

The design optimization of the dielectric assist accelerating structure for better heat and gas transfer

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Outline

- Introduction:
 - Review of the dielectric-assist accelerating (DAA) structure
 - Expected impact of the DAA cavity
- Problems of the DAA cavity and Solution
- Simulation method and result
- Conclusion

Introduction

- ◆ Figure of merit of an accelerating cavity:

$$Q_0 = \frac{\omega U}{P_{\text{loss}}}$$

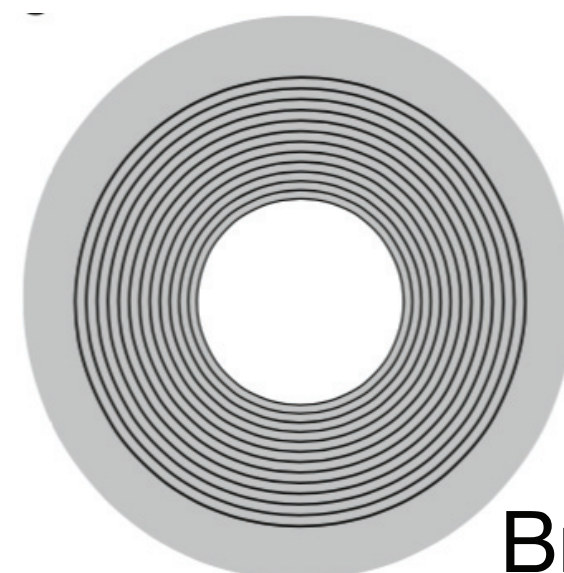
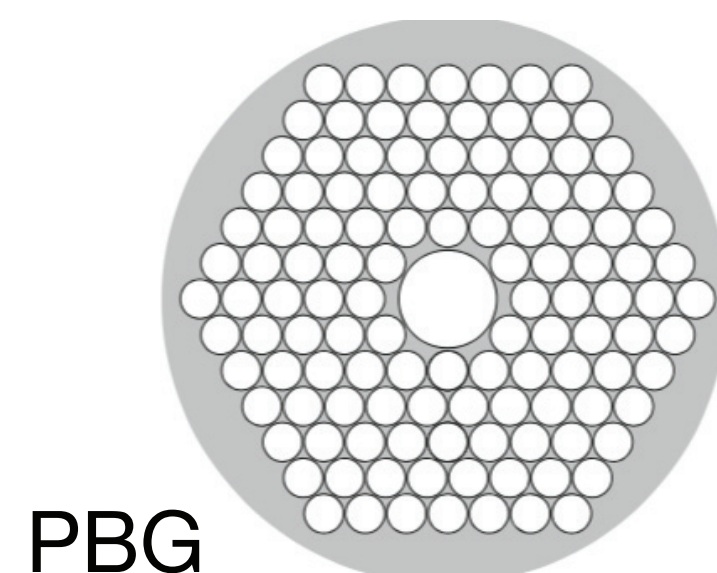
- ◆ For conventional NC cavity: $Q_0 \sim 10^4$ (@RT)

- ◆ 20MV/m → Ploss=40MW/m

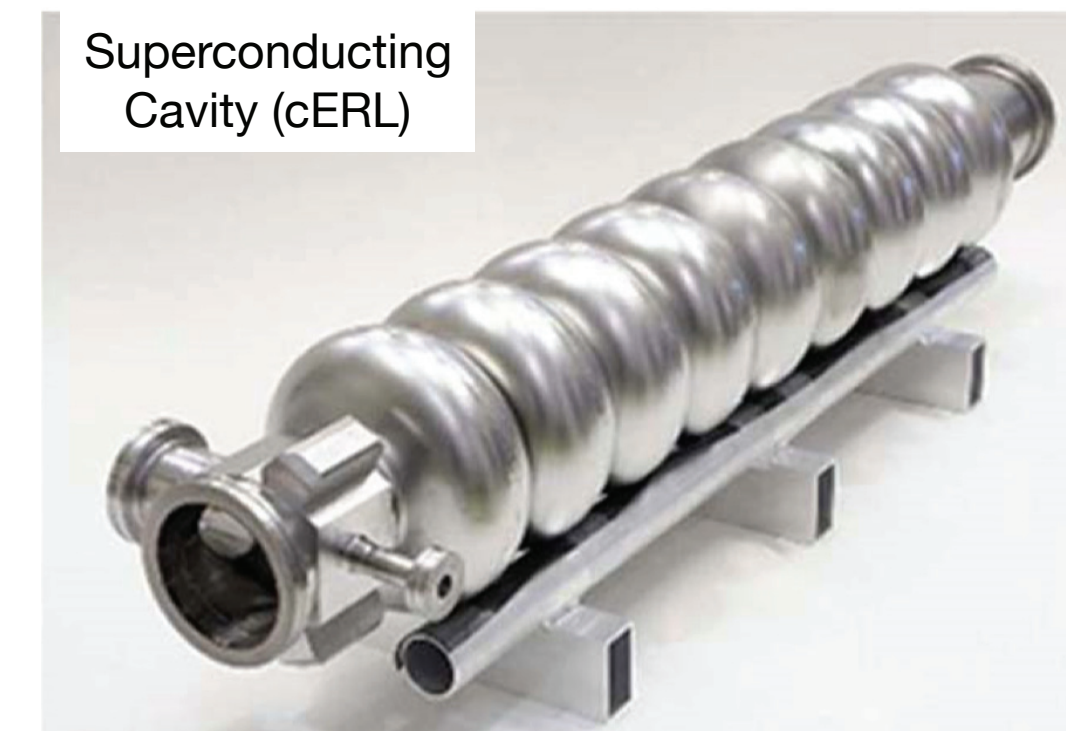
- ◆ For SC cavity: $Q_0 \sim 10^{10}$ (@2K)

- ◆ 20MV/m → Ploss=40W/m

- ◆ For dielectric structure:



Skorobogatiy, Maksim. "Resonant Biochemical Sensors Based on Photonic Bandgap Waveguides and Fibers.", 2010. 43-72.



If we can confine RF mostly in the dielectrics,
Q0 is determined by material loss, $\tan \delta$.

