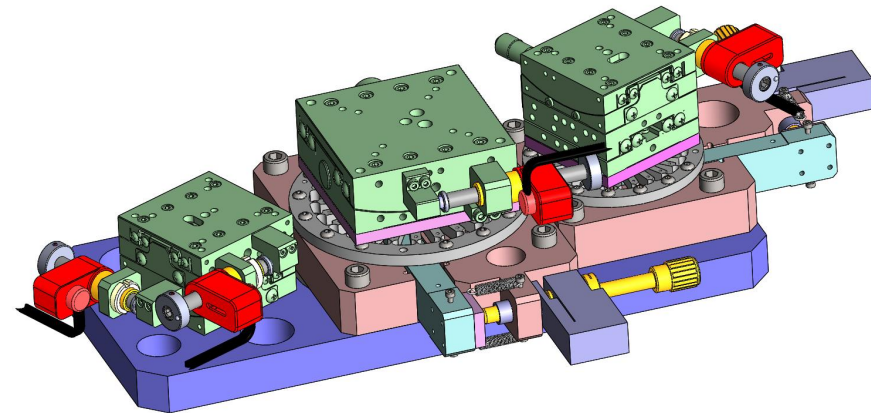


# THE DESIGN OF A PRECISION MECHANICAL ASSEMBLY FOR A HARD X-RAY POLARIZER



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<sup>1</sup>Nanopositioning Support Lab

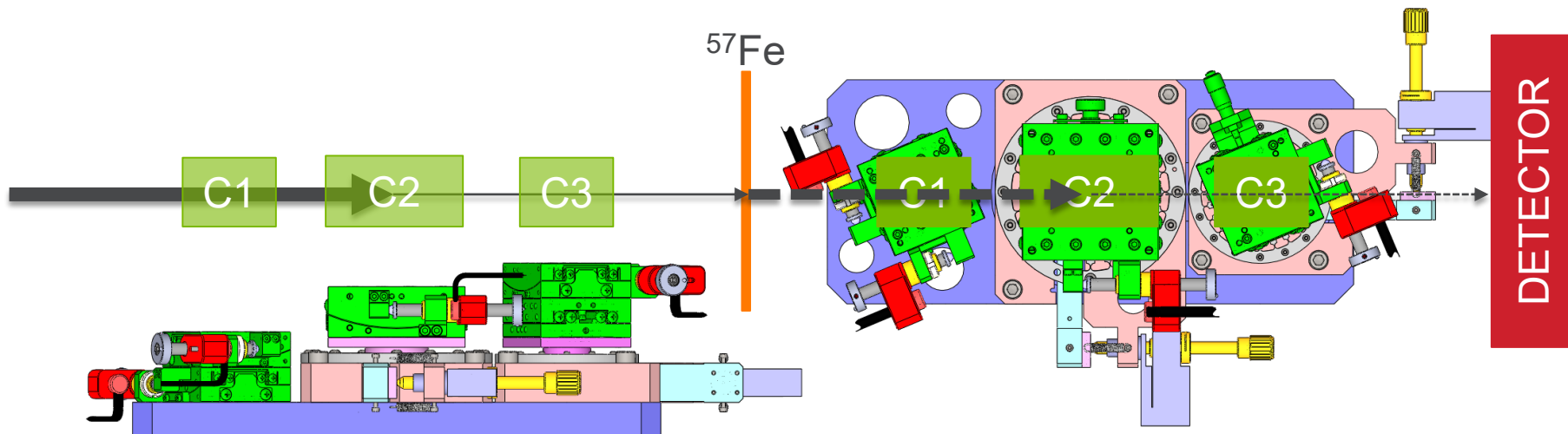
<sup>2</sup>Inelastic X-ray and Nuclear Resonant Scattering

# INTRODUCTION

What does the polarizer do?

Well... Quite simply it polarizes light.

How and why then?



Polarizer 1  
Polarizes incoming photons

Polarizer 2 rotated 90°  
Filters scattered photons

# INTRODUCTION

## Now the why.

- Allows for analysis of polarization state of scattered photons.
- Can be used as a narrow bandwidth  $10^{-7}$  eV filter for 14.413 keV synchrotron radiation using  $^{57}\text{Fe}$  resonance [1].
- This polarizer will be used for next-generation Mössbauer spectroscopy (MS) [2].
- The above will allow for energy spectra to be collected rather than time spectra.

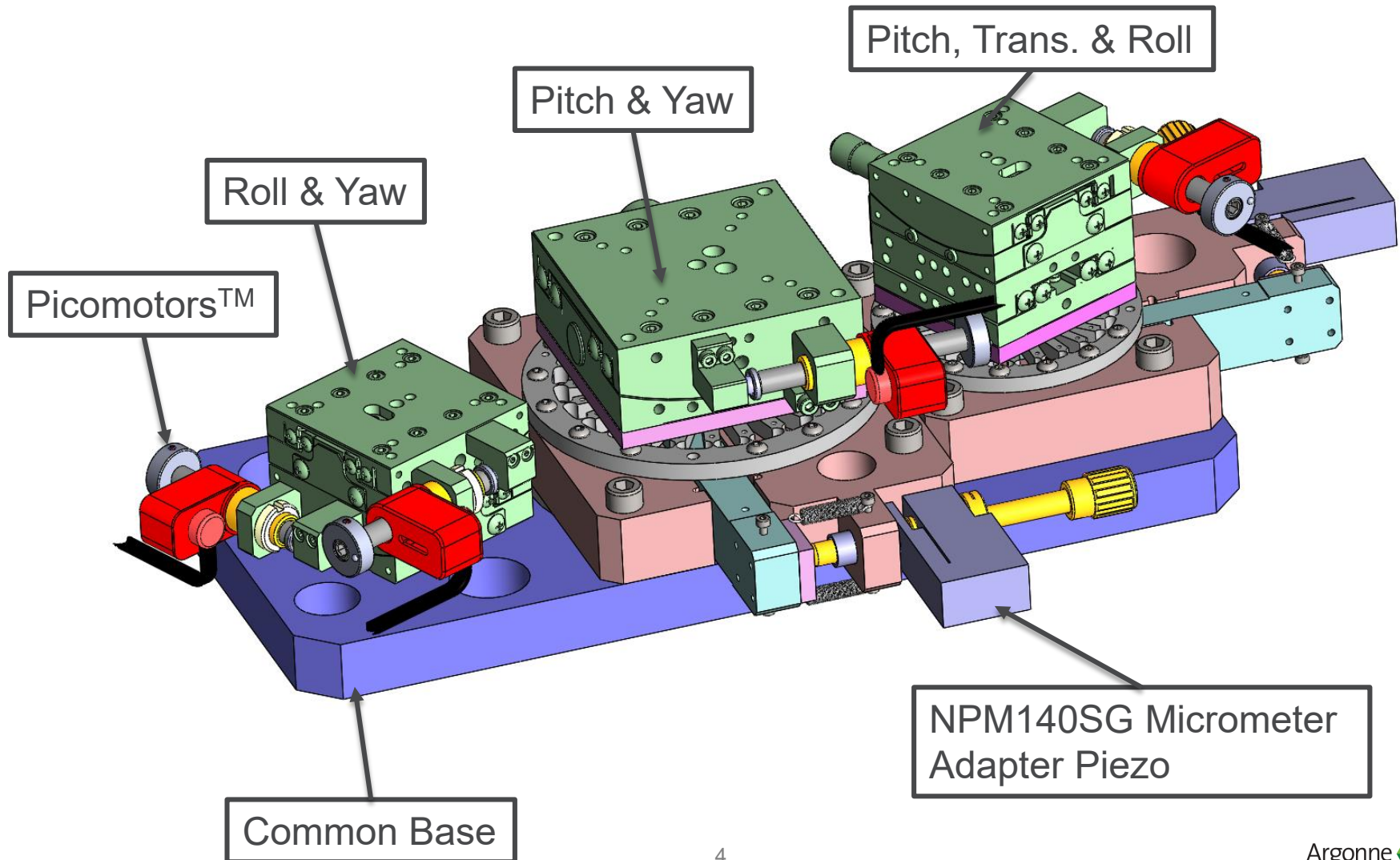
[1] T. Toellner *et al.*, *Applied physics letters*, vol. 67, no. 14, pp. 1993-1995, 1995.

