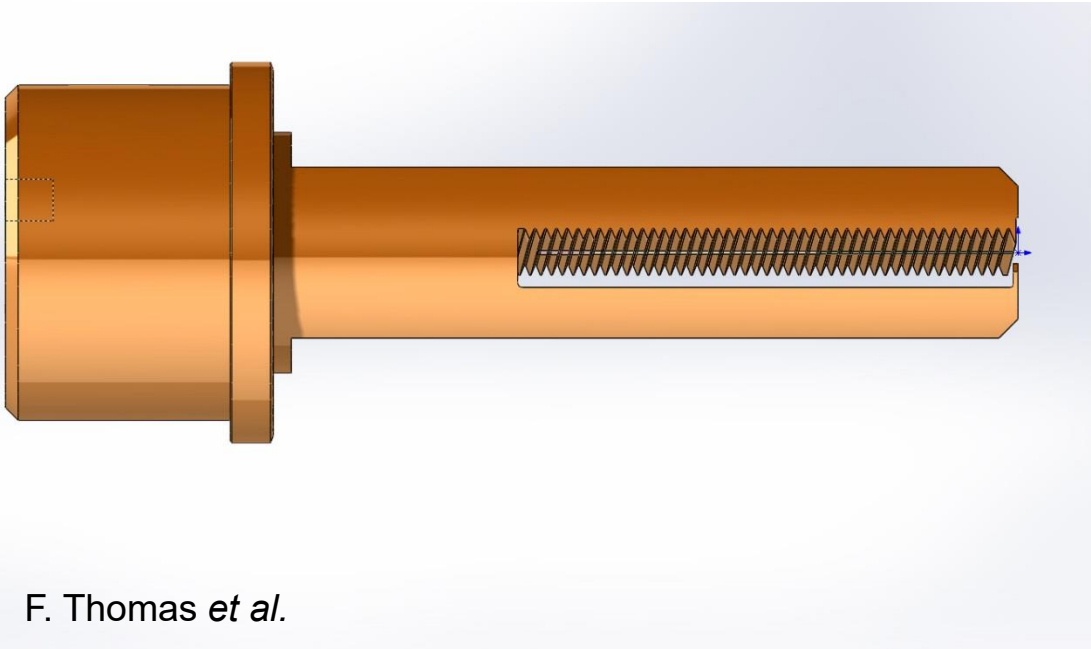


X-RAY Absorber Design and Calculations for the EBS Storage Ring

F. Thomas, Y. Dabin, P. Marion, E. Gagliardini,
D. Coulon, T. Ducoing, F. Ewald and J.C. Biasci



F. Thomas *et al.*



X-RAY Absorber Design and Calculations for the EBS Storage Ring

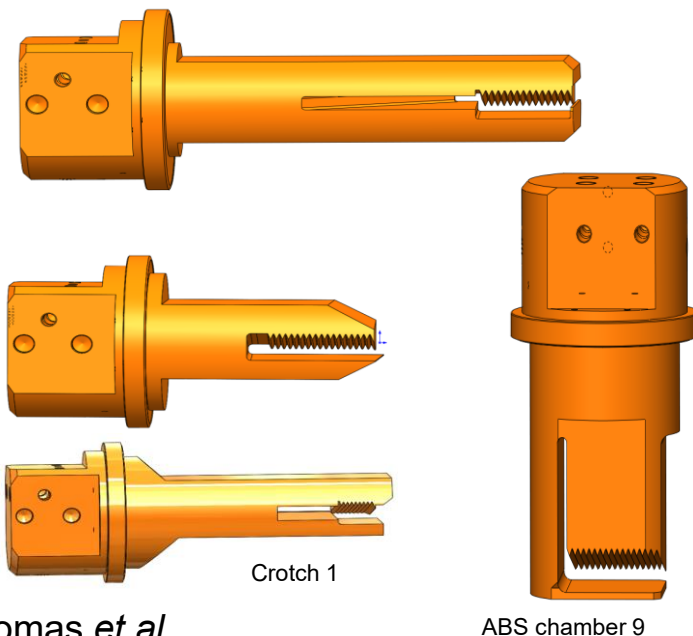


Contents:

- Introduction
- Overview of new Design and Concepts for EBS Absorbers
- CFD Modeling
- Design Criteria and Thermal-Mechanical Modeling
- Conclusion

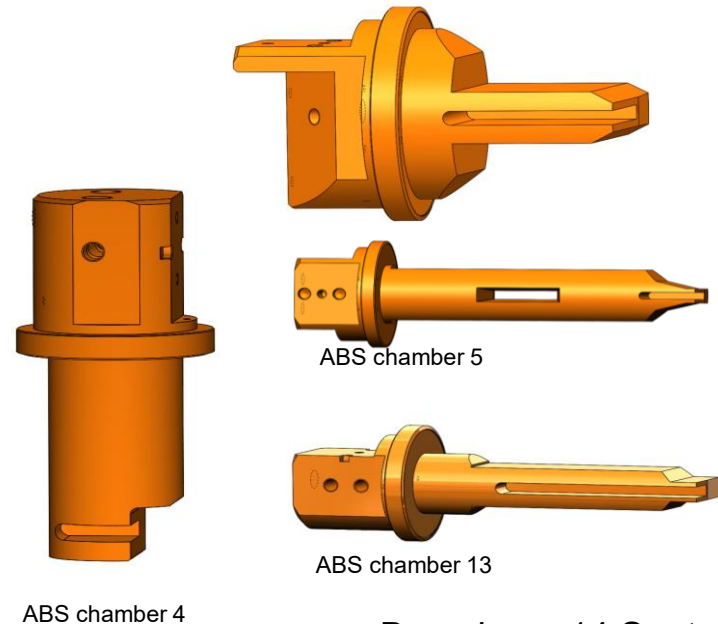
- ~ 400 new Absorbers in the Storage Ring
- Up to 110 W/mm² Normal Incident Power Densities
- Using a new Alloy for Storage Ring Absorbers: CuCr1Zr
- 100% Machined. No Braze, no Weld
- New Cooling Channel Design.