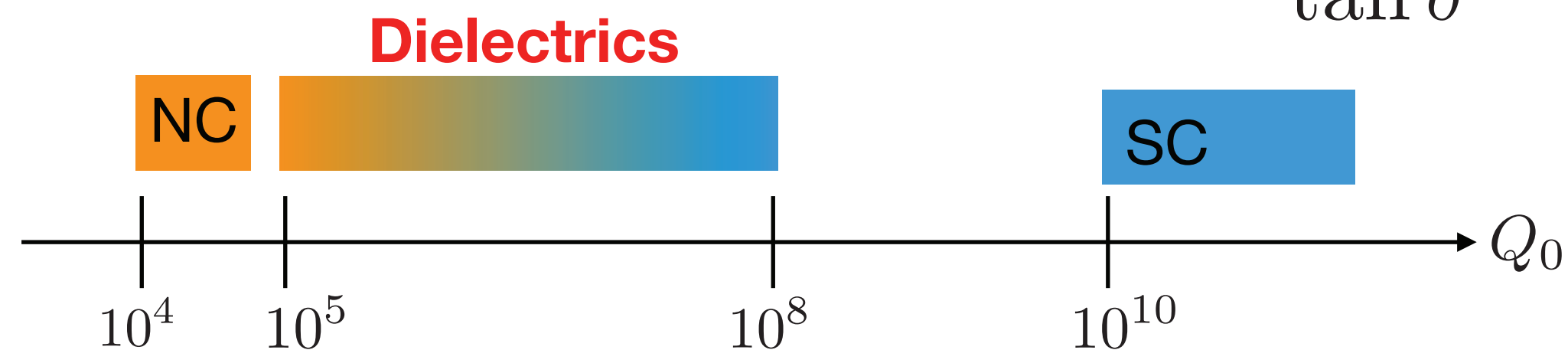
Introduction

- ♦ Dielectric cavity has potential of high Q value

Ex) sapphire has low-loss tangent:

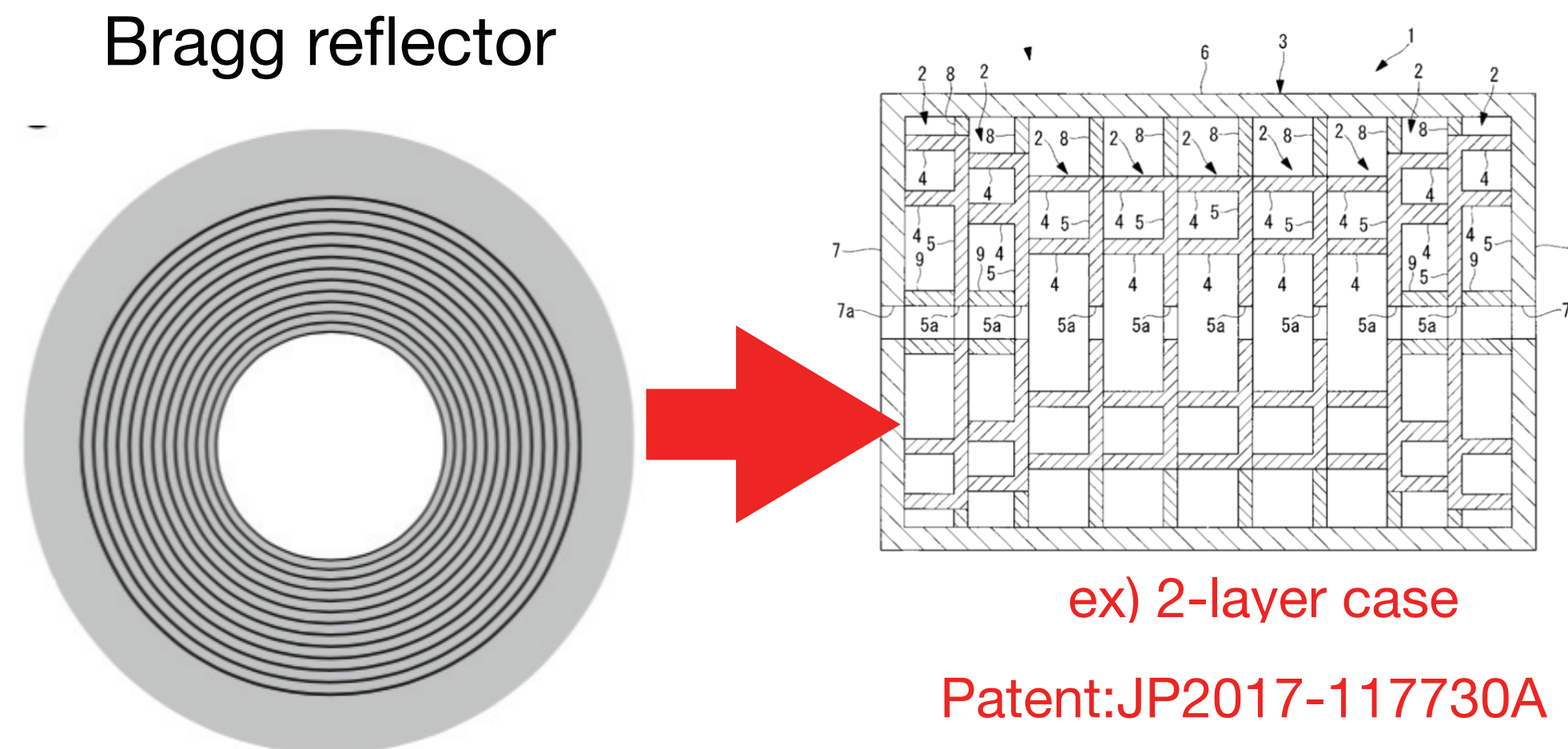
$$\tan \delta < 10^{-8} (@T < 50K) \quad Q_0 \sim \frac{1}{\tan \delta} \sim 10^8$$

Braginsky, V. B., V. S. Ilchenko, and Kh S. Bagdassarov
Physics Letters A 120.6 (1987): 300-305