[2] T. S. Toellner, A. Alatas, E. E. Alp, M. Hu, and J. Zhao, LDRD Report, 2015-164-N0, 2015

# POLARIZER DESIGN

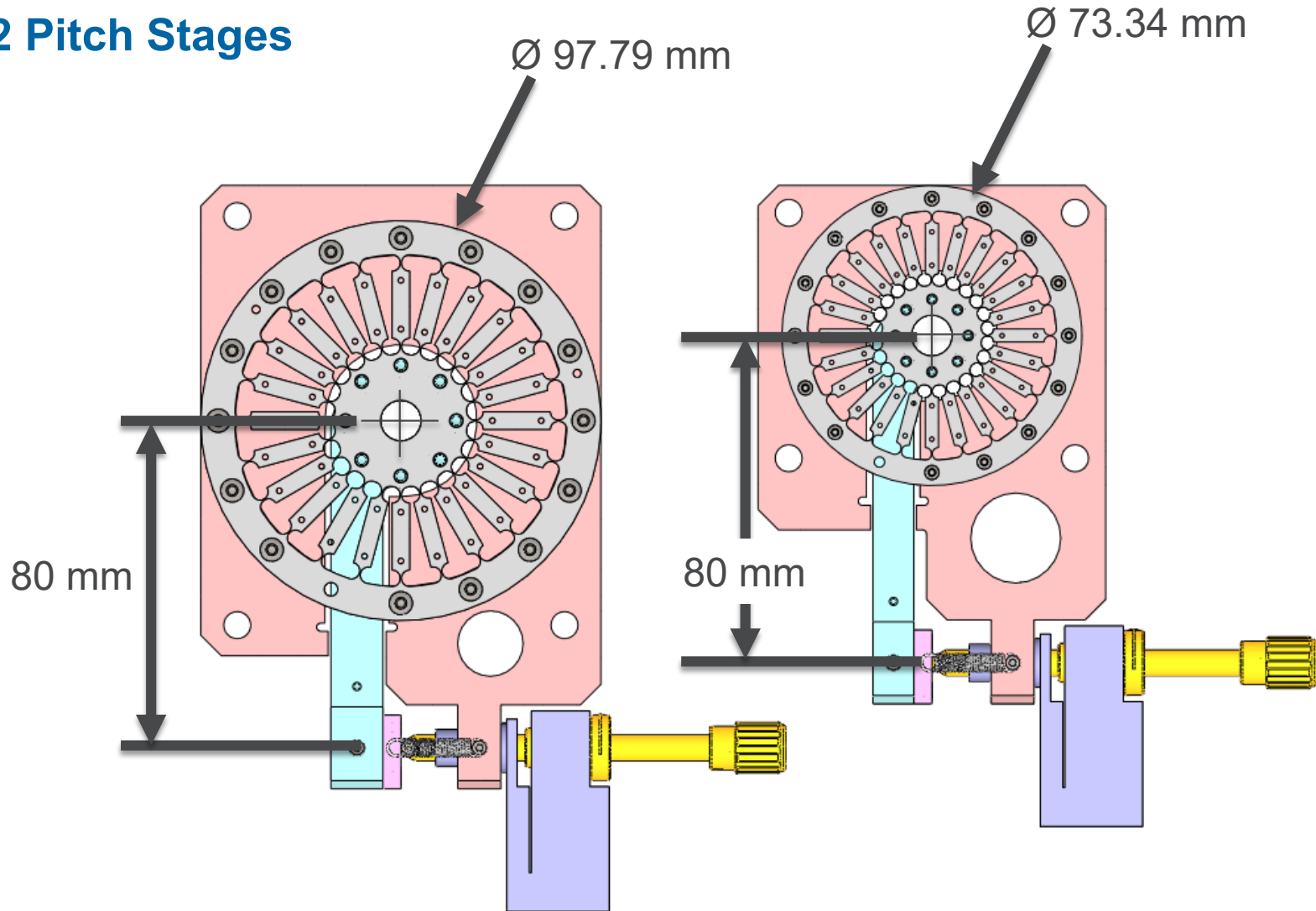
## Complete Assembly – Z4-4600

7DOF total for 3 Independent crystals (not shown)