Toothed Family (up to 110 W/mm²)



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Flat Face Family (up to 50 W/mm²)



Barcelona, 14 September 2016

		Glidcop Al-25	CuCr1 Zr	Cu- OFE
MECHANICAL PROPERTIES	Young's modulus E (GPa)	130	128	115
	Yield Strength (MPa)	330	280	75
	Ultimate limit (MPa)	380	380	200
	Elongation at break (A%)	12	8	45
	Hardness (Brinell)	120	125	100
THERMAL PROPERTIES	Thermal expansion at 20°C (1/K)	16.6	17.5	16.8
	Conductivity at 20°C (W.m ⁻² .K ⁻¹)	365	320	393
	Typical max. Heat load (W/mm ²)	70	50	20
DESIGN PROPERTIES	CF Knife edge possible	Yes	Yes	No
	Price (€/Kg) for rods > Ø100mm	45	20 (*)	25

(*) Call for tender – 12 t

Use of CuCr1Zr suggested by S. Sharma (**)

Main Advantages:

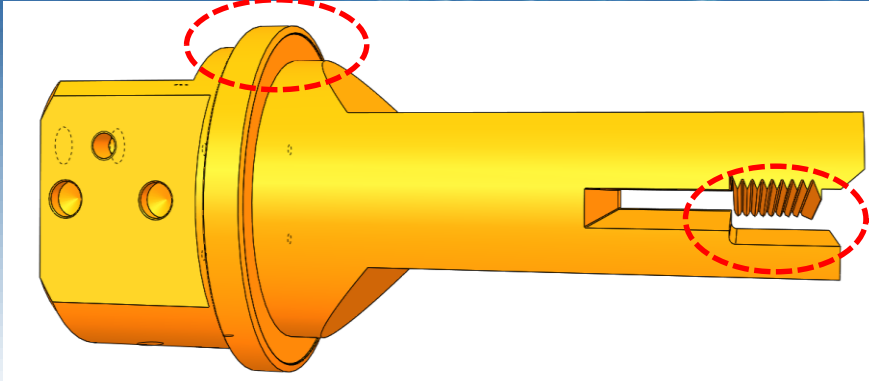
- Close to Glidcop
 - ❖ Mechanical properties significantly better than Cu.
 - ❖ Hard enough to machine CF flanges: manufacturing simplified, no weld, no braze, no problem.
- Cheap

See E. Gagliardini *et al.* poster
This conference

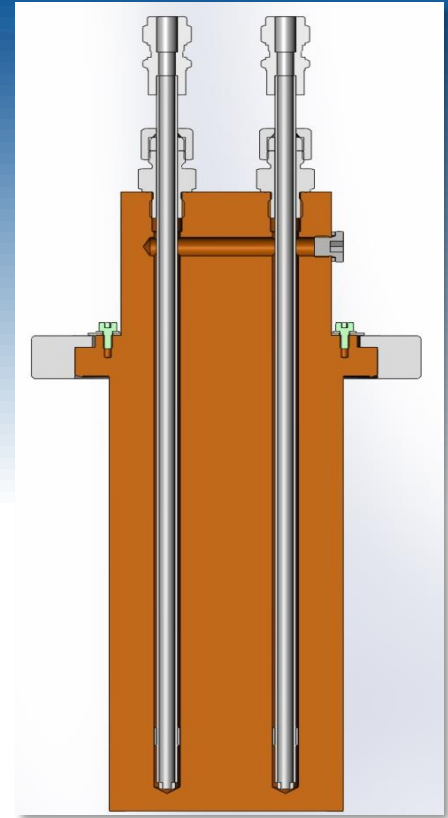
(**) S. Sharma, "A Novel Design of High Power Masks and Slits", Proc. of MEDSI2014, Australia (2014)

Overview: Toothed Absorbers

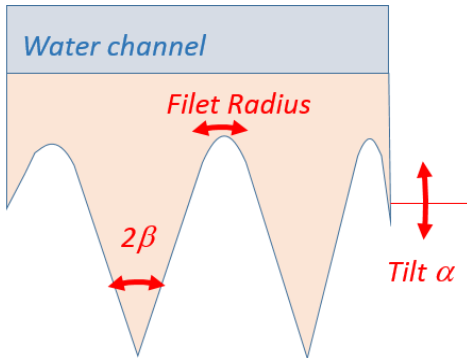
UHV Knife Edge Seal integrated
in the Absorber Body



Power Blocking Head:
- Triangular Tooth (X-Rays)
- Super Tooth + Base Face
(Compton + Rayleigh +
Fluorescence)



Concentric Cooling Channels
Stainless Steel $\phi 6 \times 8$ mm



Design Choices:

- $2\beta = 45^\circ$
- Filet Radius 0.32 mm
- Tilt $\sim 10^\circ$ (Absorber Dependent)

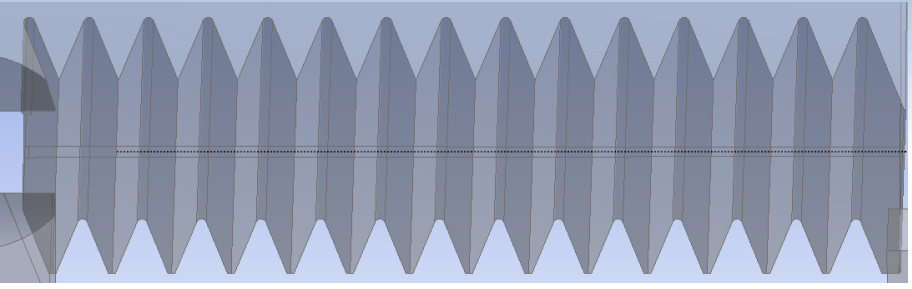
Power Density Attenuation Factor:

$$\sin(\beta)\tan(\alpha) \sim 95\%$$

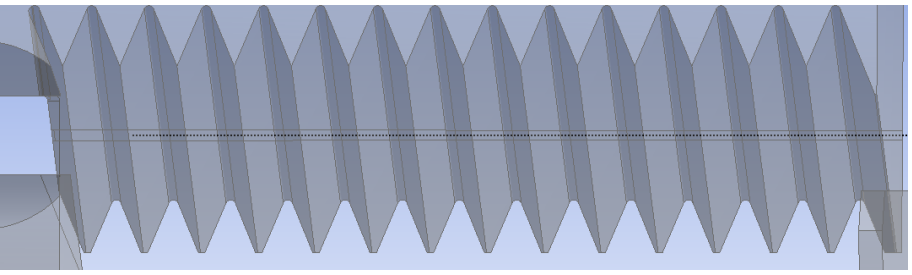
(Theoretical)

