



# Low-Dispersion Wake Field Calculation Tools

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- Introduction
- Enlarged stencil for 3D curl equation
  - Numerical dispersion & stability
  - Indirect integration for 3D wake field calculations
- Potential formalism in cylindrical symmetry
  - Numerical dispersion & stability
  - Conformal scheme vs. staircasing
- Numerical examples and comparisons
- Conclusions

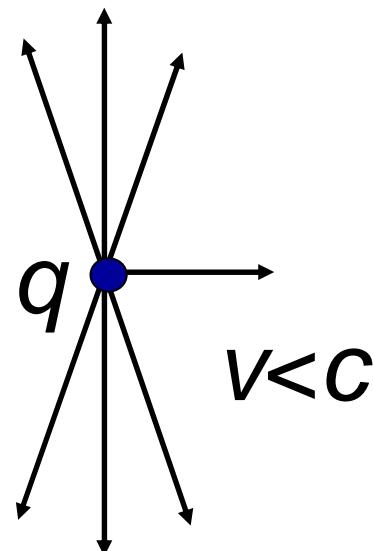


- Wake fields are caused by the **interaction of a charged particle beam with the surrounding vacuum chamber in the accelerator**
- no fields in front of a relativistic beam
- no wake fields in a smooth circular PEC-pipe
- If the pipe is not smooth and/or not perfectly conducting, a wake is created
- Wake field is a **time-domain quantity**
- Wake potential is defined as

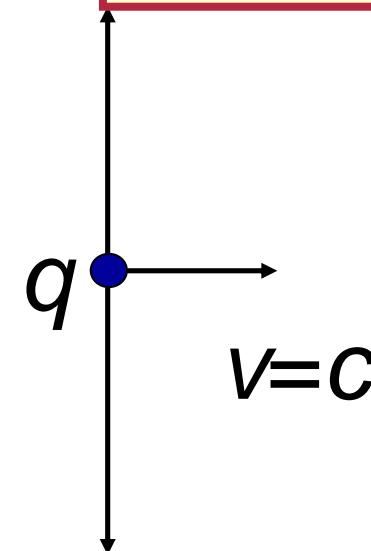
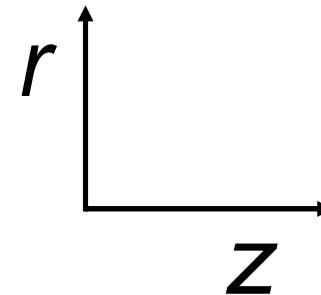
$$W_{||}(0, s) = - \int_{-\infty}^{\infty} E_z(z, 0, \frac{s+z}{c}) dz$$

- rigid beams assumed in calculations (wake fields do not perturb the bunch)
- no transversal variation of the beam
- beam propagates along the  $z$ -axis

$$E_r = \frac{q}{2\pi\epsilon_0 r} \delta(z - ct)$$



Lorentz contracted fields  
with angular spread



Ultrarelativistic limit: pancake  
in free space and in smooth pipe



# Methods in 2D and in 3D

2D

$$\Phi(z, r, t) = \int_0^r r' E_z(z, r', t) dr'$$

$$\frac{\partial^2 \Phi}{c^2 \partial t^2} = \frac{\partial^2 \Phi}{\partial z^2} + \frac{\partial^2 \Phi}{\partial r^2} - \frac{1}{r} \frac{\partial \Phi}{\partial r}$$

3D

$$\epsilon \frac{\partial \vec{E}}{\partial t} = \nabla \times \vec{H}$$

$$\mu \frac{\partial \vec{H}}{\partial t} = -\nabla \times \vec{E}$$

$$\epsilon \frac{\partial E_z}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} (r H_\theta)$$

$$\epsilon \frac{\partial E_r}{\partial t} = - \frac{\partial H_\theta}{\partial z}$$

$$\mu \frac{\partial H_\theta}{\partial t} = \frac{\partial E_z}{\partial r} - \frac{\partial E_r}{\partial z}$$