- ♦ Optical fiber

► Dielectric-assist accelerating (DAA) structure



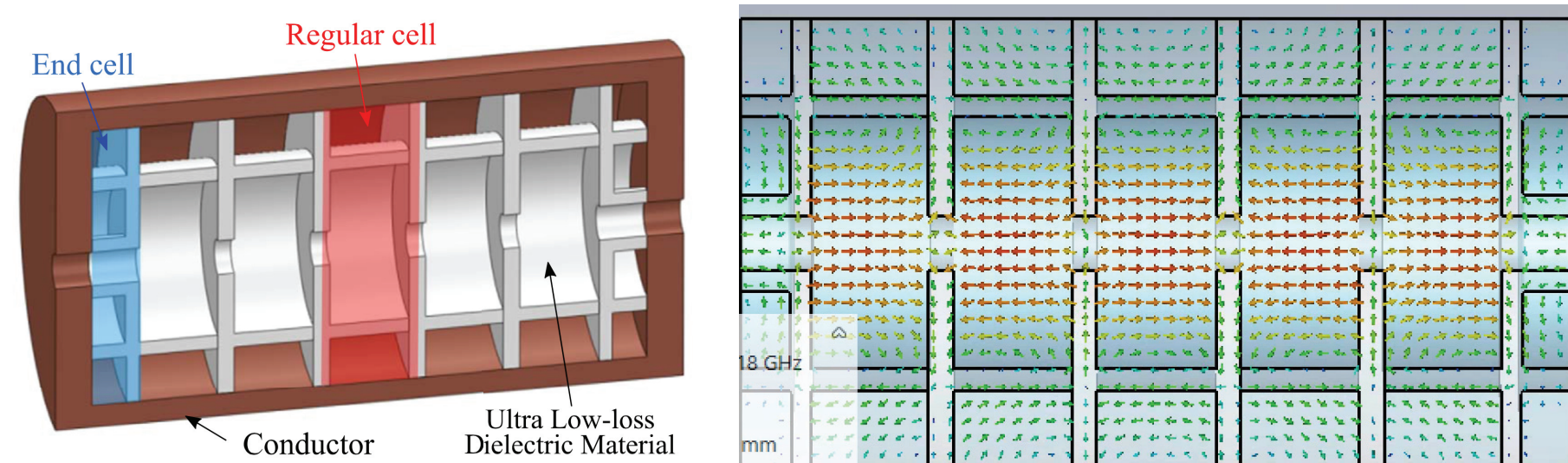
$$Q_0 > 10^7 (@T < 100K, 3Layers)$$

$$Q_0 \sim 10^5 (@RT, 1Layers)$$

Dielectric-Assist Accelerating Structure

JP2017-117730A, International patent

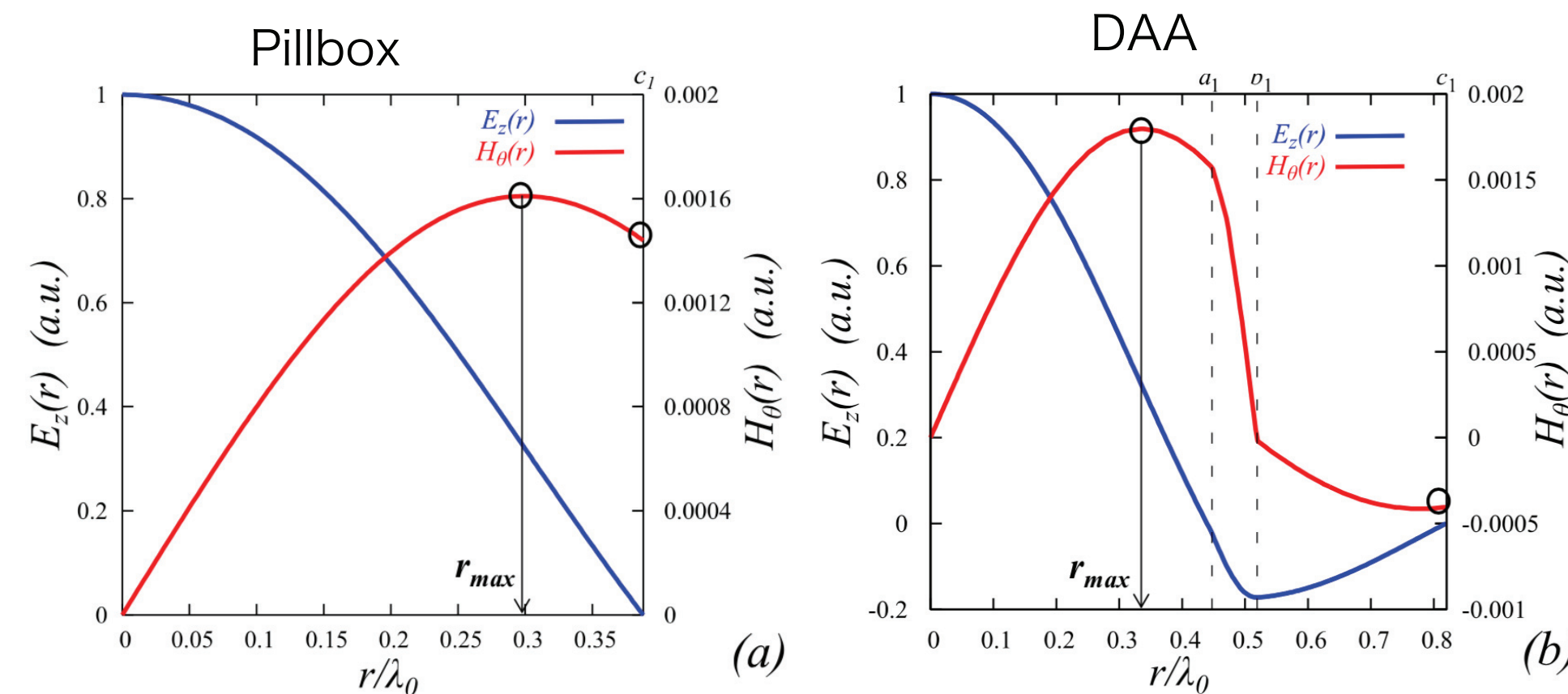
D. Satoh et al. (2016)



Center-field-enhanced TM026

$$Q_0 = \frac{\omega U}{P_{\text{tot}}}$$

$$P_{\text{tot}} = \underbrace{\frac{R_S}{2} \int_S |H|^2 dS}_{\text{Wall loss}} + \underbrace{\frac{\omega}{2} \epsilon_r \epsilon_0 \tan \delta \int_V |E|^2 dV}_{\text{Dielectric loss}}$$