Overview: Precision

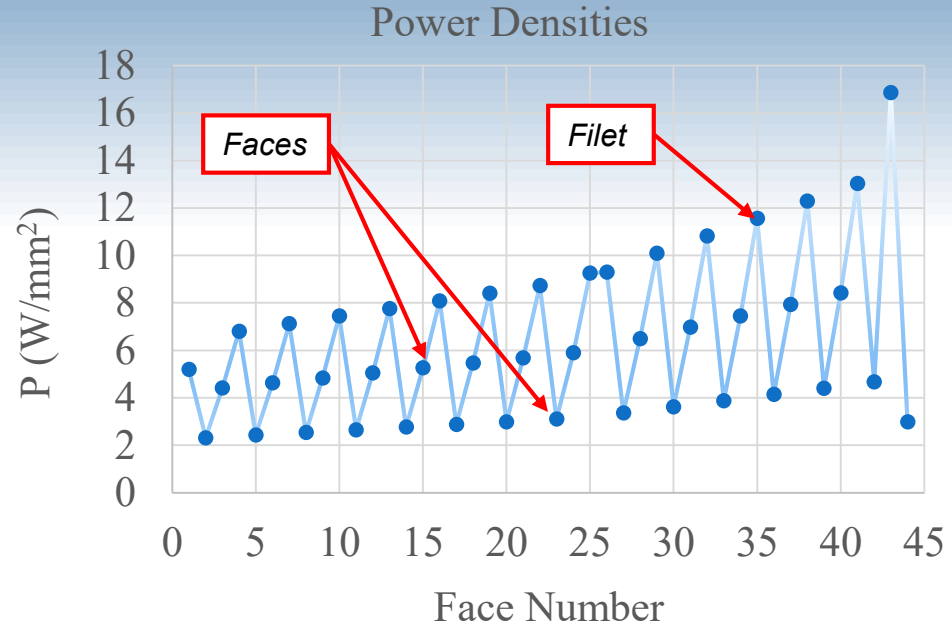
- Design Choices:
- ± 2 mm in Height
 - $\lambda = \pm 1.5^\circ$ in Angle
(0.5° Fan Opening)
(1° Alignment)



$\lambda = 0$. Symmetric Teeth



$\lambda = +1.5^\circ$. Asymmetric Teeth



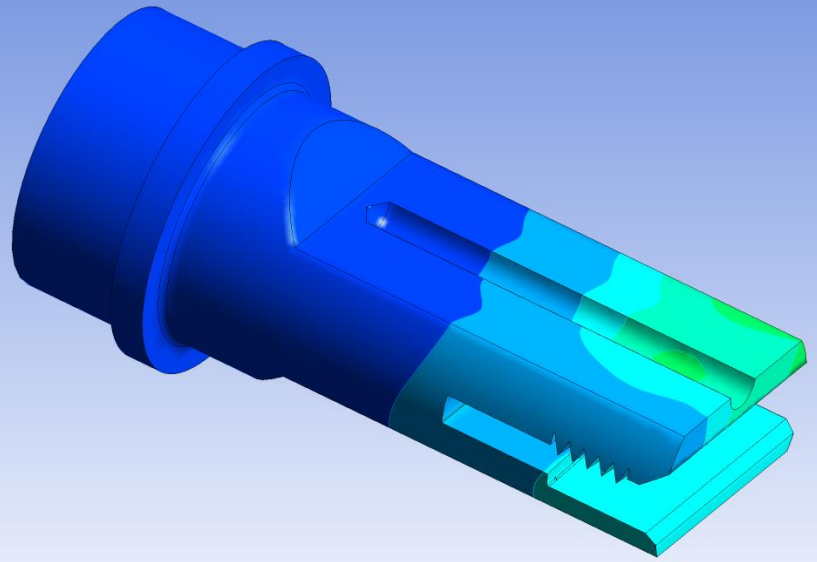
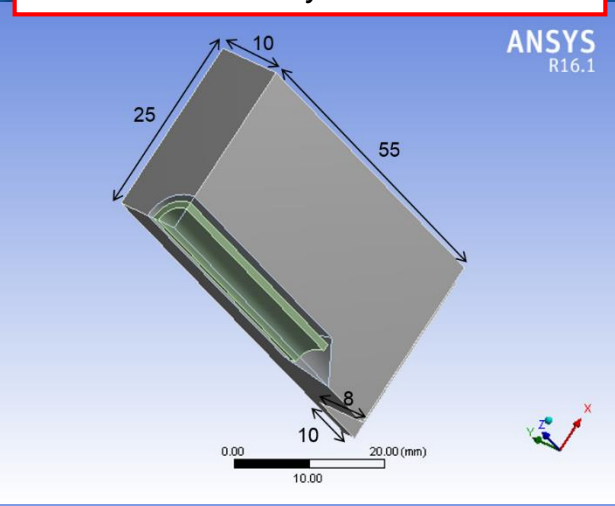
Optimization:

Worst Face and Filet Power Densities close together

CFD: Hydraulic and Thermal-Hydraulic Models

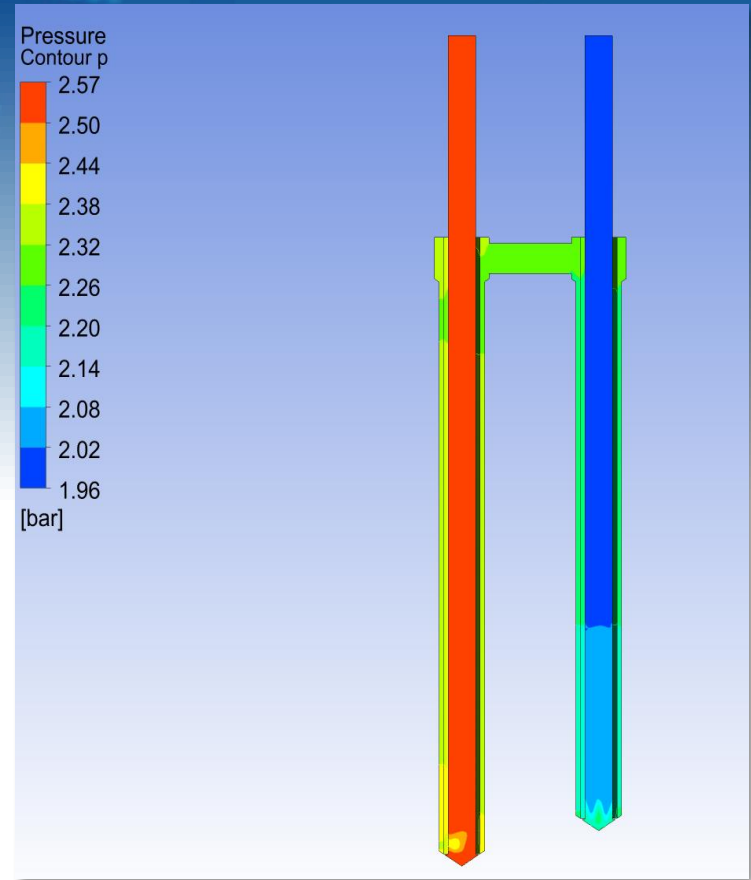
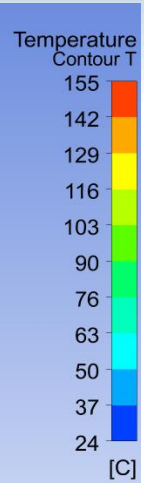


