stopband width for half-integral and sum resonances becomes large when  $v \sim \pm(m-p)$  and  $v \sim \pm(m'-p)$ . Since  $p \sim 2v$ , this condition is expressed as  $v = N_n$ ,  $3v = N_n$  ( $n$ : arbitrary integer). On the other hand, the tune shift and the stopband width for difference resonance become large only when  $v = N_n$ .

#### Conclusion

It is shown that the tunes,  $v \sim N_n$ ,  $2v \sim N_n$  and  $3v \sim N_n$ , are unfavorable because they give rise to a large dispersion or a large stopband width for linear resonances. These conditions are the same as those for integral, half-integral and third-integral resonances. We have considered linear resonances for  $\Delta p/p = 0$ , but we expect a similar resonance effect for  $\Delta p/p \neq 0$  due to the presence of  $\eta_y$  and  $\Delta\eta_x$ .

#### Acknowledgement

Most of this work has been done while the author was at CERN and SLAC. He wishes to thank the hospitality of these institutes. He wishes to thank A.W. Chao, E. Keil, M.J. Lee and P.L. Morton for helpful discussions and suggestions.

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