

WAKEFIELD BAND PARTITIONING IN LINAC STRUCTURES

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Abstract

In the NLC project multiple bunches of electrons and positrons will be accelerated initially to a centre of mass energy of 500 GeV and later to 1 TeV or more. In the process of accelerating 192 bunches within a pulse train, wakefields are excited which kick bunches off axis, can induce the beam break-up instability and dilute the luminosity. Several accelerating structures have been designed and tested at SLAC and KEK, and have been found to successfully damp wakefields [1]. However, these structures, operating at $2\pi/3$ phase advance, suffered from rf breakdown damage. This experience has prompted us to numerically explore lower group velocity structures operating at higher fundamental mode phase advances. We report on the distribution of kick factors among the lower dipole passbands as a function of accelerating mode phase advance in such structures. These results are applicable to both travelling wave and standing wave structures.

1 INTRODUCTION

The initial NLC/JLC structures, built and tested at SLAC and KEK, were designed to accelerate electron and positron beams up to 0.5 TeV and up to 1.5 TeV in later upgrades. In order to efficiently accelerate the charged particles, multiple bunches are accelerated within a pulse of the RF field and this requires loaded field gradients of the order of 70 MV/m. These accelerating structures were chosen to be 1.8 meters in length. The dipole mode frequencies of these structures were detuned, by varying the cell dimensions along the structure, in order to reduce the dipole long-range wakefield seen by trailing bunches. The first band wakefield in the structure DDS1 (Damped Detuned Structure) was well-predicted by a circuit model [2] and subsequently measured in ASSET [3]. Additional structures with optimized shunt impedance and wakefield performance were fabricated and tested. However, all these structures were damaged during high power processing. This damage has led to the testing of a series of new, shorter, low group velocity structures (the “T” series [4]) which are constant gradient and provide little detuning. Recent high gradient tests performed on these structures were very encouraging as the breakdown

damage was substantially reduced. We have two further series of structures which will incorporate detuning and damping of the dipole modes: standing wave (SW) accelerators which operate in the π mode and travelling wave (TW) accelerators which operate at a $5\pi/6$ phase advance per cell.

The new SW structure consists of 15 cells and will eventually incorporate both detuning of the dipole frequencies and damping of the wake by incorporating a limited number of choke mode cavities in the structure [4]. The TW structures are similar in design to the original DDS series except that they are shorter by a factor of up to 3 and they accelerate the beam with a reduced group velocity (3% or 5% initial group velocity compared to 12% in DDS). This series of accelerator structures is known as the “H series” because they operate at a higher phase advance ($5\pi/6$ compared to $2\pi/3$) which is needed to reduce the group velocity while at the same time preserving the average iris radius. We maintain the average iris radius (radius/accelerating mode wavelength = $a/\lambda \sim 0.18$) in order to keep the wakefield along the bunch (the intra-bunch or short range wake) to acceptable levels. For the NLC bunch the average strength of the short-range wakefield kick is proportional to the -3.8 power of the iris radius.

A comparison of the dipole wakefield band structure for a TW $2\pi/3$ phase advance structure with a π SW detuned structure is presented in the following section. Damping requirements for these structures are discussed. In section 3 we will explore how the kick factors are distributed among the lower 6 dipole passbands (band partitioning).

2 UNCOUPLED ANALYSIS OF TRANSVERSE WAKEFIELDS

The transverse wakefield excited by a particle beam can be decomposed into modes which kick the beam transversely to the axis of acceleration. Here, we use an uncoupled analysis in which we calculate the wakefield at the synchronous frequency using the individual cell kick factors. This analysis is valid to a good approximation for the first few meters behind the driving bunch. At longer distances a coupled mode [6] or spectral function [7] analysis must be used. For an N-cell accelerating structure the envelope of the wakefield at a distance s behind the first bunch we derive as the absolute value of a summation:

$$W(s) = 2 \left| \sum_{n=1}^N K_n \text{Exp} \left[j \frac{\omega_n s}{c} \left(1 + \frac{j}{2Q_n} \right) \right] \right| \quad (2.1)$$

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where for the n^{th} mode, K_n is the transverse kick factor, $\omega_n/2\pi$ is the synchronous frequency and Q_n is the quality factor of the mode. A modal expansion similar to eq. (2.1) is also found in [8]. The kick factor is evaluated as:

$$K_n = \frac{\left| \int_L E_z \text{Exp}[j\omega_n s/c] dz \right|^2}{4 \frac{\omega_n a_n^2}{c} U_n L \left(1 - \frac{v_{gn}}{c}\right)} \quad (2.2)$$

Here, a_n is the radius of the n^{th} iris, L the periodic length of the cell, E_z is the on-axis electric field and U_n is the energy stored per cell in a mode. The kick factor also depends on the group velocity v_{gn} [9] and provided the synchronous phase is close to π then the group velocity dependence will be a negligible correction and it can be ignored. For all DDS structures it has indeed been found to be a small correction (first dipole band modes). However, for the SW and new high phase advance structures this is may no longer be the case.