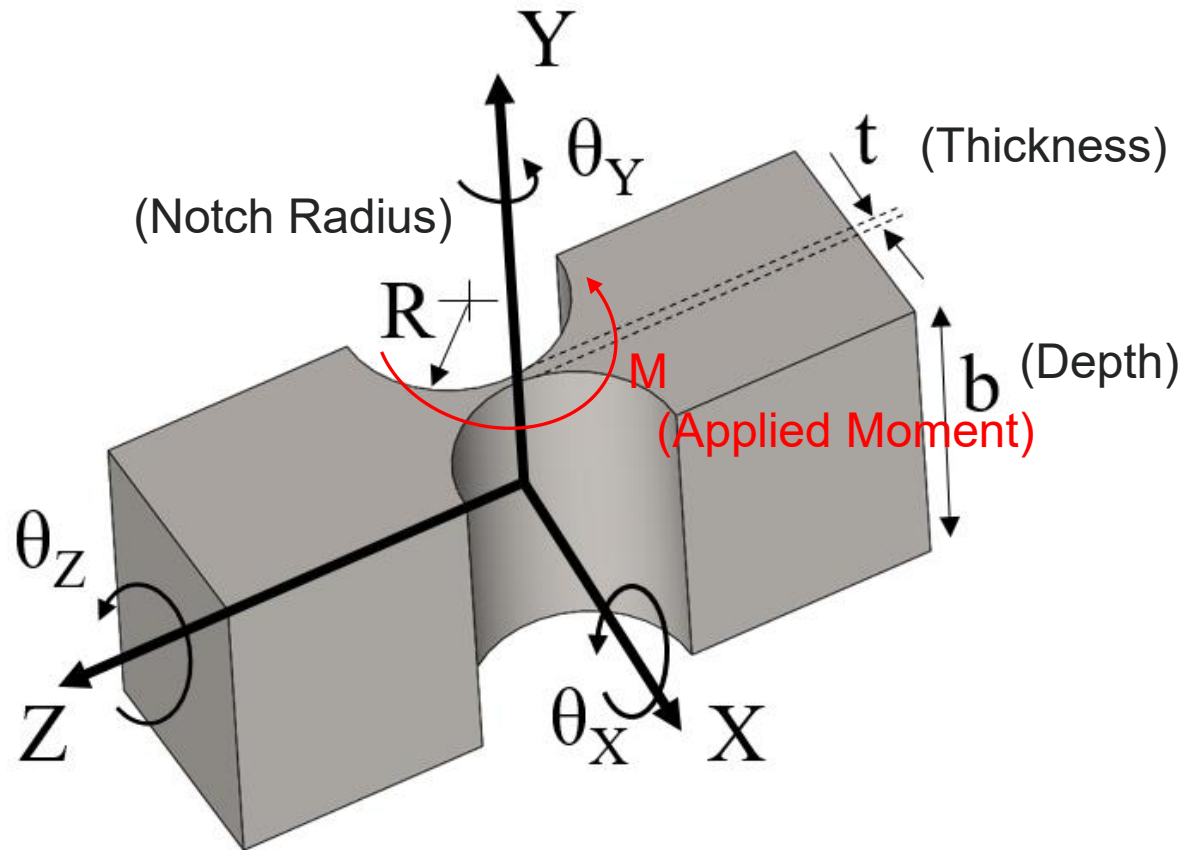
# POLARIZER DESIGN

## 2 Pitch Stages



# DESIGN ANALYSIS

## Flexure Modeling





# DESIGN ANALYSIS

## Flexure Modeling

Not Approximated (Ling's Method [3])

$$K_{\theta_Y} = \frac{M}{\theta_Y} = \frac{2EbR^2}{3f(\beta)}$$

$$f(\beta) = \frac{1}{\Delta} \left\{ \left( \frac{3 + 4\beta + 2\beta^2}{\gamma\Delta} \right) + \left( \frac{6\gamma}{\Delta^{3/2}} \right) \tan^{-1} \sqrt{\frac{2 + \beta}{\beta}} \right\},$$

$$\beta = t/(2R), \quad \gamma = 1 + \beta \quad \Delta = 2\beta + \beta^2,$$

$$\sigma = K_t \sigma_{nom}$$

$$K_t = (1 + \beta)^{9/20}$$

Approximate Method

$$K_{\theta_Y} \approx \frac{M}{\theta_Y} = \frac{2Ebt^{5/2}}{9\pi R^{1/2}}$$

$$\sigma_{nom} = \frac{6M}{t^2 b}$$

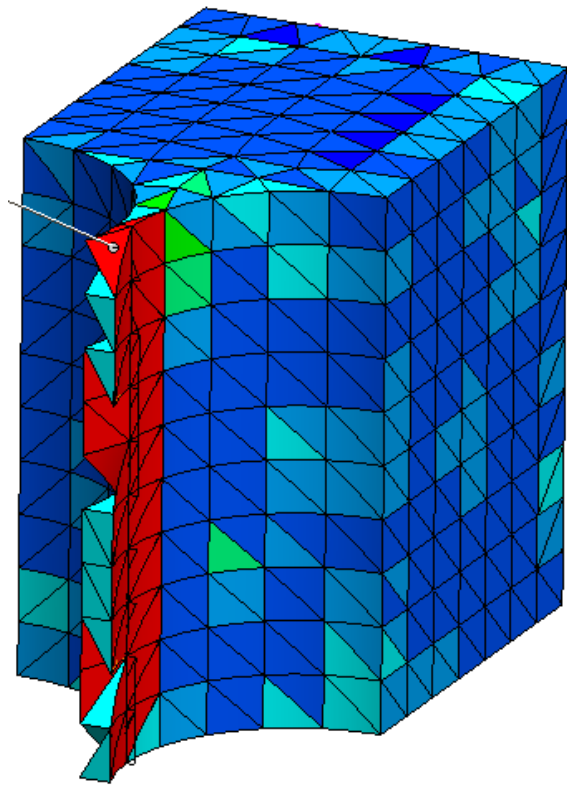
$t = 0.115$ ,  $b = 4.572$ ,  $R = 1.524$  mm,  $M = 1$  N mm,  $E = 204$  GPa

Method	Stress [Mpa]	Angle [°]	Torsional Stiffness [N·mm/°]
Ling's	100.9	0.25	4.07
Approx.	99.2	0.24	4.18
% Error	-1.65	-2.68	2.70

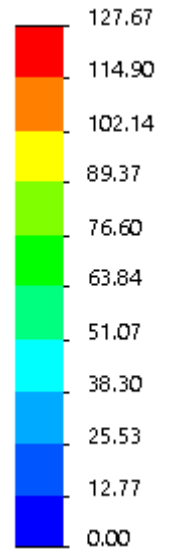
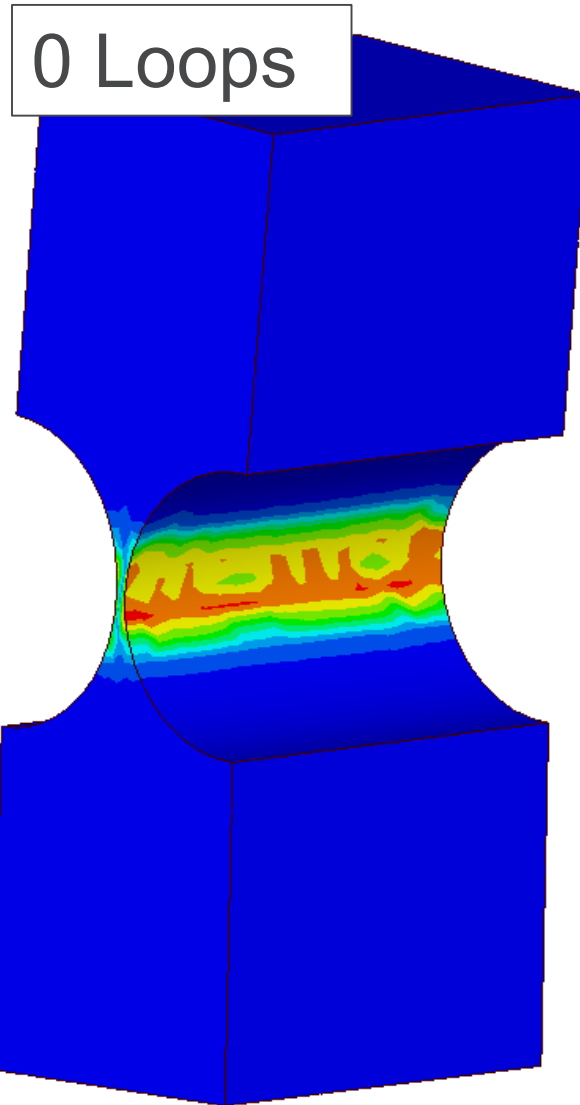
[3] C.-B. Ling, "On the stresses in a notched strip," *J. of Appl. Mech. Trans. ASME*, vol. 19, no. 2, pp. 141-146, 1952