Generic Thermal Hydraulic 1/4th Model



Thermal Hydraulic Model – Real Absorber

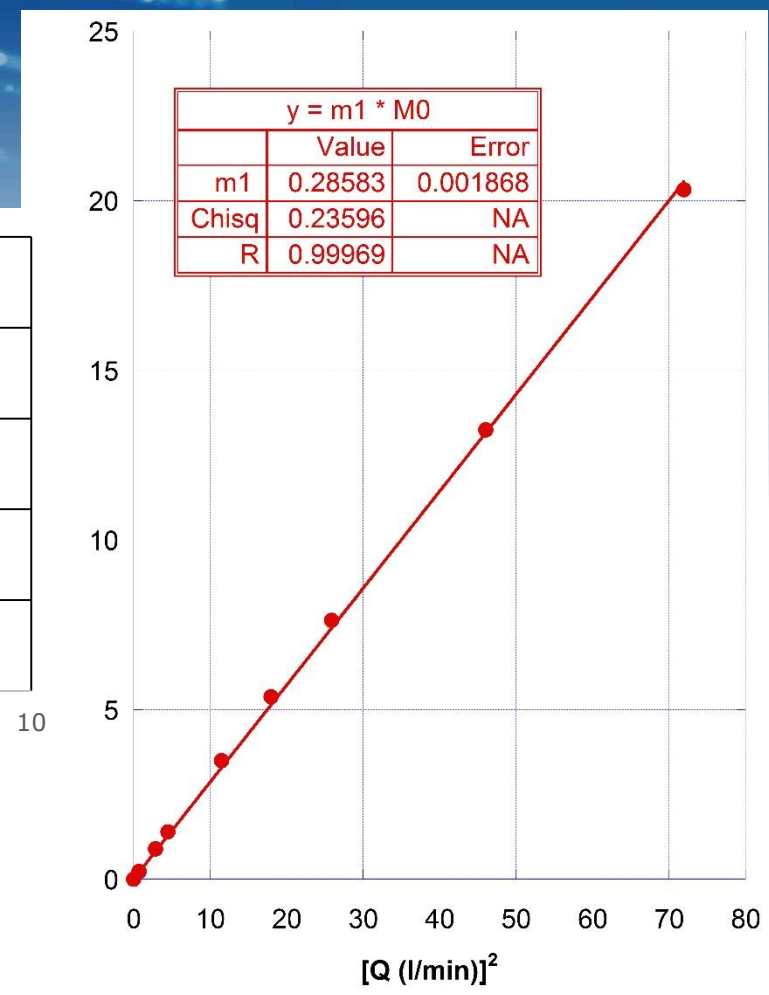
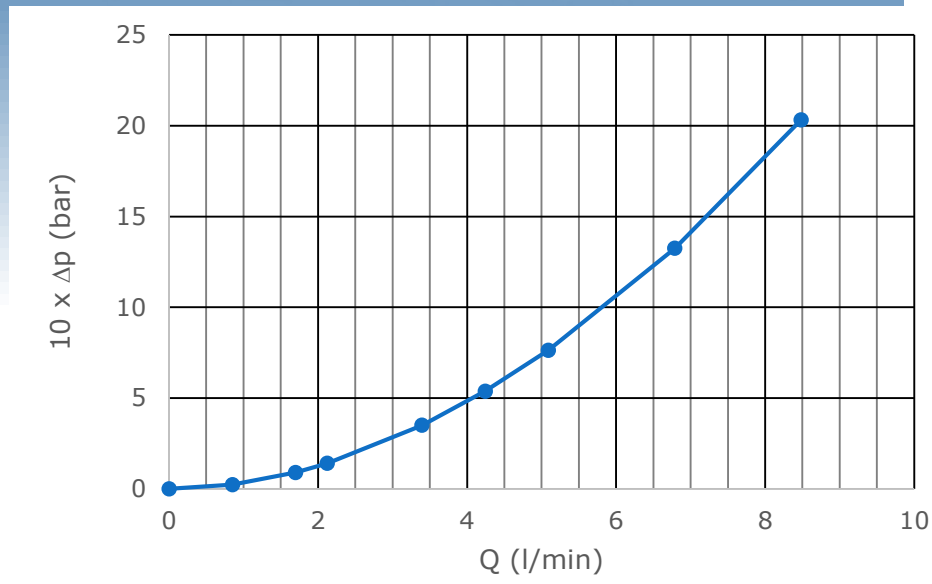
F. Thomas *et al.*