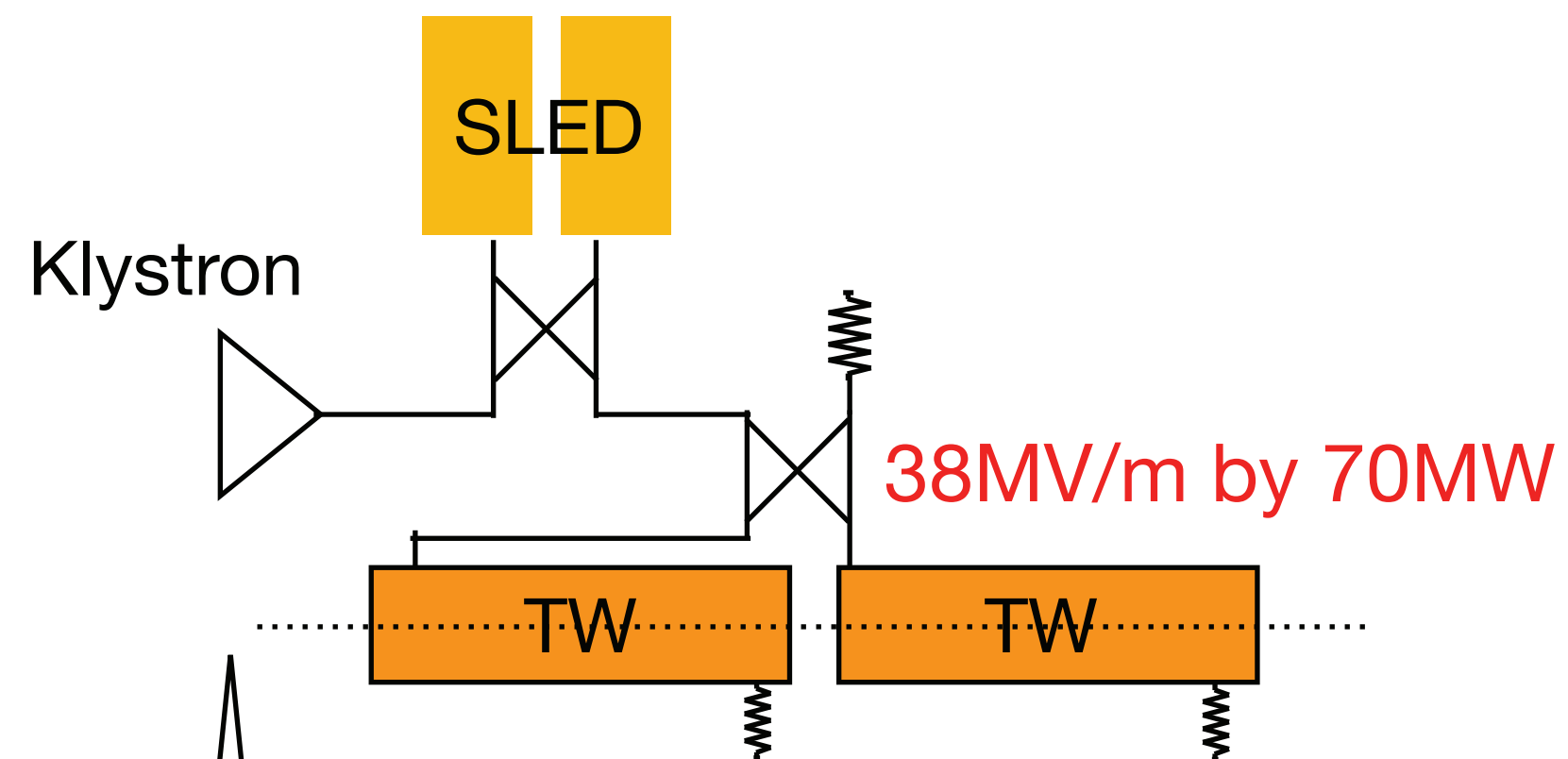
Choose a low loss
Dielectric material
 $\tan \delta = 6 \times 10^{-6}$
@RT

- ▶ Even at room temperature, $Q_0 \sim 10^5$
- ▶ x10 Q0 improvement is important!

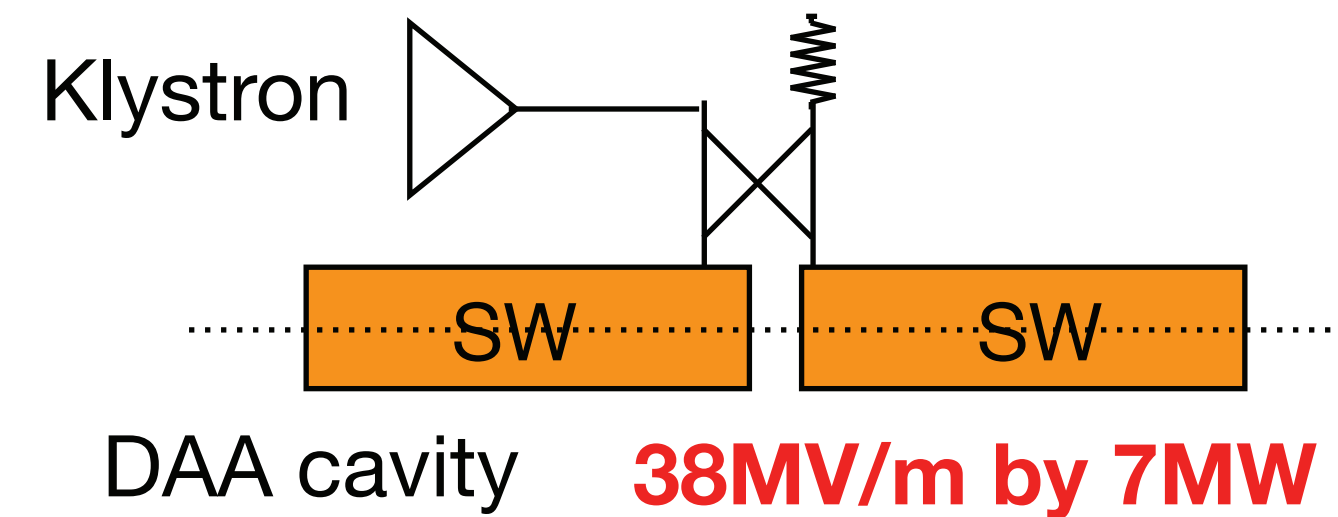
DAA accelerator does not need Pulse Compressor.

► Possibility of longer flat top!