# DESIGN ANALYSIS

## FEA Flexure Mesh Validation



Aspect  
Ratio

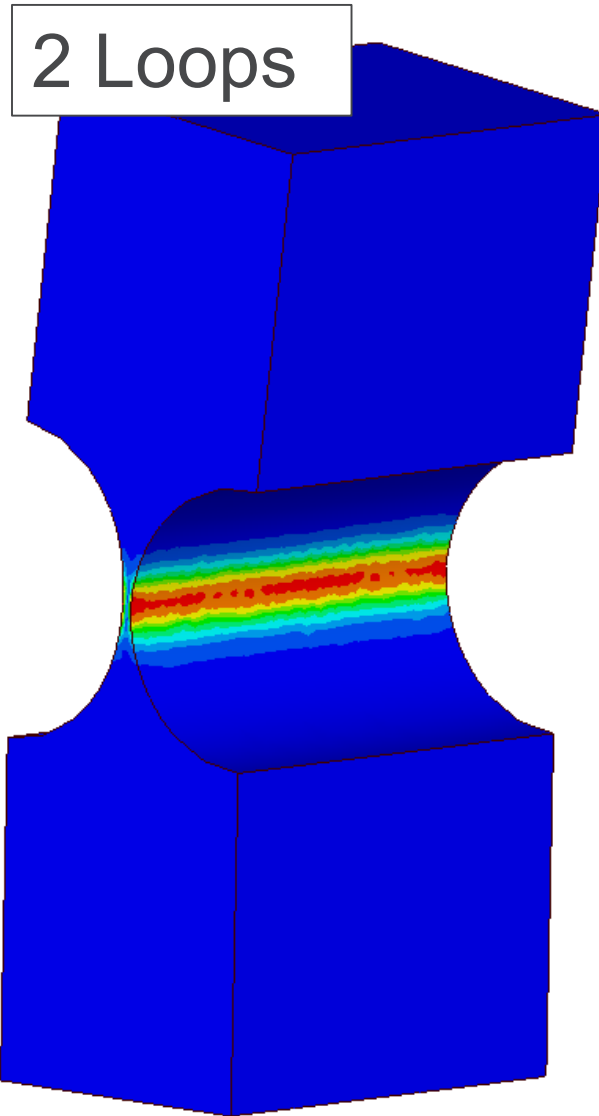
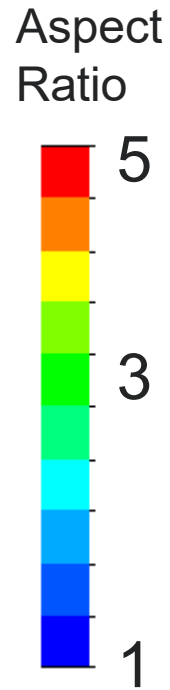
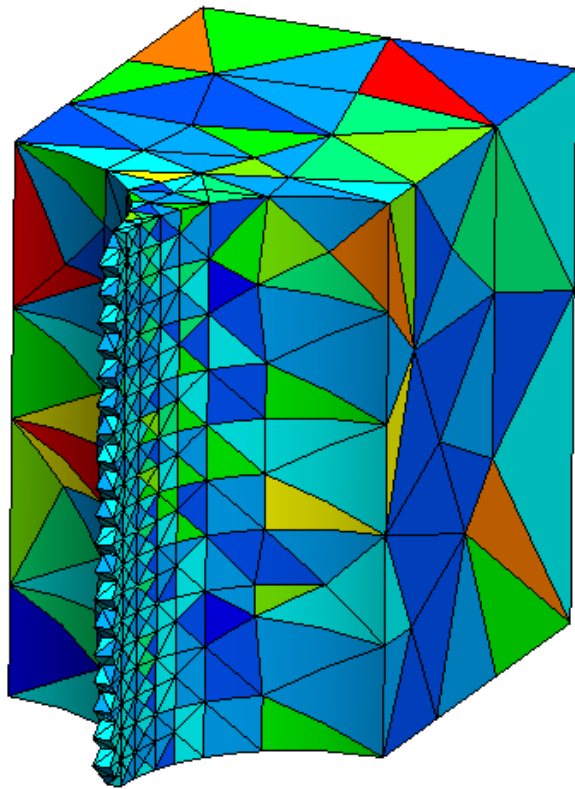