Second part of the talk  
First part of the talk

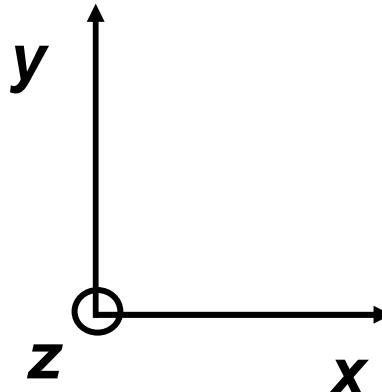
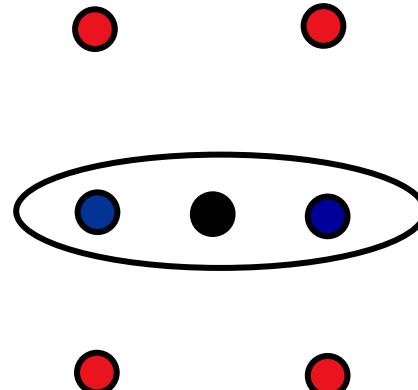


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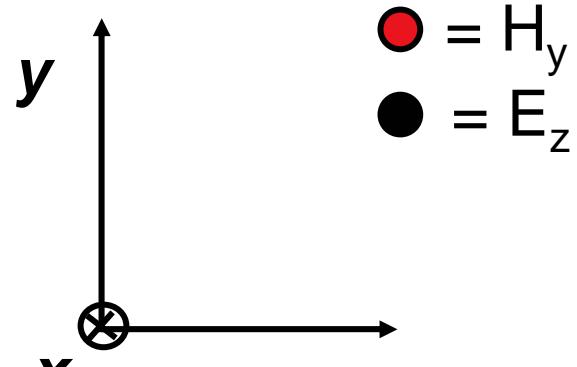
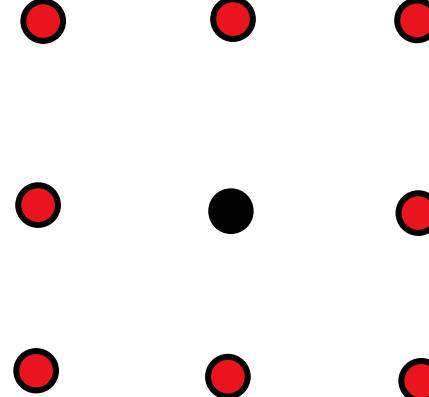
# Enlarged Stencil, 3D



Consider computing the  $x$ -derivative of the  $H_y$ -component in the  $E_z$ -component update equation:



Only this one exists with the original Yee scheme



$\bullet = H_y$   
 $\bullet = E_z$

More  $H_y$ -points used with the new scheme



- Electric field updates modified, magnetic fields updated exactly as in standard FDTD/FIT
- Example: x-component of the electric field:

