

OPTIMIZATION OF TWO-CELL CAVITIES FOR THE W AND H WORKING POINTS OF THE FCC-ee CONSIDERING HIGHER-ORDER MODE EFFECTS

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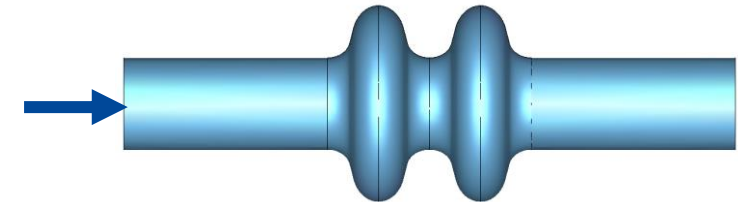
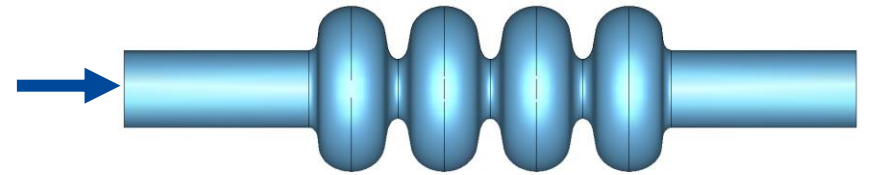
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Introduction

- The lepton collider of the Future Circular Collider (FCC-ee) aims at conducting precision measurements on the Z, W, and H bosons and the top quark
- The present RF baseline considers four-cell 400 MHz cavities for the W and H working points
- A detailed study of the W working point has shown strong higher-order mode (HOM) effects in the four-cell cavities [1]
- In this study, a two-cell cavity is designed as an alternative scenario for the current W- and H-RF setups with special attention paid to HOM aspects



[1] S. Gorgi Zadeh, *Accelerating cavity and higher order mode coupler design for the Future Circular Collider*, PhD thesis, Universität Rostock, 2020. <http://purl.uni-rostock.de/rosdok/id00003023> - open access

Quantities of Interest

- The primary quantities of interest are the impedances of higher-order modes (HOM)
 - HOM Longitudinal Impedance $|Z_L|$ and
 - HOM Transverse Impedance $|Z_T|$

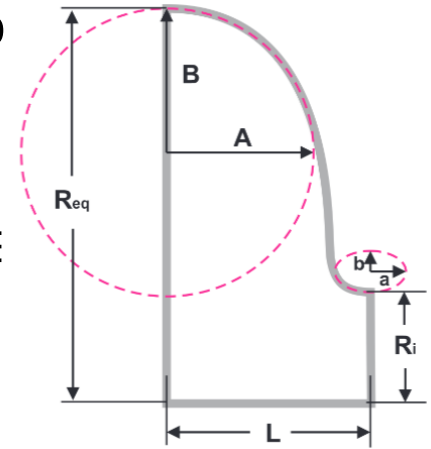
$$Z_L = \frac{1}{c} \int_{-\infty}^{\infty} w_{\parallel}(r, s) e^{-\frac{j\omega s}{c}} ds$$
$$Z_T = \frac{-j}{c} \int_{-\infty}^{\infty} w_{\perp}(r, s) e^{-\frac{j\omega s}{c}} ds$$

- Secondary quantities of interest are these quantities of the fundamental mode (FM):
 - E_{pk}/E_{acc}
 - B_{pk}/E_{acc}

where E_{pk} , B_{pk} and E_{acc} represent the peak electric field on the surface of cavity, peak magnetic field on the surface of the cavity, and accelerating field, respectively

Optimization Method

- In order to reduce the search space for this study, the equator and iris ellipses were assumed to have a circular shape, i.e. $A = B$ and $a = b$
- A parameter sweep in 4D was carried out considering $A \in [50, 110]$, $a \in [20, 70]$, $L \in [160, 190]$, and $R_i \in [150, 160]$, where all dimensions are in mm
- The HOM and FM quantities of interest are combined to form objective functions using the weighted exponential sum method



$$F_{obj} = \left(\sum_i^m (w_i f_{i,n})^p \right)^{\frac{1}{p}} [2]$$

where w_i represents weights, p represents the norm order and n is used to indicate that the objective functions are normalised. w and p are both set to 1 in this study