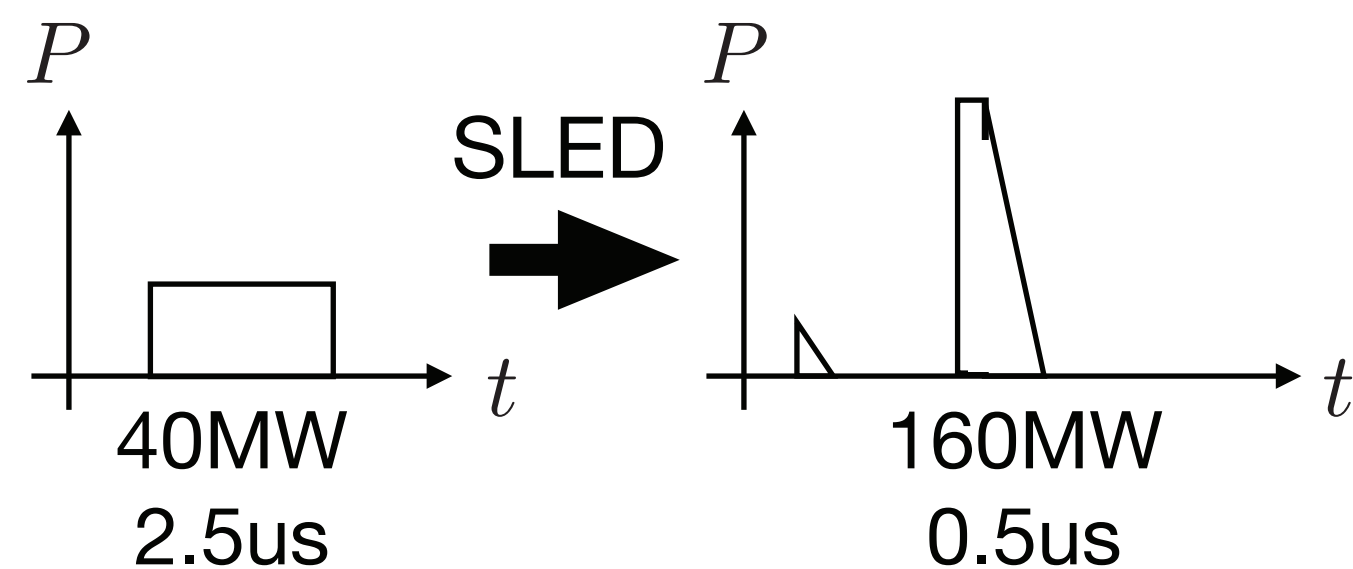
Ex) SACLA, Japan
Klystron + Pulse compressor + TW tube