$t = 0.115$ ,  $b = 4.572$ ,  $R = 1.524$  mm,  $M = 3$  N mm,  $E = 204$  GPa



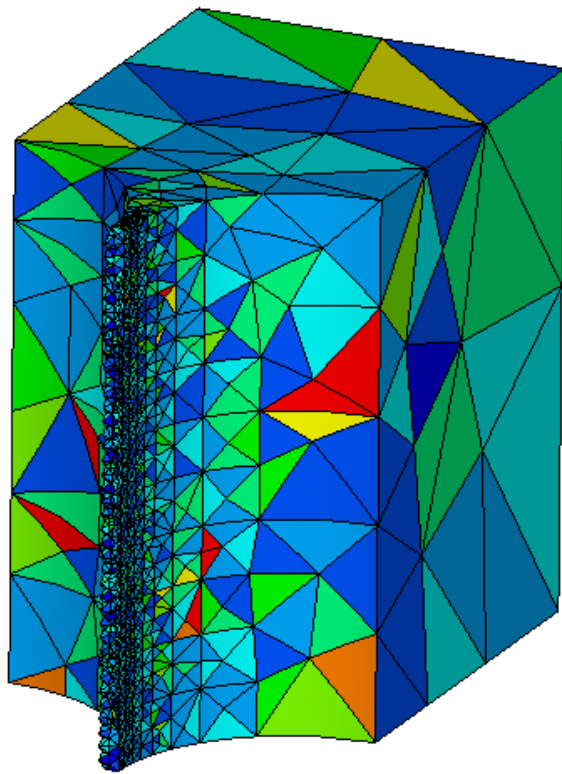
# DESIGN ANALYSIS

## FEA Flexure Mesh Validation



# DESIGN ANALYSIS

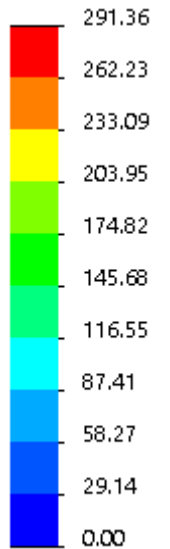
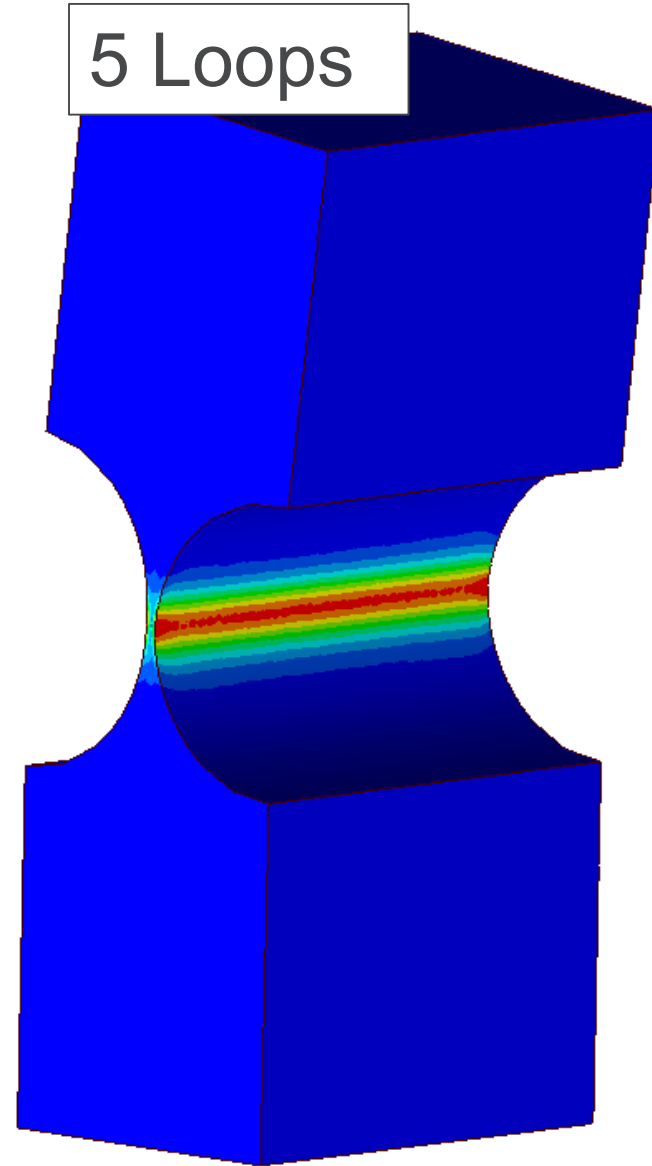
## FEA Flexure Mesh Validation



Aspect  
Ratio

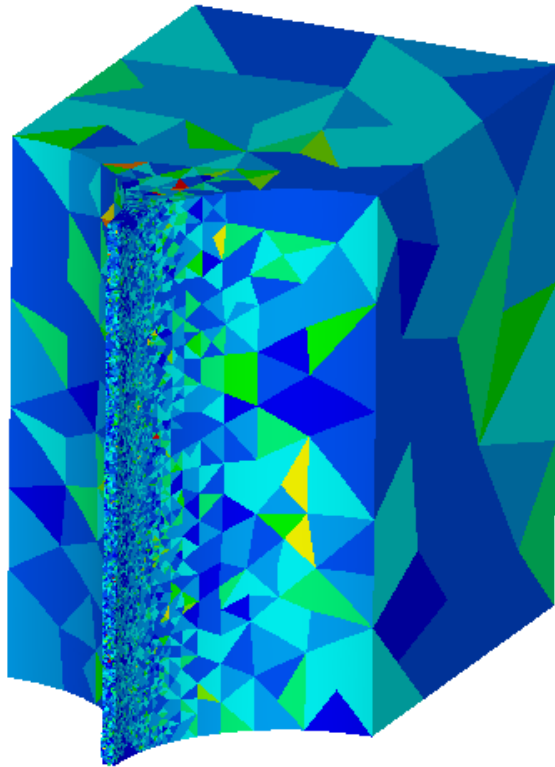


5 Loops

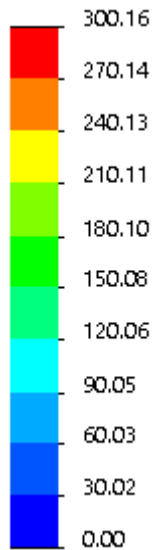
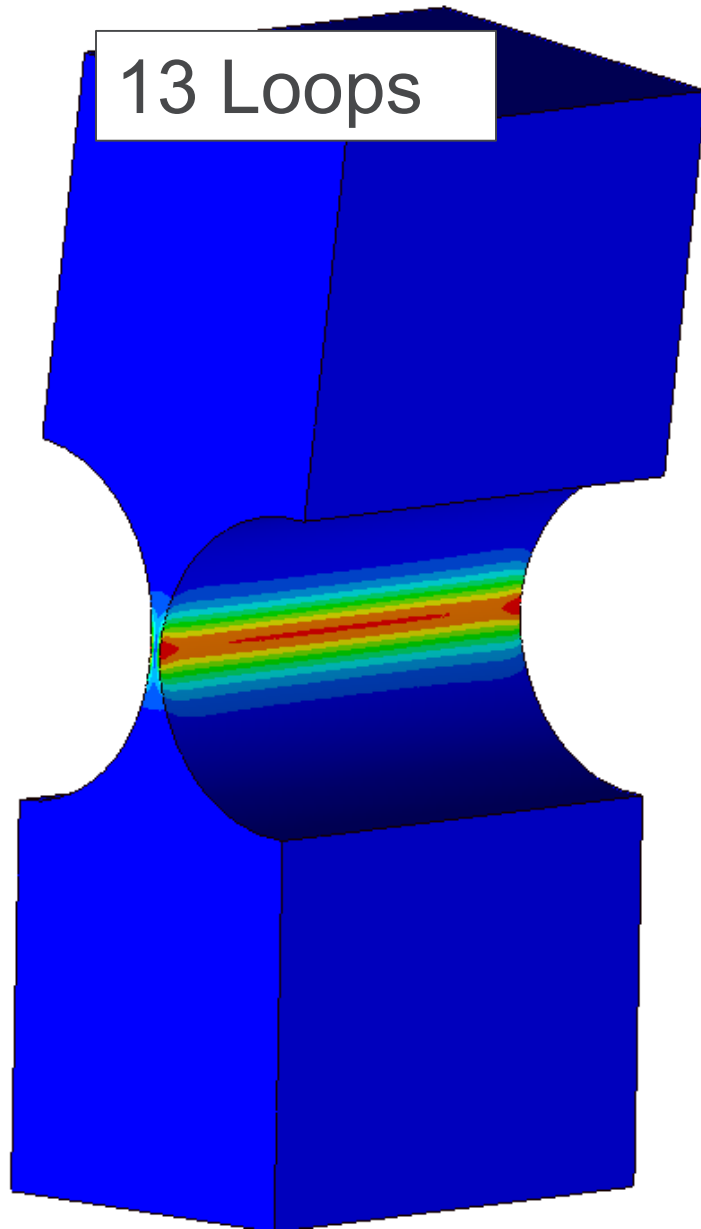