[2] R.T. Marler and J.S. Arora, *Survey of multi-objective optimization methods for engineering*, *Structural Multidisciplinary Optimization* 26,369–395 (2004), DOI 10.1007/s00158-003-0368-6

Objective Functions

$$\begin{aligned}
 & \min_{L, R_i, A=B, a=b} (F_{\text{FM}}, F_{\text{HOM}}) \\
 & \text{s. t. } f_{\text{FM}}(R_{\text{eq}}) = 400.79 \text{ MHz}
 \end{aligned}$$

$$F_{\text{HOM}} = \frac{\text{Max}(\text{Real}\{Z_{L(f>450 \text{ MHz})}\})}{0.3 \text{ k}\Omega} + \frac{\text{Max}(|Z_{T(f>650 \text{ MHz})}|)}{3 \text{ k}\Omega/\text{m}}$$

$$F_{\text{FM}} = \frac{\frac{E_{\text{pk}}}{E_{\text{acc}}}}{2.2} + \frac{\frac{B_{\text{pk}}}{E_{\text{acc}}}}{5 \frac{\text{mT}}{\text{MV/m}}}$$

FM frequency tuning

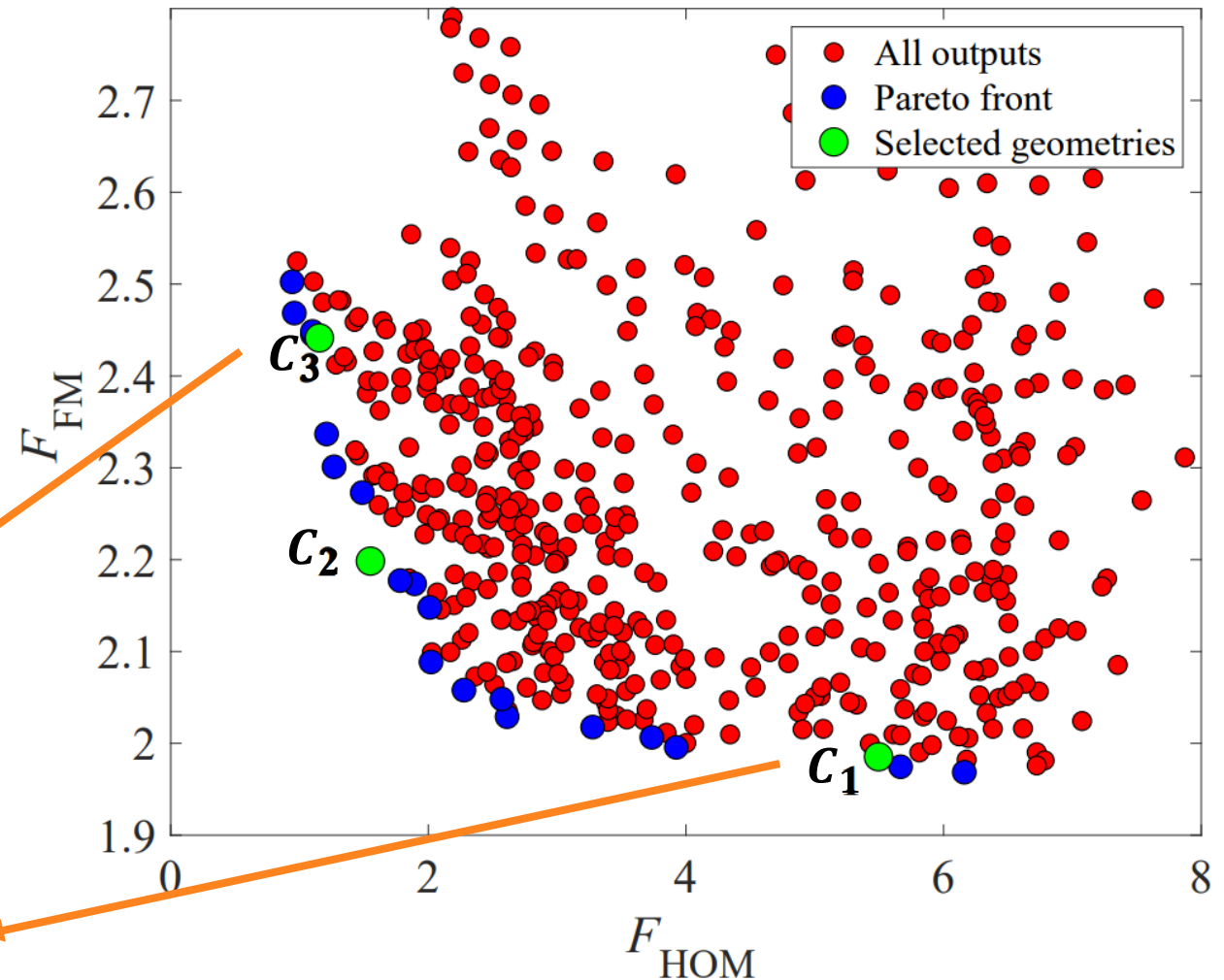
- $E_{\text{pk}}/E_{\text{acc}}$ is normalized by 2.2 and $B_{\text{pk}}/E_{\text{acc}}$ by $5 \frac{\text{mT}}{\text{MV/m}}$
- The maximum longitudinal impedance peak above the FM is normalized to 0.3 k Ω , and the maximum transversal impedance peak above the frequency of the first two dipole passbands is normalized to 3 k Ω/m , considering a wake length of 50 m