$$\begin{aligned} E_x|_{i+1/2,j,k}^{n+1} = & E_x|_{i+1/2,j,k}^n + \alpha \frac{\Delta t}{\epsilon \Delta z} [H_y|_{i+1/2,j,k+1/2}^{n+1/2} - H_y|_{i+1/2,j,k-1/2}^{n+1/2}] + \\ & \beta \frac{\Delta t}{\epsilon \Delta z} \left[ H_y|_{i+1/2,j+1,k+1/2}^{n+1/2} - H_y|_{i+1/2,j+1,k-1/2}^{n+1/2} + H_y|_{i+1/2,j-1,k+1/2}^{n+1/2} - H_y|_{i+1/2,j-1,k-1/2}^{n+1/2} \right] + \\ & \gamma \frac{\Delta t}{\epsilon \Delta z} \left[ H_y|_{i+3/2,j+1,k+1/2}^{n+1/2} - H_y|_{i+3/2,j+1,k-1/2}^{n+1/2} + H_y|_{i-1/2,j+1,k+1/2}^{n+1/2} - H_y|_{i-1/2,j+1,k-1/2}^{n+1/2} \right. \\ & \quad \left. H_y|_{i+3/2,j-1,k+1/2}^{n+1/2} - H_y|_{i+3/2,j-1,k-1/2}^{n+1/2} + H_y|_{i-1/2,j-1,k+1/2}^{n+1/2} - H_y|_{i-1/2,j-1,k-1/2}^{n+1/2} \right] + \\ & \alpha \frac{\Delta t}{\epsilon \Delta y} [H_z|_{i+1/2,j+1/2,k}^{n+1/2} - H_z|_{i+1/2,j-1/2,k}^{n+1/2}] + \\ & \beta \frac{\Delta t}{\epsilon \Delta y} \left[ H_z|_{i+3/2,j+1/2,k}^{n+1/2} - H_z|_{i+3/2,j-1/2,k}^{n+1/2} + H_z|_{i-1/2,j+1/2,k}^{n+1/2} - H_z|_{i-1/2,j-1/2,k}^{n+1/2} \right. \\ & \quad \left. H_z|_{i+1/2,j+1/2,k+1}^{n+1/2} - H_z|_{i+1/2,j-1/2,k+1}^{n+1/2} + H_z|_{i+1/2,j+1/2,k-1}^{n+1/2} - H_z|_{i+1/2,j-1/2,k-1}^{n+1/2} \right] + \\ & \gamma \frac{\Delta t}{\epsilon \Delta y} \left[ H_z|_{i+3/2,j+1/2,k+1}^{n+1/2} - H_z|_{i+3/2,j-1/2,k+1}^{n+1/2} + H_z|_{i-1/2,j+1/2,k+1}^{n+1/2} - H_z|_{i-1/2,j-1/2,k+1}^{n+1/2} \right. \\ & \quad \left. H_z|_{i+3/2,j+1/2,k-1}^{n+1/2} - H_z|_{i+3/2,j-1/2,k-1}^{n+1/2} + H_z|_{i-1/2,j+1/2,k-1}^{n+1/2} - H_z|_{i-1/2,j-1/2,k-1}^{n+1/2} \right] \end{aligned}$$



# Numerical Dispersion & Stability

- Basic observation:
  - The scheme should lead to:
  - With  $\alpha+4\beta+4\gamma=1$  and  $\Delta t=\Delta z/c$  the update equation leads to numerical phase velocity being equal to  $c$  along  $x,y,z$ -directions

$$\sin^2\left(\frac{\omega\Delta t}{2}\right) = \left(\frac{c\Delta t}{\Delta z}\right)^2 \sin^2\left(\frac{k\Delta z}{2}\right)$$