# DESIGN ANALYSIS

## FEA Flexure Mesh Validation

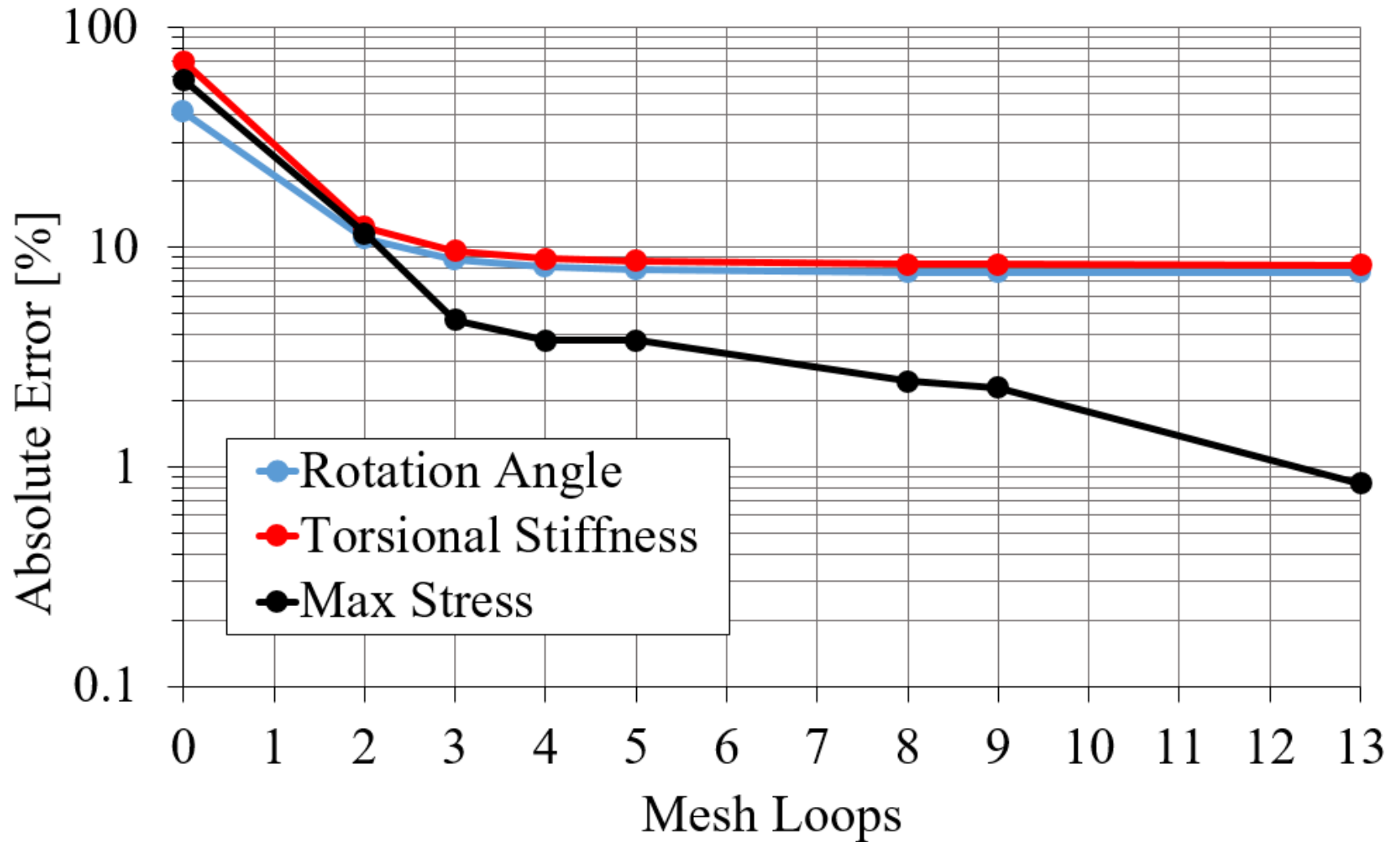


Aspect Ratio



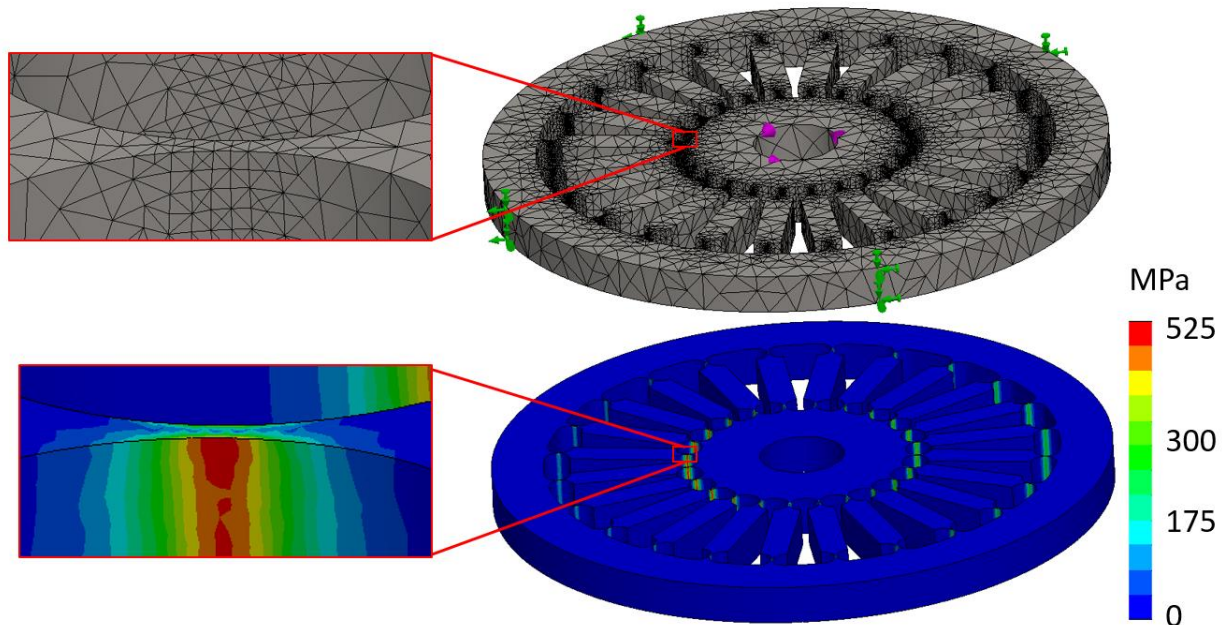
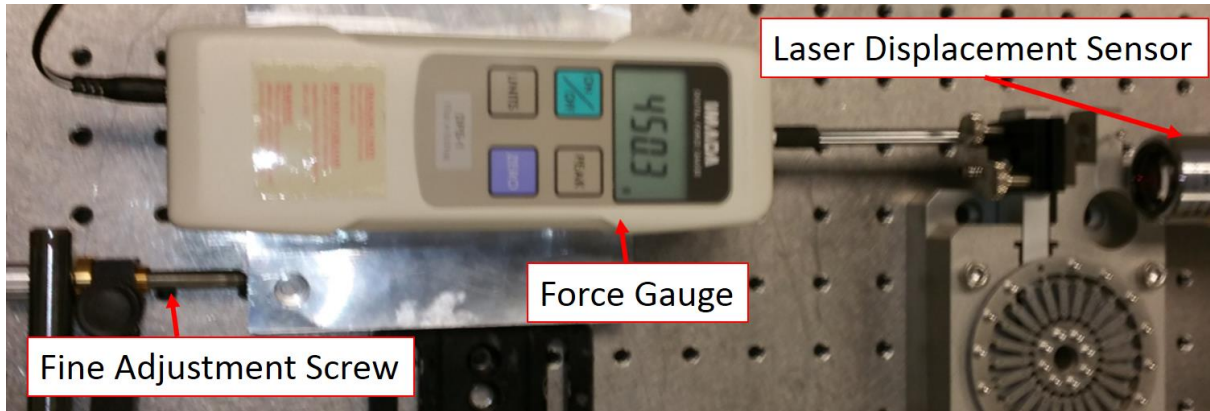
# DESIGN ANALYSIS