Generic Hydraulic 1/2 Model

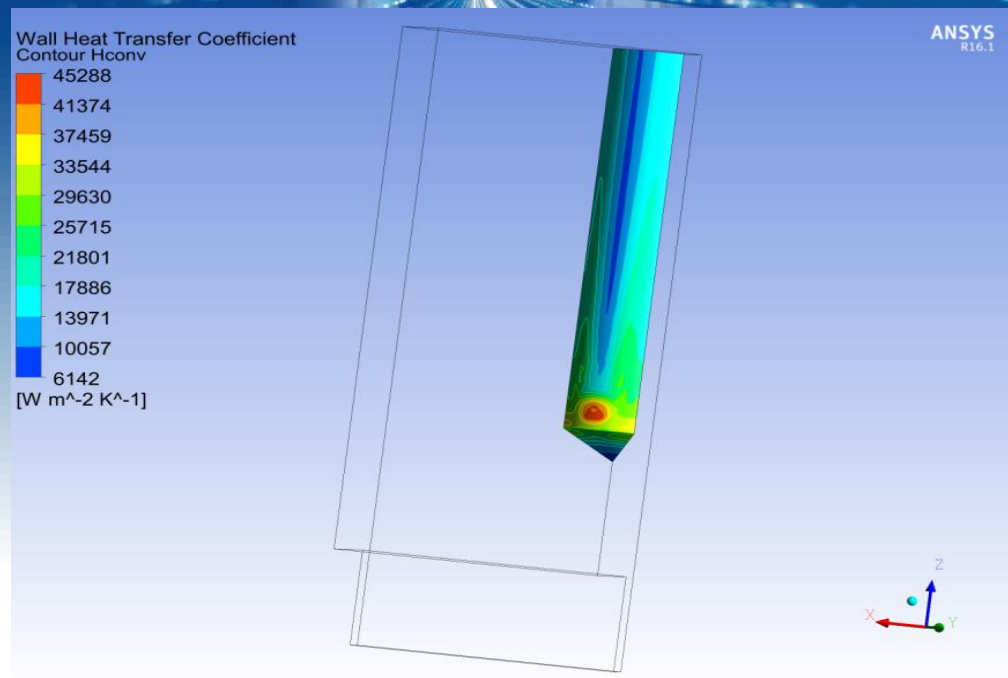
Barcelona, 14 September 2016

**2 Concentric Cooling Channels:
⇒ Turbulent**



$\Delta p > 8$ bar at 25 l/min
Nominal: 4.5 l/min – 0.6 bar

$$\Delta p(\text{bar}) = (0.029 \pm 0.002) \times [Q(\text{l/min})]^2$$

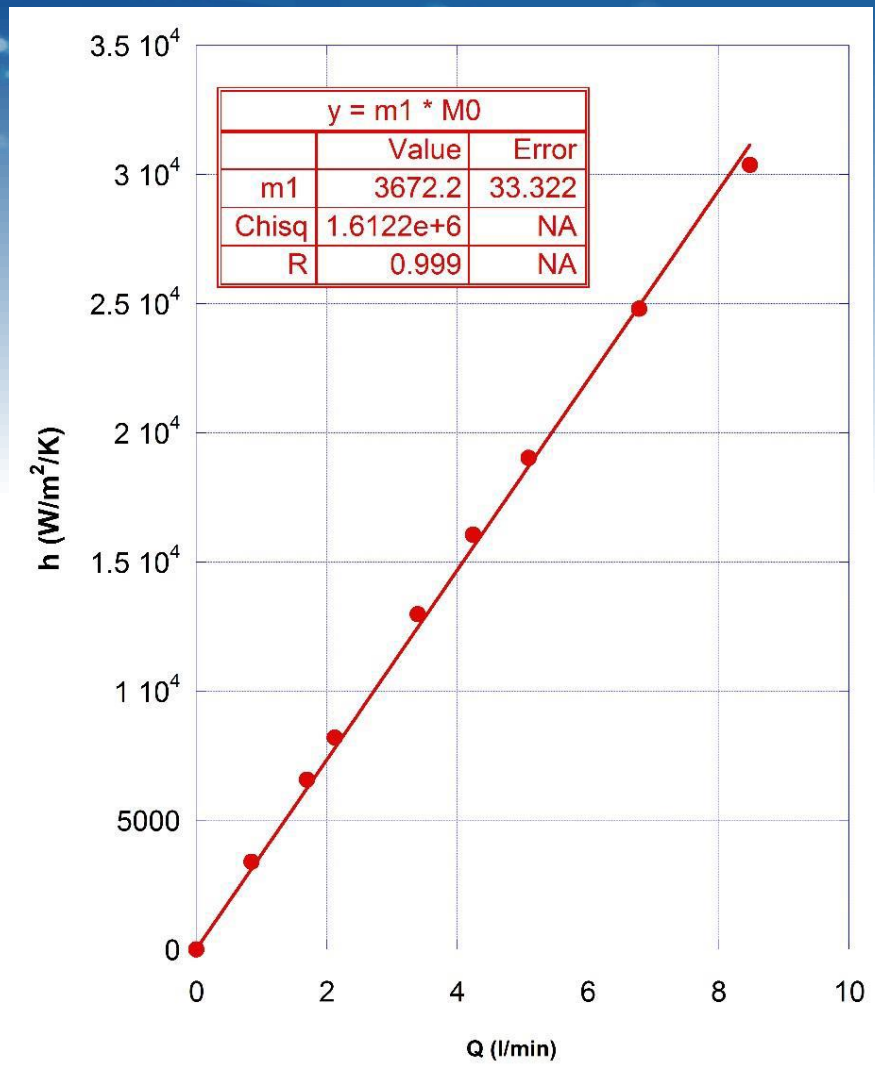


Heat Transfer Coefficient not Constant

Average Heat Transfer Coefficient:

$$h(W/m^2/K) = (3672 \pm 33) \times Q(l/min)$$

$$h = 16.5 kW/m^2/K \text{ at } 4.5 l/min$$



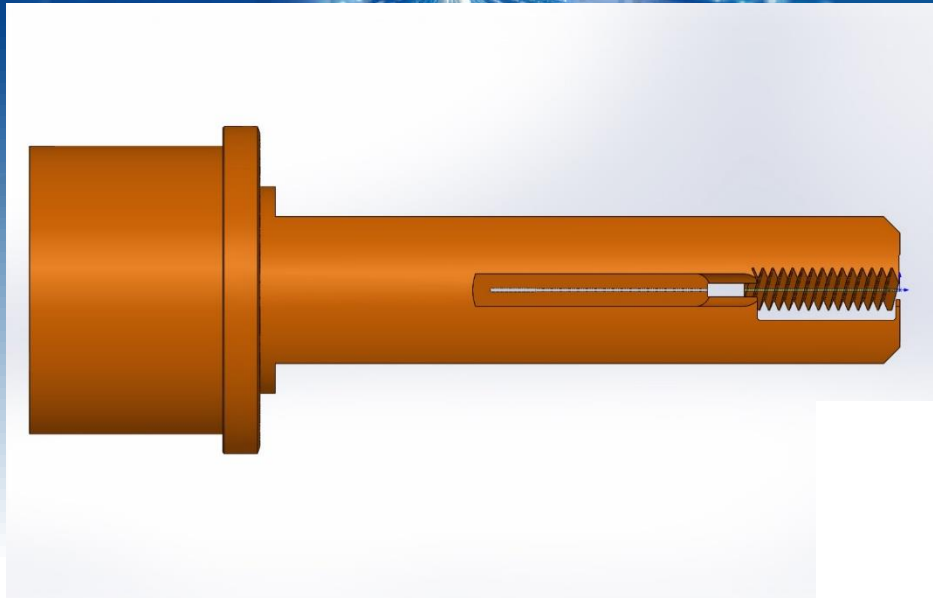
- All Absorbers calculated so far
- Temperature: $T_{Max} < 250^{\circ}C$
- All Absorbers are in the Elastic Regime. No Fatigue.
 - ⇒ S_y is the relevant parameter
- All Stresses are Secondary Stresses.
 - ⇒ S_y is the relevant limit

To be "Elastic ASME" like

Key point: making optimized tooth geometry allows us to stay within the purely elastic regime

Accelerator	Maximum Temperature	Maximum Stress / Strain
ALBA	400° (Glidcop®)	0.2% strain (10 ⁵ cycles)
ANKA, SLS	(Copper)	0.2% strain (10 ⁴ cycles)
APS	541° (Copper) 405° (Glidcop®)	2.S _y , S _F (10 ⁵ cycles) Fatigue Model
DIAMOND	(Copper)	0.5% peak strain 0.1% bulk strain
ESRF	T _{Melt} /2 (All Materials)	$\sigma_{VM} < S_y$
ESRF, EBS	250° (CuCr1Zr)	$\sigma_1 < S_y = 280MPa$ $\sigma_3 > -S_y$ $\tau_{Max} < S_y/2$
SOLEIL	(All Materials)	$\sigma_{VM} < 0.75.S_y$
SPRING-8	(All Materials)	Fatigue Model