A Pareto distribution of the two objective functions

- The Pareto front of this optimization with the two objective functions F_{HOM} and F_{FM} is highlighted by the blue markers
- Three geometries are selected from the Pareto front. Geometry 1 (C_1) favors F_{FM} , Geometry 3 (C_3) favors F_{HOM} , and Geometry 2 (C_2) is a sample in the middle range

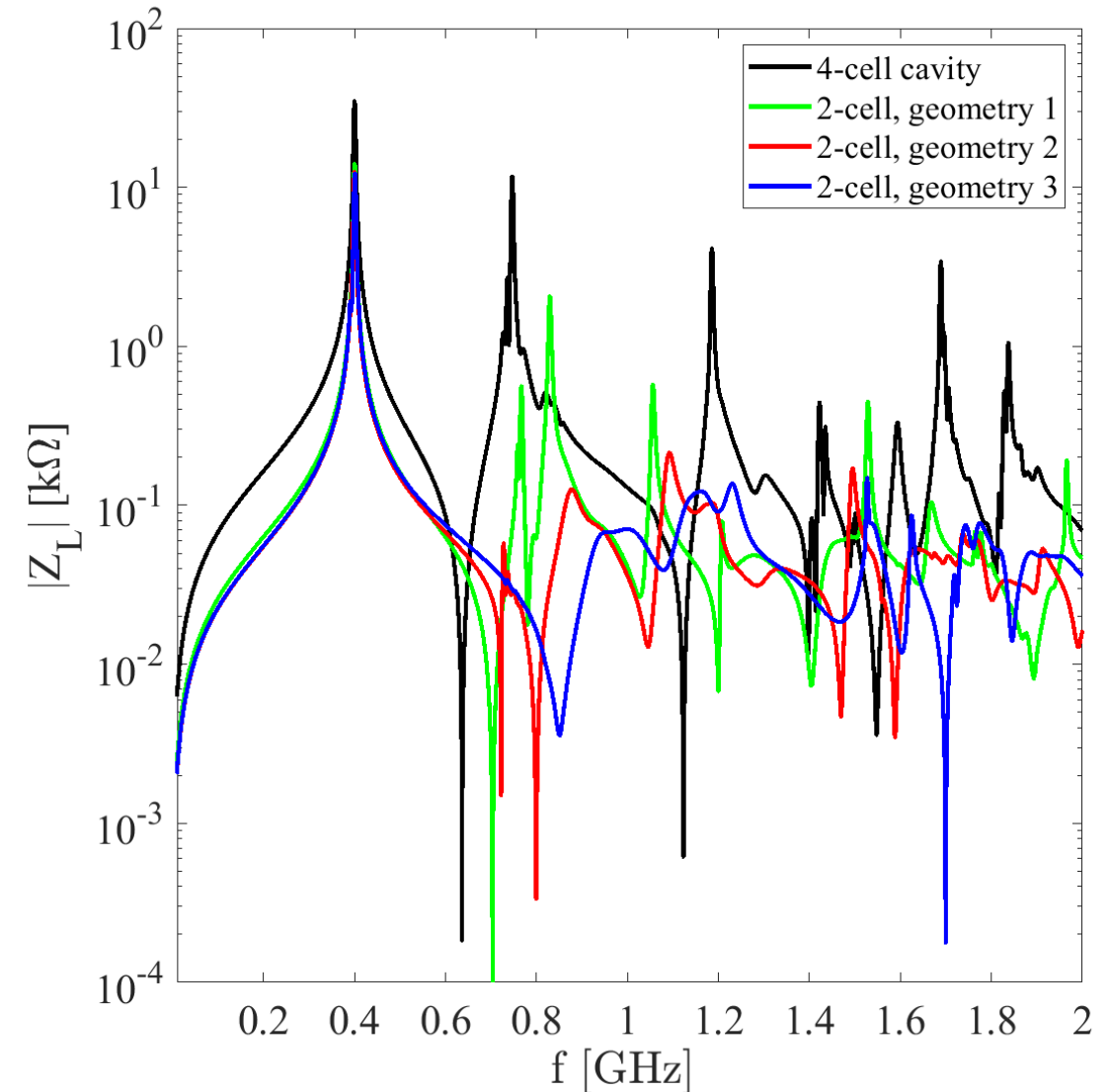
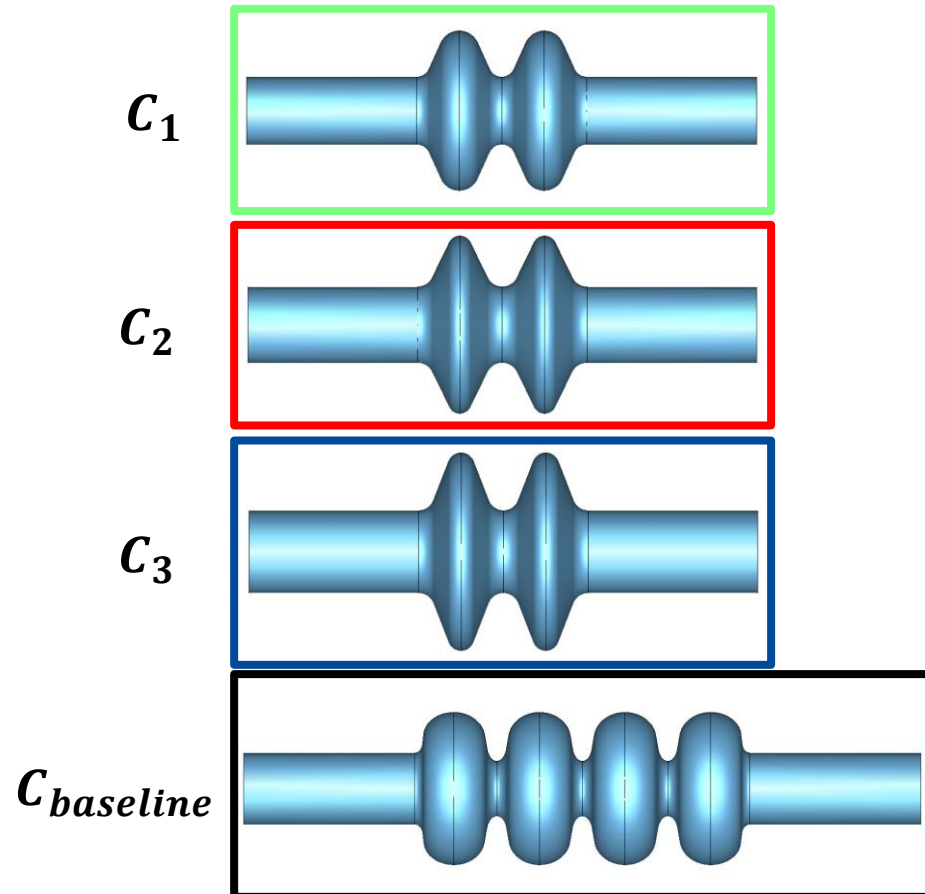
More in favor of F_{HOM}