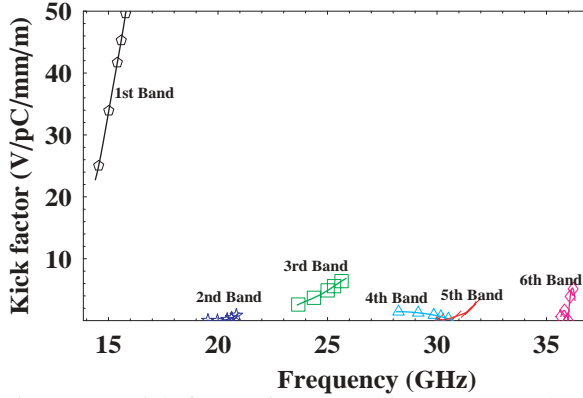


Figure 1. Kick factors in a travelling wave accelerator: DS1 (Detuned Structure). The complete set of 206 kick factors is obtained by interpolation from the calculation of kick factors for 5 cells (shown with dots). The largest kick factors are all concentrated in the first band. The third and sixth bands, although they are almost an order of magnitude smaller than the first, also affect the beam dynamics in the linac. All of these three bands must be detuned.

We calculated the kick factors and wakefields for a representative TW detuned structure known as DS1 and for a 8 SW structures each of which consists of 15 cells and they are both detuned with a 10% bandwidth. The 8 different SW structures effectively make up a 120 cells structure. We require 8 structures as the detuning provided by 15 cells in one structure alone is insufficient.

The results of these calculations, performed with HFSS and GdfidL [10], are shown in Figs 1 and 2 respectively. For the standing wave structure the kick factors are no longer linearly dependent on the synchronous frequency and they are not concentrated in only the first band. The wakefield that results from each of these bands for the travelling wave detuned structure and the standing wave

structure is shown in Fig 3 and 4 respectively. In this calculation we have not included the effects of the finite group velocity of the dipole mode.

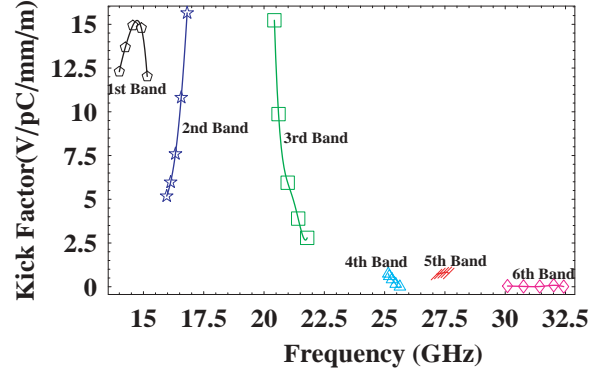


Figure 2. Kick factors in standing wave accelerator design SW1. The complete set of 120 kick factors is obtained by interpolation from the calculation of kick factors for 5 cells (shown with dots). The first three bands kicks are of similar order of magnitude and they all must be damped and detuned. The 4th and 5th bands are an order of magnitude smaller than the first three but they also must be considered in a full analysis of the beam dynamics as they also contribute to BBU instability.

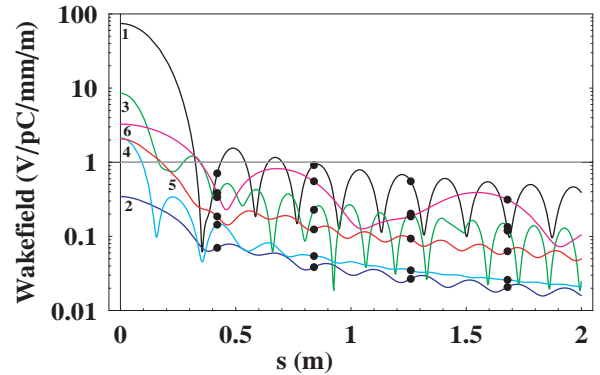


Figure 3. Individual bands, ranging from the first to the sixth of the envelope of the wakefield corresponding to the kick factors of the travelling wave structure given in Fig 1. The dots are positioned at the location of each individual bunch (spaced by 42cm). Four out of a total 191 trailing bunches are shown.

NLC beam dynamics studies [11] indicate that if the wakefield is kept below one, then the BBU instability will tend not to be an issue. The wake at the position of the bunches is shown in Fig 3 for the travelling wave structure and it is clear that the wake remains below unity at these locations and thus BBU is unlikely to be a problem. The 3rd and 6th bands have significant kick factors compared to the first band and these modes were detuned by enforcing an Erf variation to the iris thickness of all cells. The

wakefield for the SW structure shown in Fig 4 reveals that the first three bands are all equally important and consequently they all must be carefully damped. The wake at the position of the first trailing bunch is below unity for all bands apart from the third band. The third band requires additional detuning in order to accelerate the rate of decay of the wake.