Klystron + DAA cavity

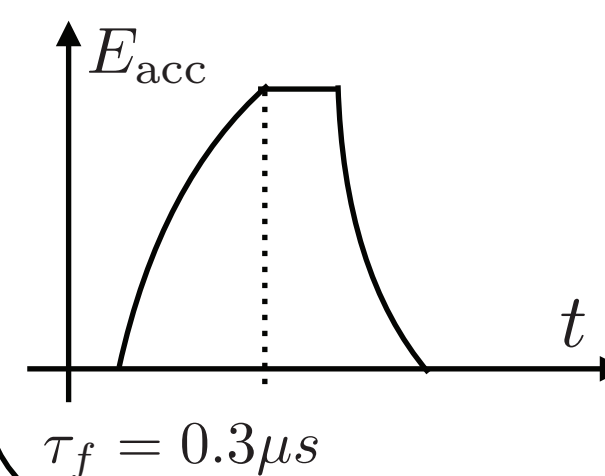


Pulse Compression

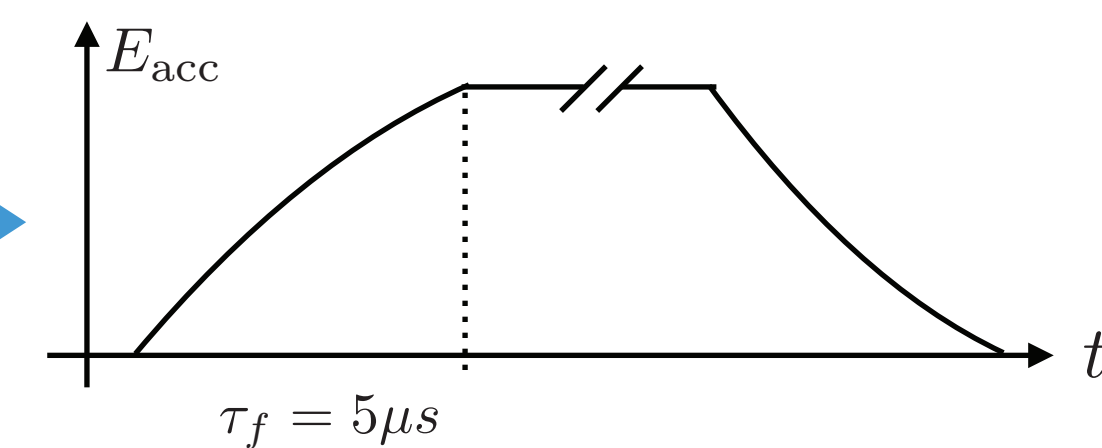


Flat top

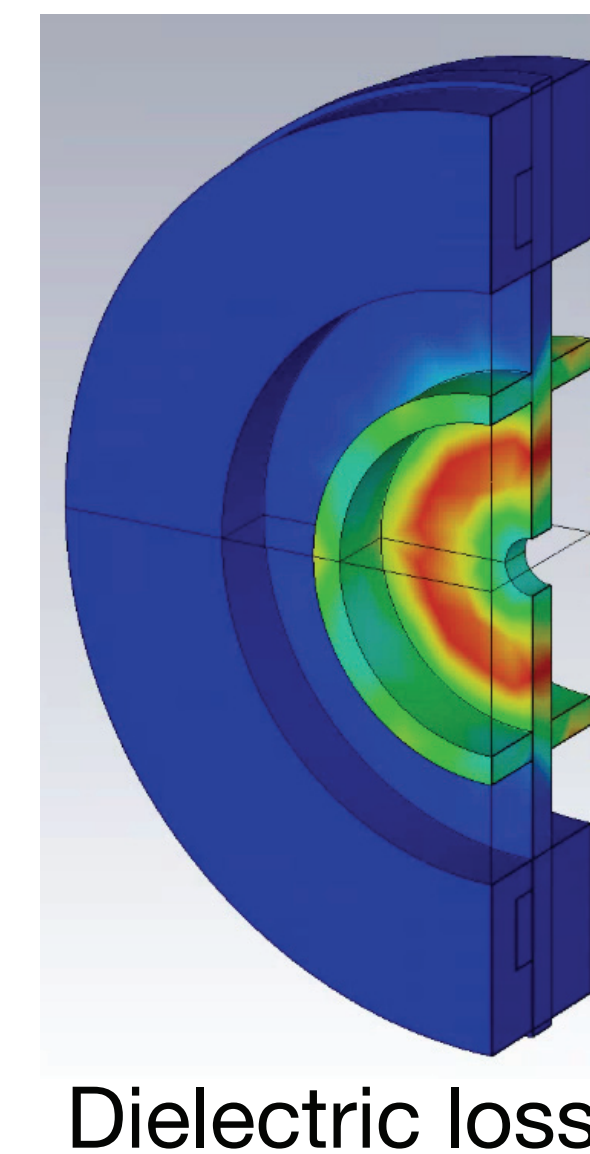
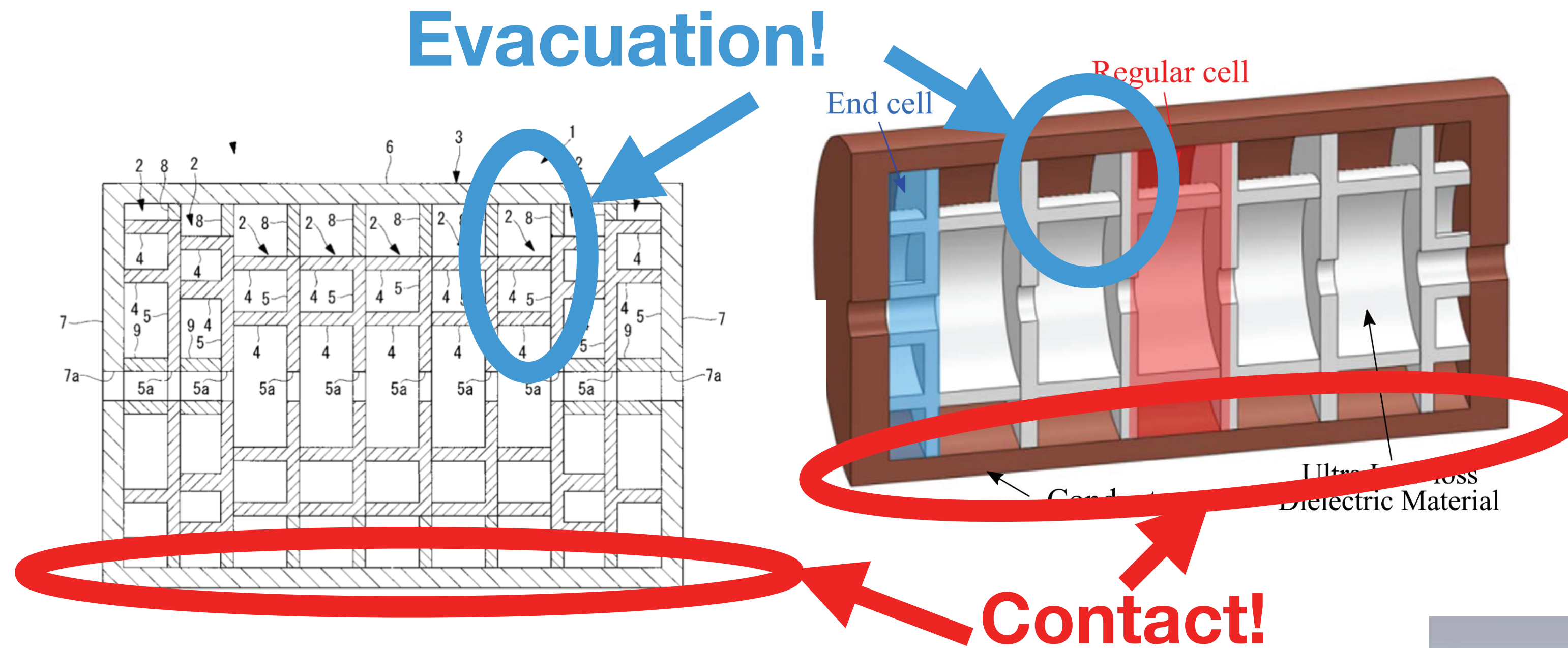
$$\Delta t = 0.2 [\mu s]$$



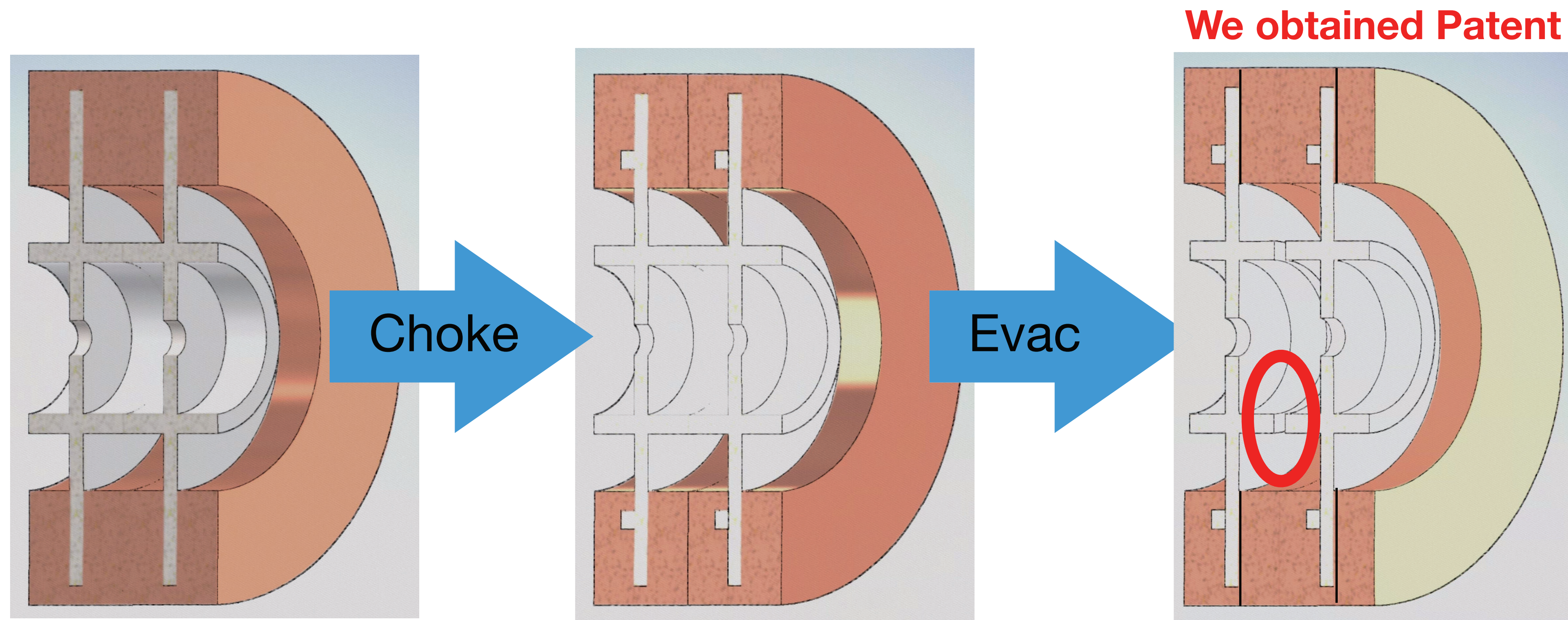
Longer flat top?