More in favor of F_{FM}

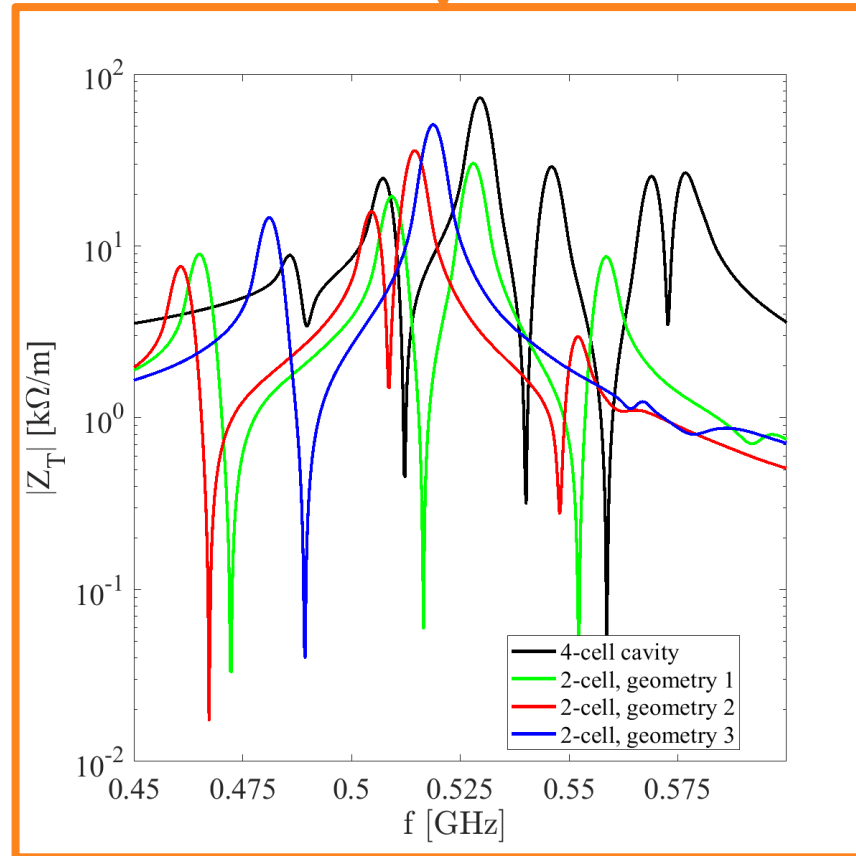
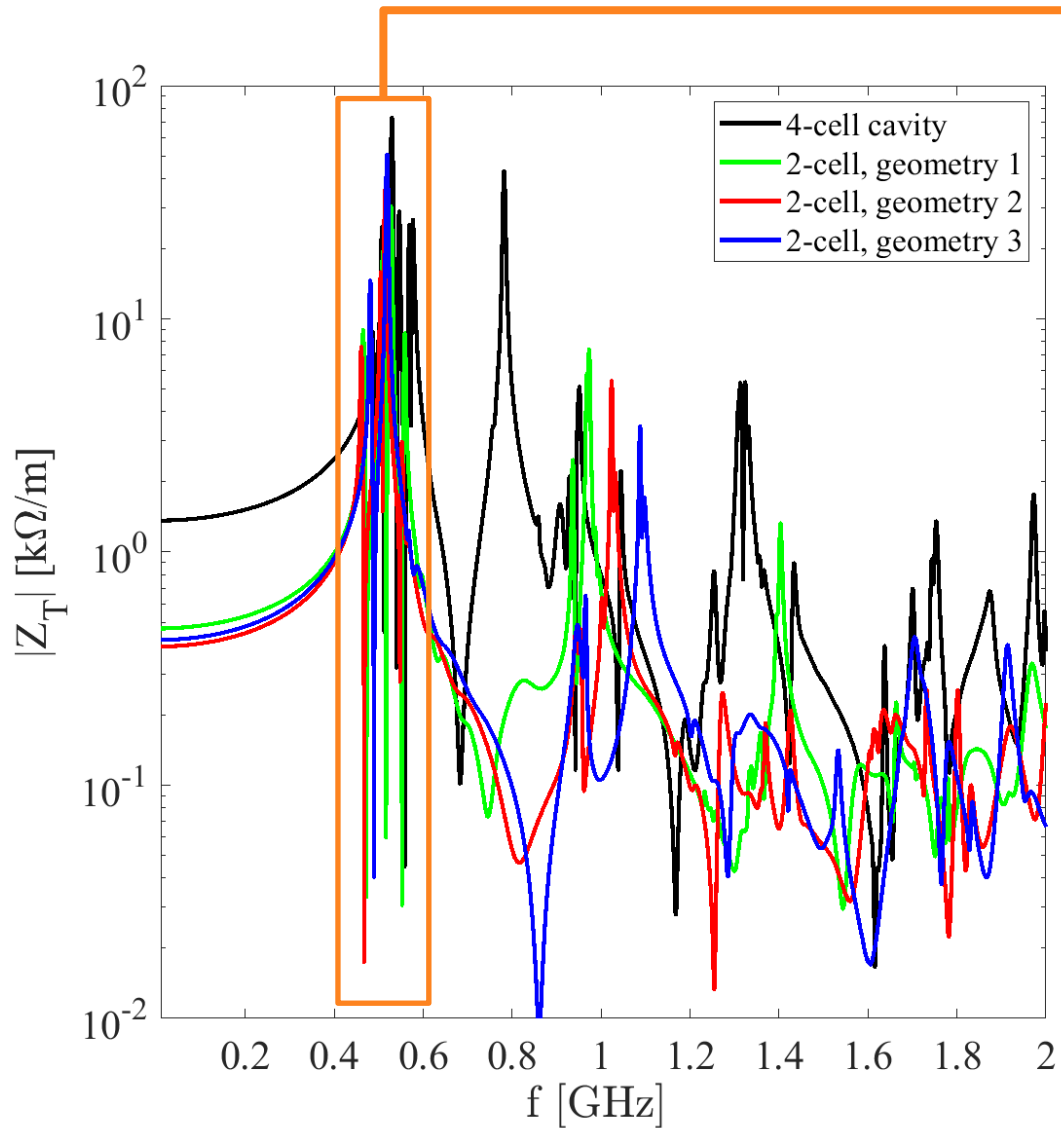