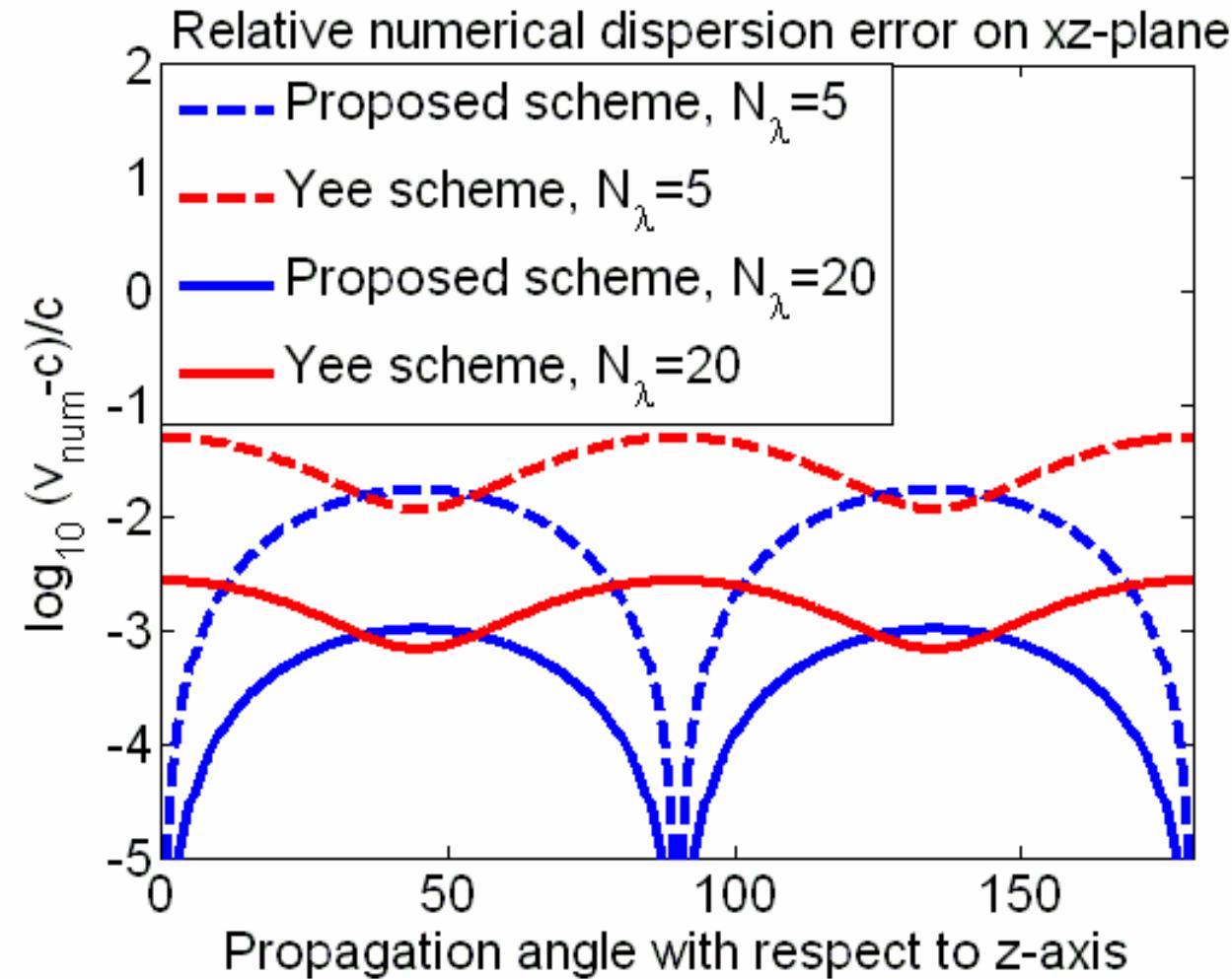


$$E_x = E_0 e^{j(kz-\omega t)}, E_y = 0, E_z = 0$$

$$H_x = 0, H_y = \frac{E_0}{\eta} e^{j(kz-\omega t)}, H_z = 0$$

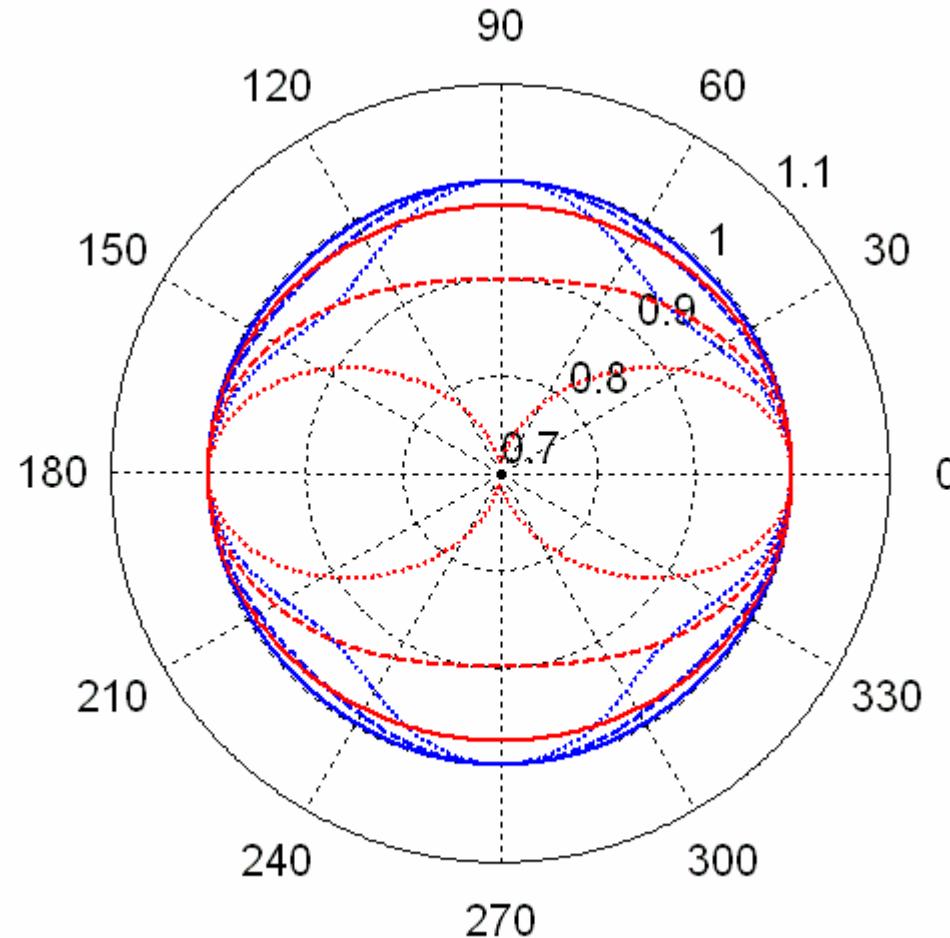
- The scheme is stable (for example) with  $\alpha=7/12$ ,  $\beta=1/12$ ,  $\gamma=1/48$  assuming cubic cells.
- With  $\alpha=1$ ,  $\beta=0$ ,  $\gamma=0$  and reduced time step the scheme reduces to the standard FDTD/FIT-scheme