Problems of the DAA cavity



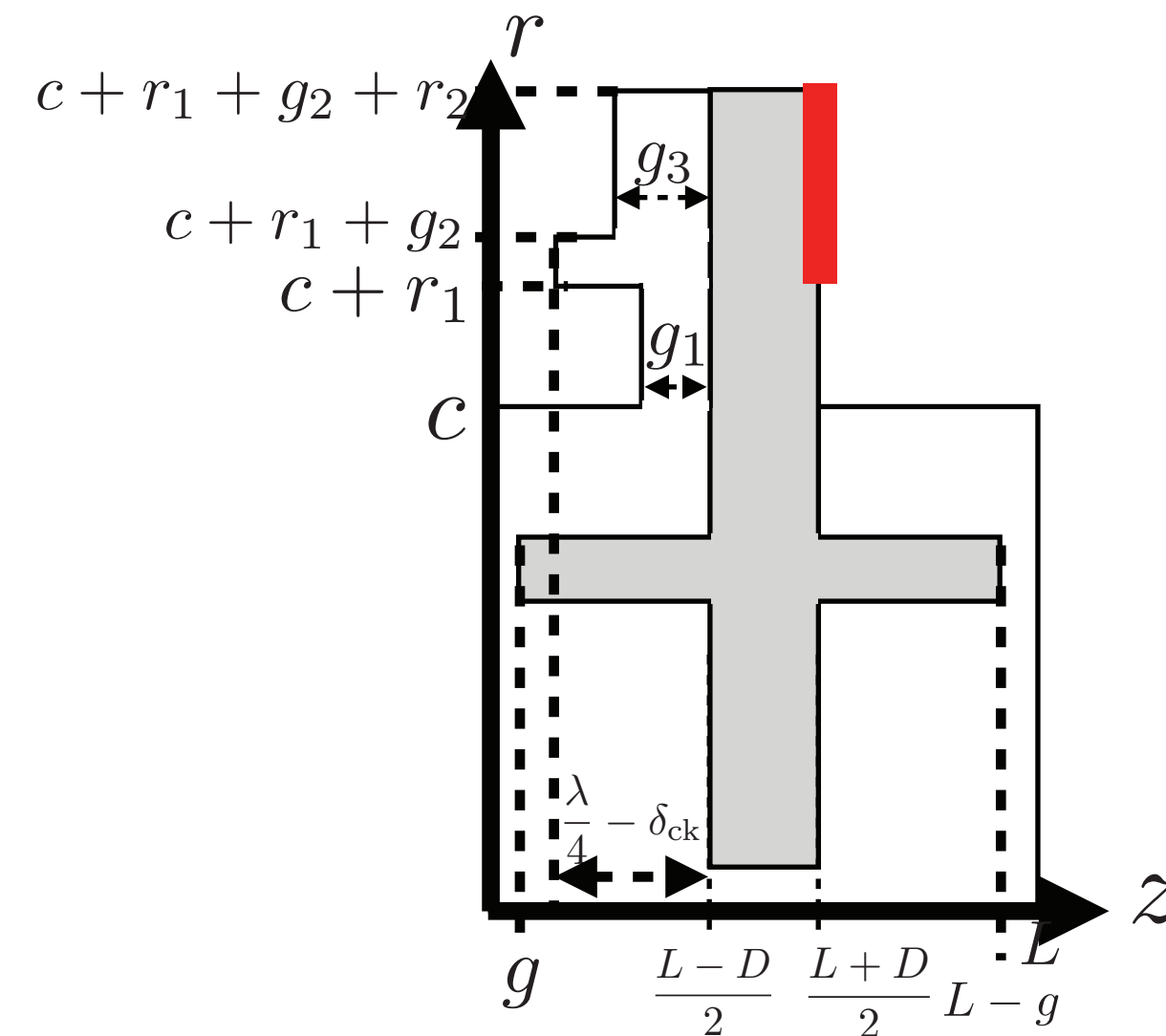
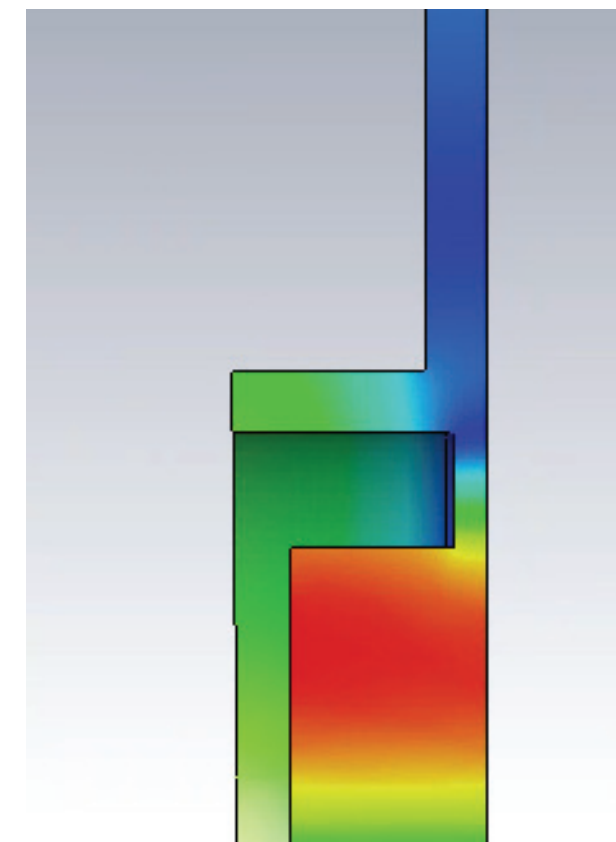
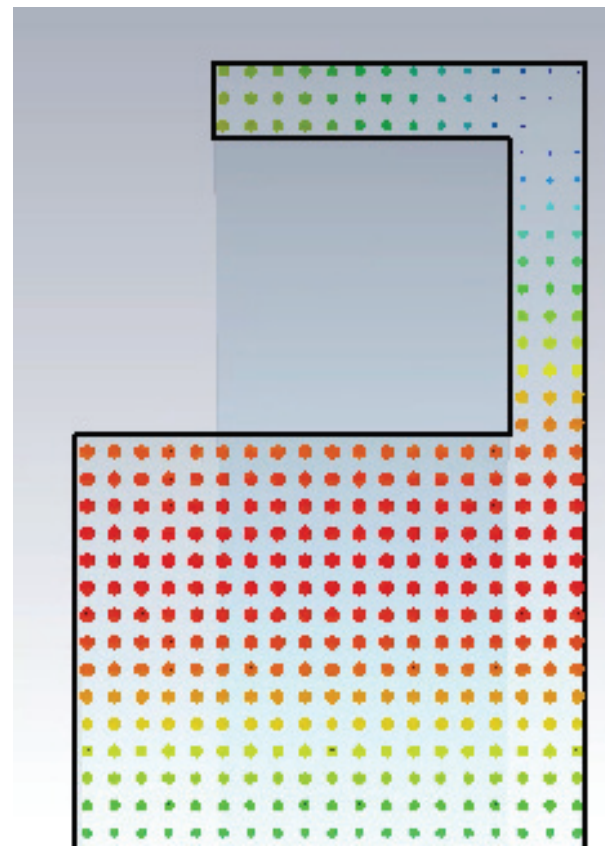
The simple solution to problems