Longitudinal Wakefield Impedance Plots for Selected Cavities

- The longitudinal wakefield impedance plot shows a strong reduction in the HOM impedance for the selected two-cell cavities, especially for C_3



Transversal Wakefield Impedance Plots for Selected Cavities



From the zoomed area, it can be seen that geometry 3 has less number of peaks which simplifies the design of HOM couplers

Result Summary

Parameter	$k_{\parallel}^*$ [V/pC]	$k_{\perp}$ [V/pC/m]	$f_{TE111} - f_{TM010}$ [MHz]	R_{sh}/Q_{FM} [Ω]	E_{pk}/E_{acc}^{**}	B_{pk}/E_{acc} [mT/(MV/m)]
C_1	0.02678	0.5401	66.01	165.8	2.03	5.3
C_2	0.017582	0.4242	60.21	147.2	2.12	6.2
C_3	0.01504	0.4564	80.51	144.7	2.46	6.6
$C_{baseline}$	0.048025	0.82	85.21	411.3	2.0	4.2

*A bunch length of 50 mm was used for the calculation of the HOM loss factors, ** E_{acc} is calculated from V_{acc} with a length of $n_{cell} \times 374$ mm.

The dimensions are given in mm

Var	C_1	C_2	C_3	$C_{baseline}$
A/A_e	90	50	50	135.44/133
B/B_e	90	50	50	114.9/102
a/a_e	60	70	60	43.5/34
b/b_e	60	70	60	71.19/46
$R_i/R_{i,e}$	150	160	155	120/156
L/L_e	190	180	160	187/171.5
R_{eq}	355.042	374.924	372.642	333.182
α/α_e	114.5°	116.1°	111.3°	100°/96.9°