# Numerical Dispersion vs. Yee



# New Scheme vs. LT Splitting

Proposed scheme: Blue curves (3,5 and 10 cells per wavelength). LT splitting: red curves. Phase velocity anisotropy error is lower than with LT splitting (**PBCI-code**).





# Indirect Integration

- The problem
  - How to calculate the wake potential in „infinitely“ long beam pipes ?
- Solution (according to H. Henke)
  - Transformation of the infinite integral into a finite one by using Stokes' theorem
  - Requires a solution of a **Poisson's equation** over the arbitrary cross-section of the beam pipe at every time step within the moving window
  - Allows truncating the outgoing beam pipe
- Implementation
  - Direct integration in C-code, post-processing (solutions to Poisson's equations) in Matlab

$$W_{\parallel}(0, s) = - \int_{-\infty}^{\infty} E_z(z, 0, \frac{s+z}{c}) dz$$

$$\nabla^2 \Phi = \frac{\partial E_z}{c \partial t} - \frac{\partial E_z}{\partial z}$$



RHS of the Poisson's equation is saved within the moving window at the end of the simulation

Details of the scheme can be found in EPAC 2006 paper: H. Henke, W. Bruns, „Calculation of wake potentials in general 3D structures“



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# New Discrete Scheme in 2D

- How to discretize the partial differential equation ?

$$\frac{\partial^2 \Phi}{c^2 \partial t^2} = \frac{\partial^2 \Phi}{\partial z^2} + \frac{\partial^2 \Phi}{\partial r^2} - \frac{1}{r} \frac{\partial \Phi}{\partial r}$$

$$\begin{aligned}\frac{\partial^2 \Phi}{\partial z^2}(i, j) &= a_z \frac{\Phi(i+1, j) - 2\Phi(i, j) + \Phi(i-1, j)}{\Delta z^2} + \\ b_z \frac{\Phi(i+1, j+1) - 2\Phi(i, j+1) + \Phi(i-1, j+1)}{\Delta z^2} + \\ b_z \frac{\Phi(i+1, j-1) - 2\Phi(i, j-1) + \Phi(i-1, j-1)}{\Delta z^2}\end{aligned}$$



# New Discrete Scheme

- How to choose good parameters  $a$  and  $b$ ?
  - the scheme must be numerically **stable** if  $\Delta t = \Delta z/c$
  - the scheme must be **free of dispersion** in the longitudinal direction
  - the scheme must be at least second-order accurate

$$\xi^2 - 2 \left[ 1 + \left( \frac{c\Delta t}{\Delta z} \right)^2 g \right] \xi + 1 = 0$$

Stability equation

$$|\xi| \leq 1 \iff -2 \leq g \leq 0$$

$$g = \cos(k_z \Delta z) \times \left[ 1 - 4b_z \sin^2\left(\frac{k_r \Delta r}{2}\right) - \frac{2b_r \Delta z^2}{\Delta r^2} \right] + \\ \frac{\Delta z^2 \cos(k_r \Delta r)}{\Delta r^2} \times \left[ 1 - 4b_r \sin^2\left(\frac{k_z \Delta z}{2}\right) - \frac{2b_z \Delta r^2}{\Delta z^2} \right] - a_z - \frac{\Delta z^2 a_r}{\Delta r^2}$$