- ◆ The stacked structure ► longer standing wave tube
- ◆ Ceramics are fixed to the copper ring ► gap between ceramics
- ◆ Evacuation from beam hole in any number of layers

Simulation method and result

Ex) Pillbox with choke
Magnetic Field

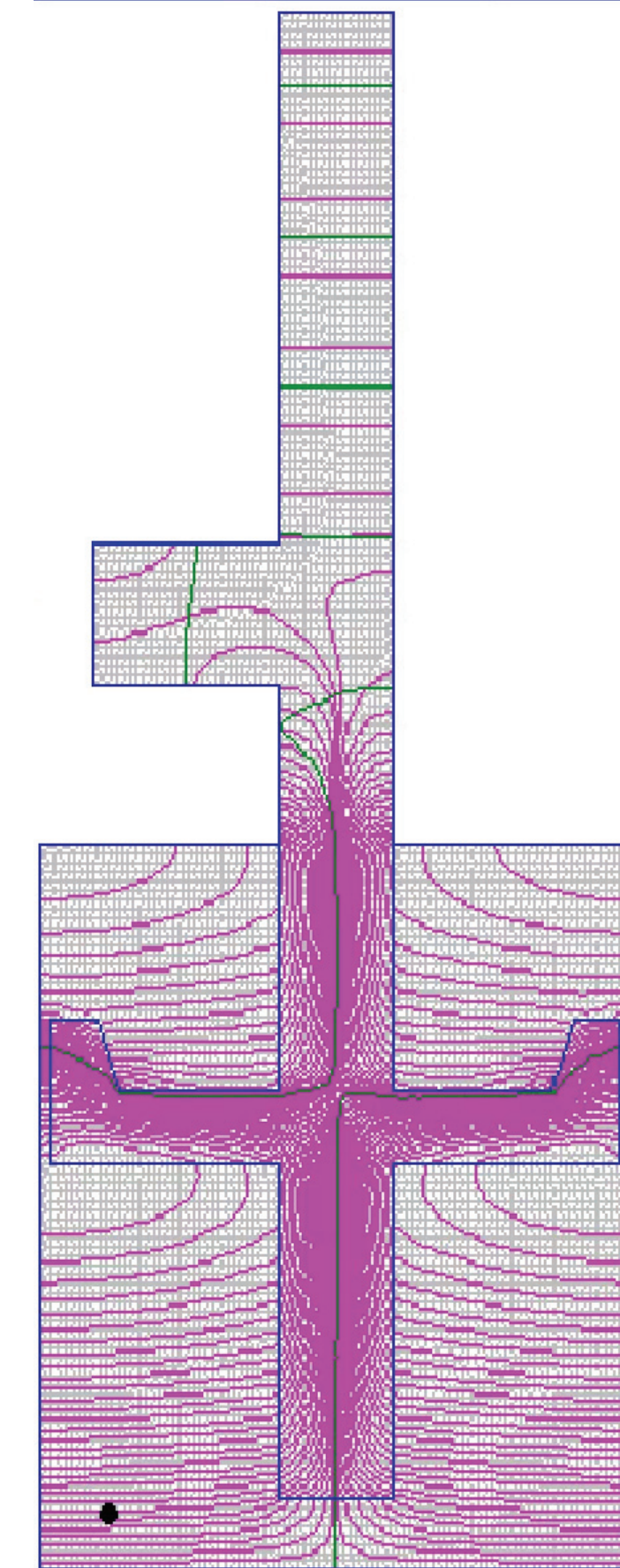


- ♦ At the junction the wall current should be zero.

$$I_{\text{rad}} \equiv \int_{c+r_1}^{c+r_1+r_2+g_2} dr H \Big|_{z=\frac{L+D}{2}} - 0$$

Method:

1. Using SuperFish, we calculate configurations in the parameter space of r_1 , g_2 , δ_{ck} .
2. Choose the configurations with higher Q_0 value in top 10%.
3. Choose the configuration with lowest I_{rad} .



Gap:
1mm

$$Q_0 = 1.21 \times 10^5$$

$$I_{\text{rad}} = 0.175[A]$$

- 8% Q_0 decrease per 1mm separation of adjacent cells

Conclusion

- ◆ The DAA structure provides $Q0 \sim 10^5$ at room temperature, and can work without a pulse compressor.
- ◆ Since the contact between the ceramics and copper cavity has not been considered, we propose solutions to solve both the contact and evacuation.
- ◆ We show a solution to mitigate the problem of the thermal contact and evacuation from the side room.

In future work,

- ✱ After the fabrication of the new design, we need to measure the thermal resistance of the contact.
- ✱ We will consider the effect of the wakefield and the effect of the radial transmission line to reduce them.
- ✱ We need to mitigate the multipactoring between the narrow gaps in the cavity by coatings.