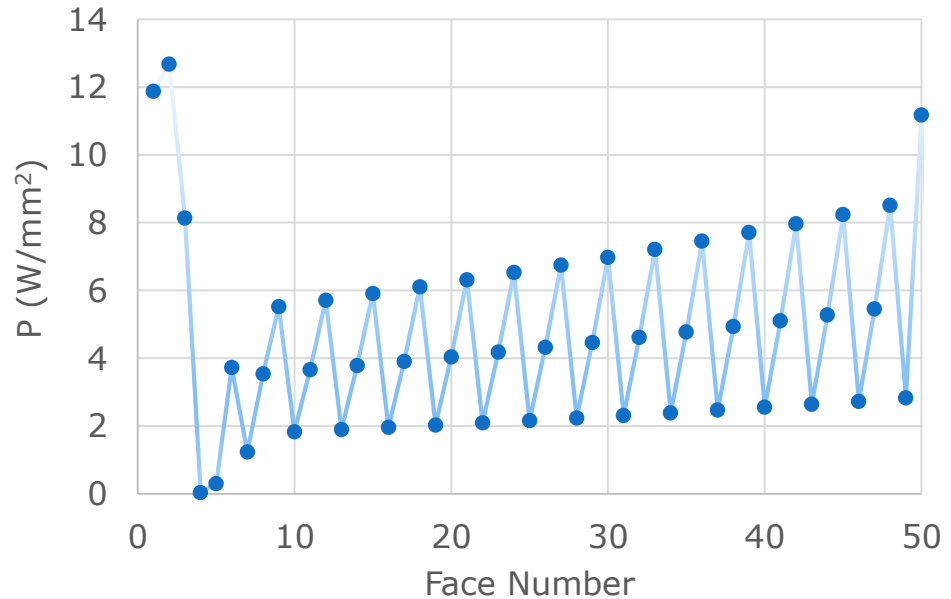
Updated form: M. Quispe *et al.*, "Development of the Crotch Absorber for ALBA storage ring", Proc. of MEDSI2008, Canada (2008)

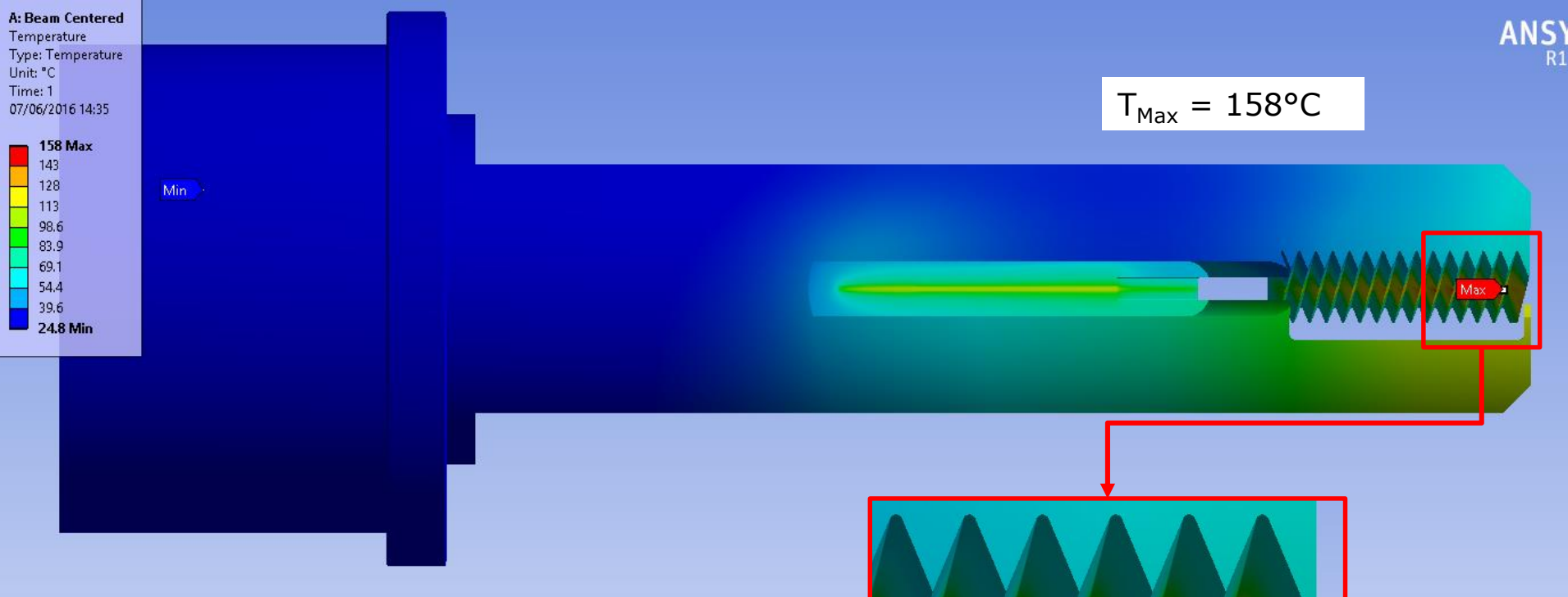


ABS-CH9-1-2:

- Crotch Absorber
- 16 Teeth
- 51 illuminated Faces
- 3 Dipoles – Quadrupoles: 3037 W
- 2 Cooling Channels
- Beam centered, Rotation 1.5°