## FEA Flexure Mesh Validation



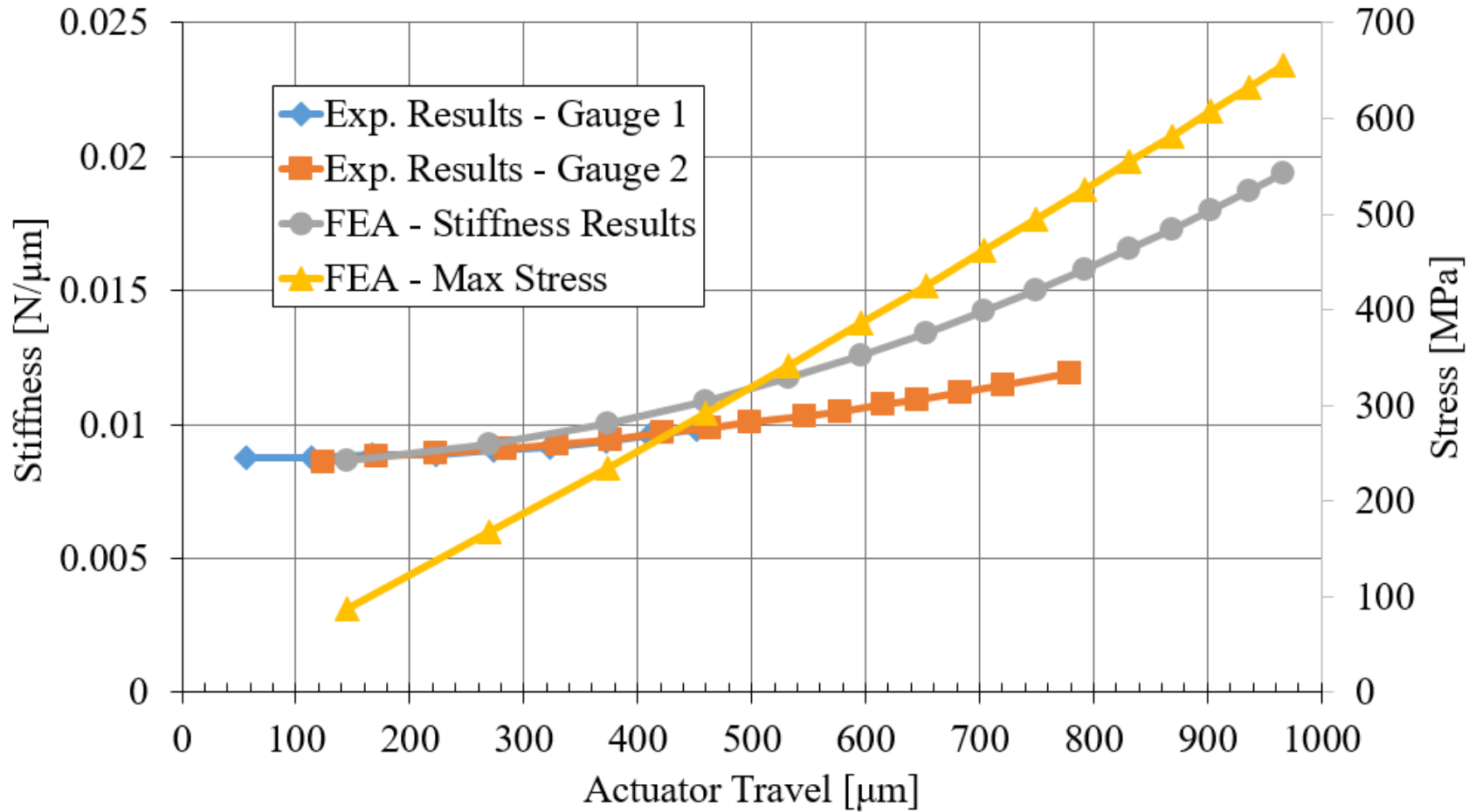
# DESIGN ANALYSIS

## FEA Weak-Link Model Validation and Simulation

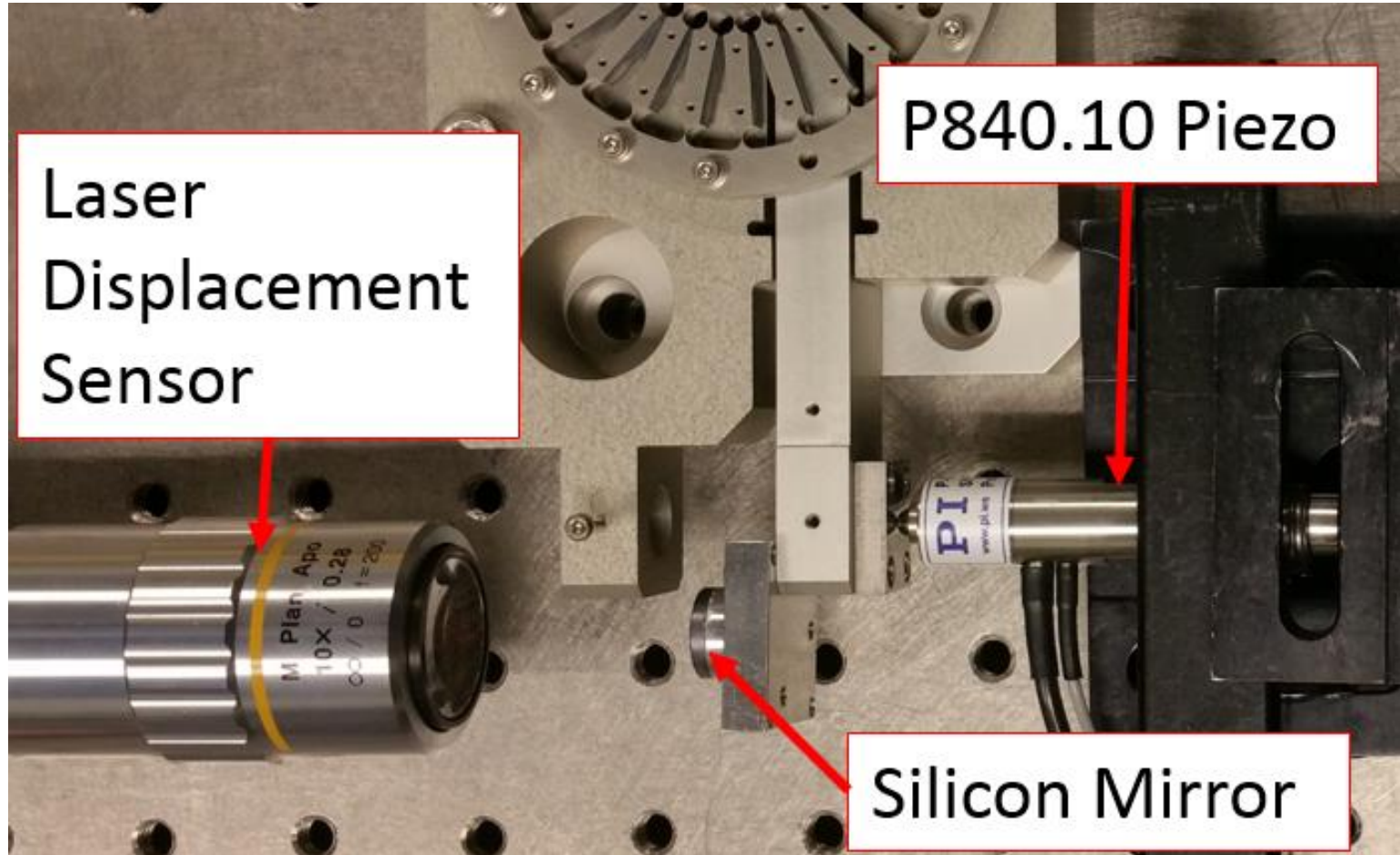


# DESIGN ANALYSIS

## FEA Weak-Link Model Validation and Simulation

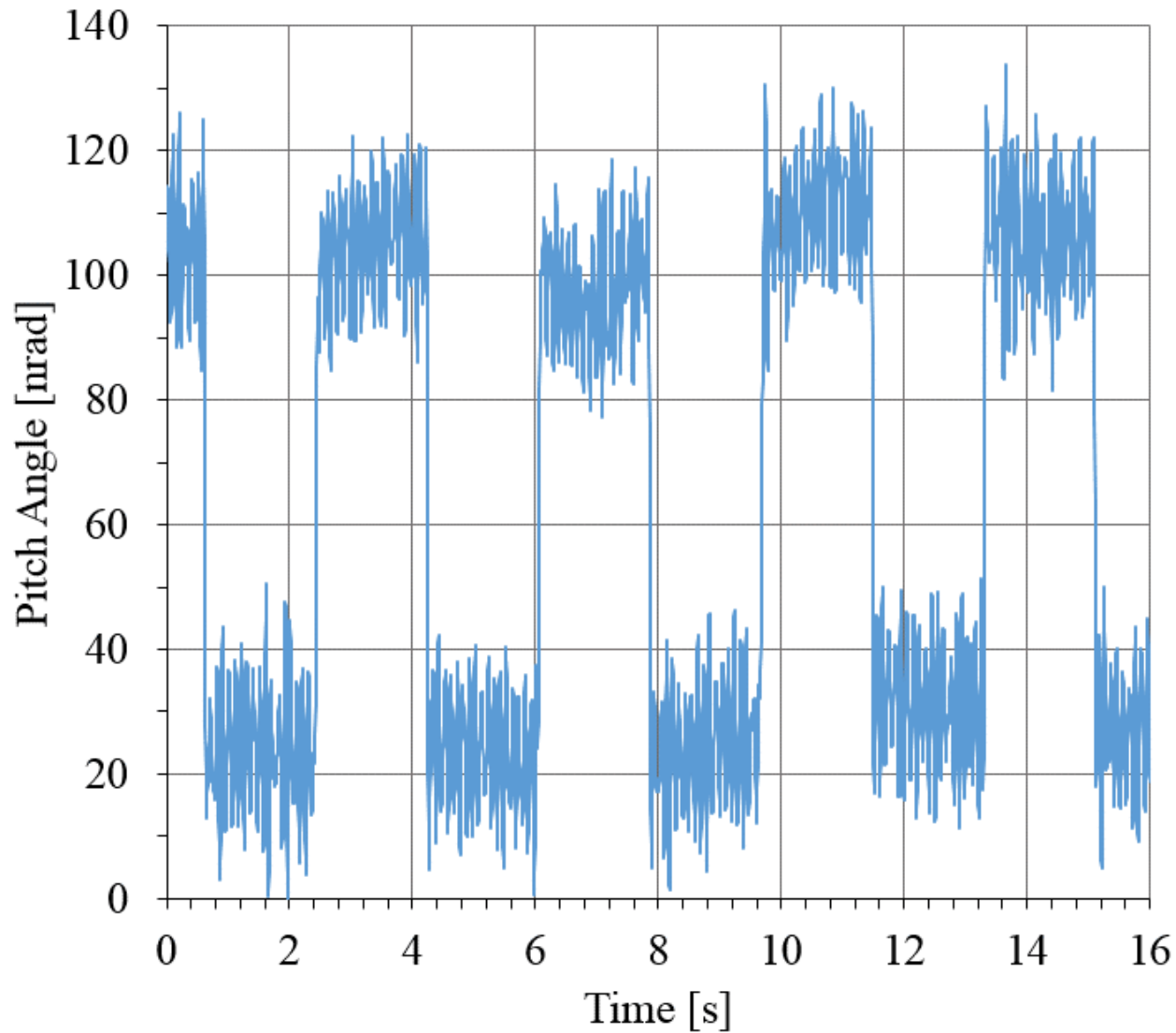


# EXPERIMENTAL RESULTS





# EXPERIMENTAL RESULTS



# CONCLUSION

- 5 adaptive mesh loops reduce stress error to ~5%.
- Too fine of a mesh can start to increase stress error.
- Only small deformations in the FEA model, on the order of 12% of yield, agree with measurements.
- Final resolution of pitch stage could be as low as 5-10 nrad

**THANK YOU!**

**QUESTIONS?**

**FUNDING SUPPORT**

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