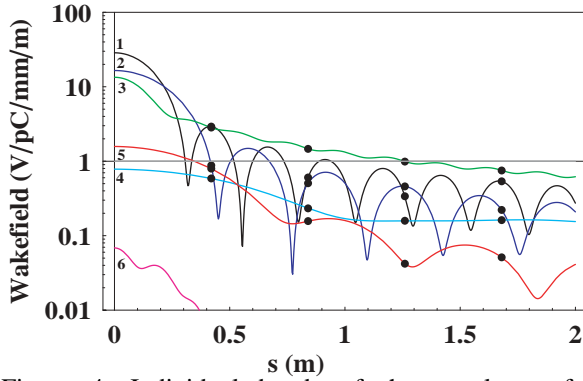


Figure 4. Individual bands of the envelope of the wakefield corresponding to the kick factors of the standing wave structure given in Fig 2.

3 GENERAL PROPERTIES

In order to assess the behaviour of band partitioning as a function of synchronous frequency we used the Fortran code *Transvrs* [12] driven with by a Mathematica input to the data set to calculate the kick factors and synchronous frequencies. The results of this calculation are shown in Fig 5 for a/λ given by 0.229 (a), 0.19 (b) and 0.161 (c), in which the kick factors are calculated for structures with a phase advance ranging from 120 to 180 degrees. The general trend for the first three bands is quite clear, namely, rather independently of the iris dimension, the second and third dipole bands are enhanced at the expense of the first band as the phase advance per cell increases from the initial value of $2\pi/3$. The effect of finite group velocity on the kick factor has been left to a later publication, as until recently the code was unable to incorporate this effect. However, inclusion of the group velocity does not modify our general conclusions on the partitioning of modes.

In conclusion: as the phase advance moves from $2\pi/3$ toward π the first band kick factors become smaller and the second and third become larger; at π phase advance (SW structure) all three are of comparable size. Therefore, the first three bands of the SW structure should be damped and detuned. For the $5\pi/6$ TW structure the first band has largest kick factors, but a second and third are more significant than in $2\pi/3$. Further studies are in progress concerning the damping and detuning of the these three bands (and higher bands) for the SW and the $5\pi/6$ TW structures.

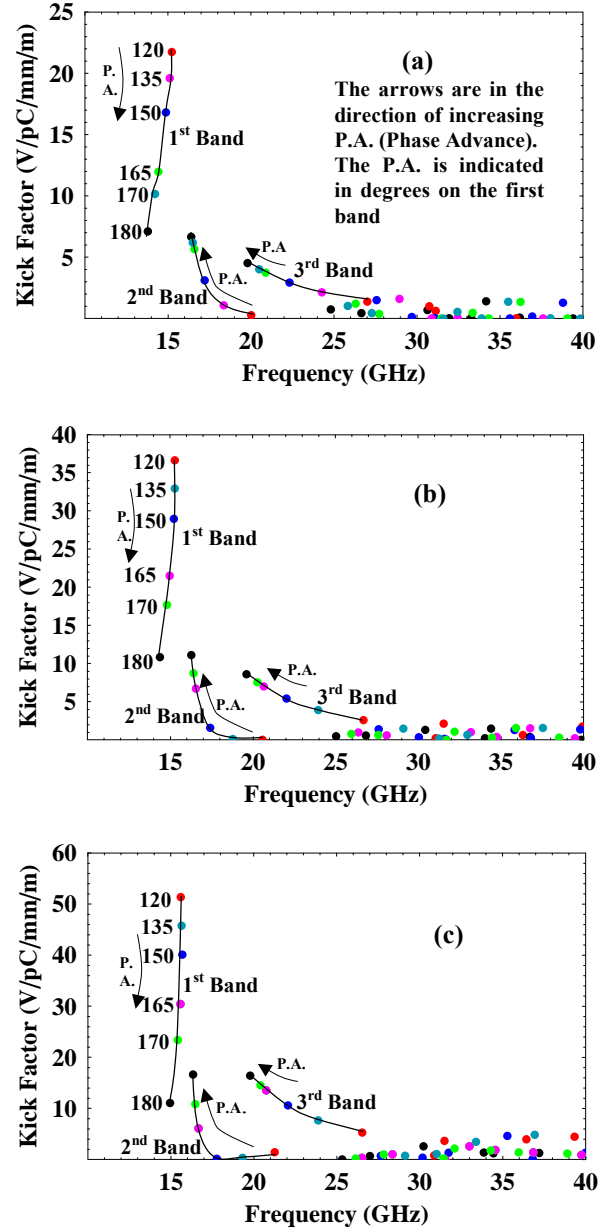


Figure 5. K_n as a function of synchronous frequency for several irises radii: (a) 6mm, (b) 5 and (c) 4.23 mm.

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