Power Densities

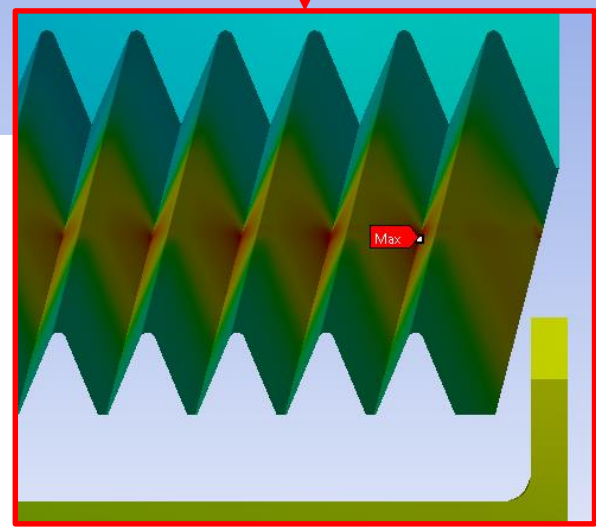


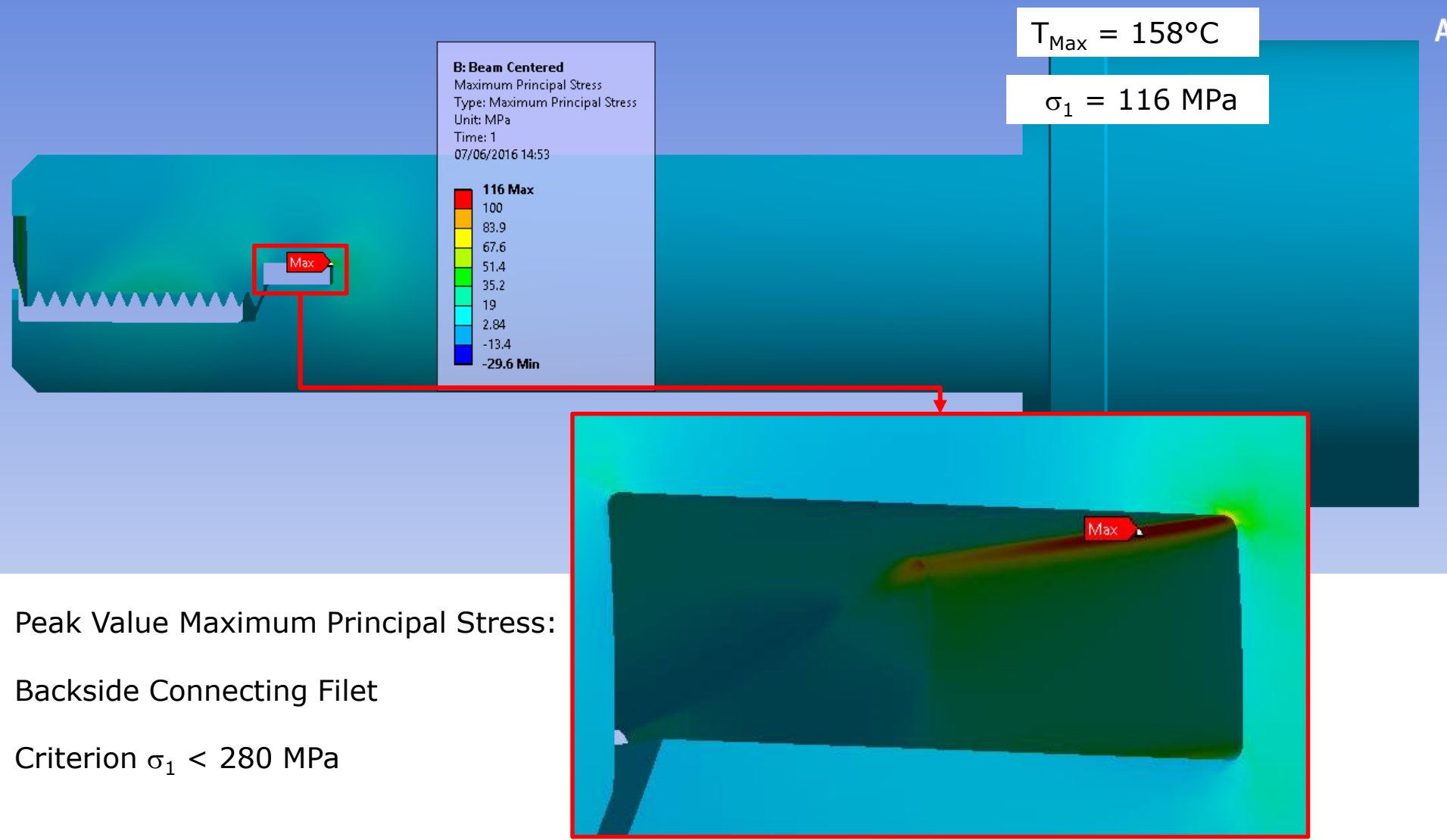


Maximum Temperature:

Tooth 15

Criterion $T_{Max} < 250^{\circ}C$





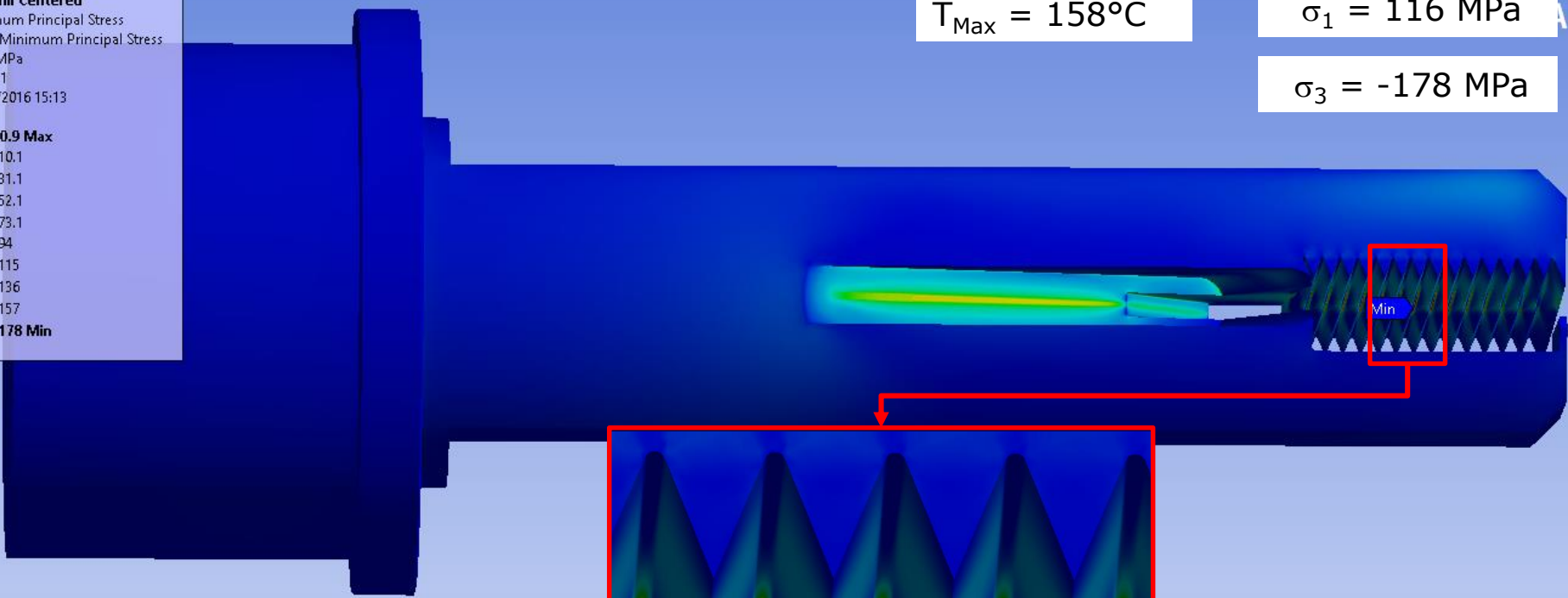
B: Beam Centered
Minimum Principal Stress
Type: Minimum Principal Stress
Unit: MPa
Time: 1
07/06/2016 15:13

10.9 Max
-10.1
-31.1
-52.1
-73.1
-94
-115
-136
-157
-178 Min

$T_{Max} = 158^{\circ}C$

$\sigma_1 = 116 \text{ MPa}$

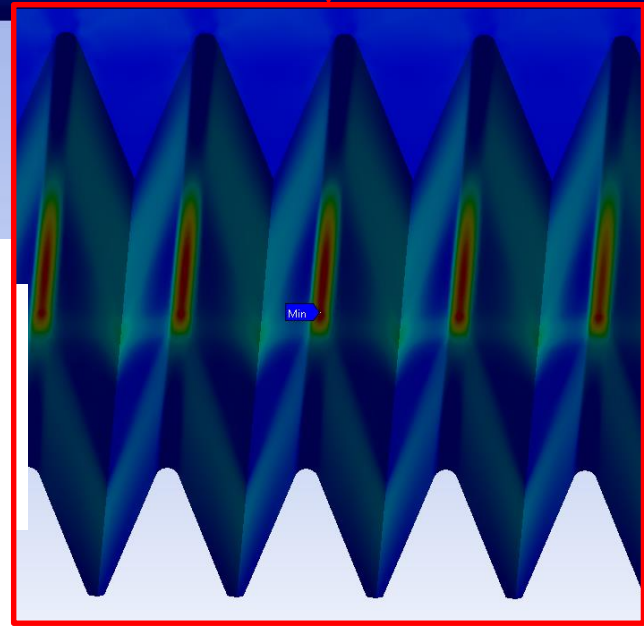
$\sigma_3 = -178 \text{ MPa}$



Peak Value Minimum Principal Stress:

Filet between Teeth

Criterion $\sigma_3 > -280 \text{ MPa}$



Thermal-Mechanical Results

B: Beam Centered
Maximum Shear Stress
Type: Maximum Shear Stress
Unit: MPa
Time: 1
07/06/2016 15:19

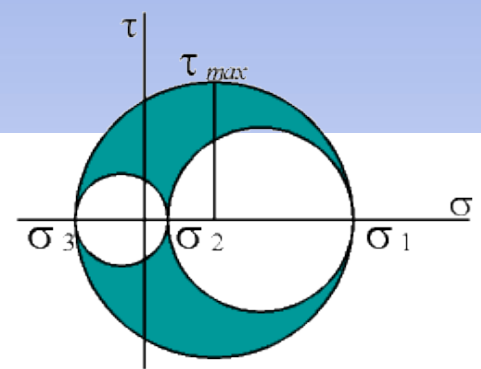
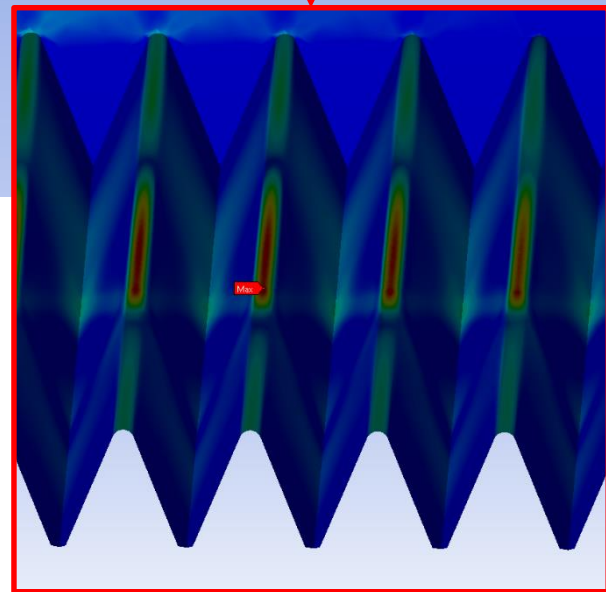
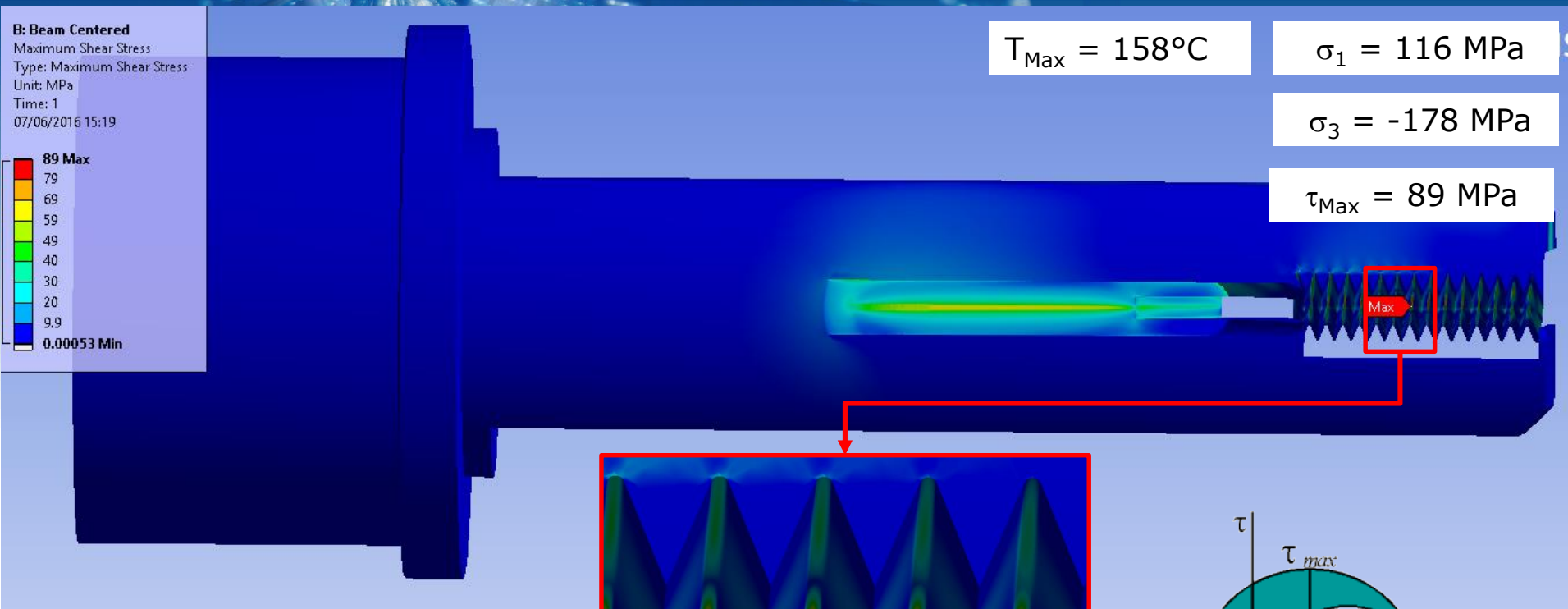
89 Max
79
69
59
49
40
30
20
9.9
0.00053 Min

$T_{Max} = 158^{\circ}C$

$\sigma_1 = 116 \text{ MPa}$

$\sigma_3 = -178 \text{ MPa}$

$\tau_{Max} = 89 \text{ MPa}$



$$\tau_{Max} = \frac{\sigma_1 - \sigma_3}{2}$$

Peak Value Maximum Shear Stress:

Filet between Teeth

Criterion $\tau_{Max} < 140 \text{ MPa}$

Conclusion:

- ~ 400 new Absorbers in the Storage Ring in CuCr1Zr
- 100% Machined. No Braze, no Weld
- Concentric Cooling Channels for Simplicity and Compactness
- Design Optimization:
 - Working in the purely Elastic Regime
 - No Water Cooling for Vacuum Chambers
- Price Optimization:
 - All Absorbers sharing the same Tooth Profile
 - Loose Mechanical Positioning allowed