# New Discrete Scheme

The parameter choice

$$a_r = a_z = \frac{\Delta z^2 + 2\Delta r^2}{2\Delta z^2 + 2\Delta r^2}$$

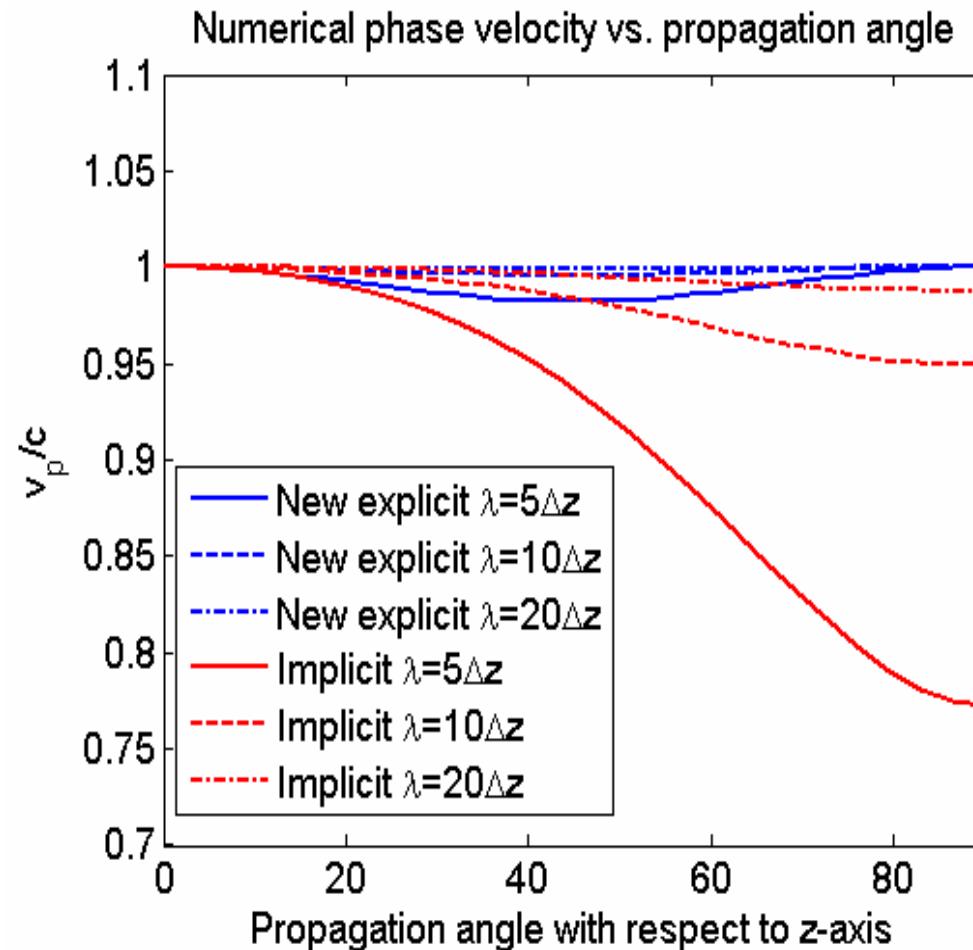
$$b_r = b_z = \frac{\Delta z^2}{4(\Delta z^2 + \Delta r^2)}$$

satisfies the required conditions if  $\Delta r / \Delta z \geq 1$ . The first-order term is discretized according to

$$\frac{\partial \Phi}{\partial r}(i, j) = \frac{1}{2} \frac{\Phi(i, j+1) - \Phi(i, j-1)}{2\Delta r} + \frac{1}{4} \frac{\Phi(i+1, j+1) - \Phi(i+1, j-1)}{2\Delta r} + \frac{1}{4} \frac{\Phi(i-1, j+1) - \Phi(i-1, j-1)}{2\Delta r}$$

and the scheme remains stable with the same time-step.

- Comparison of the new explicit scheme and the implicit scheme.

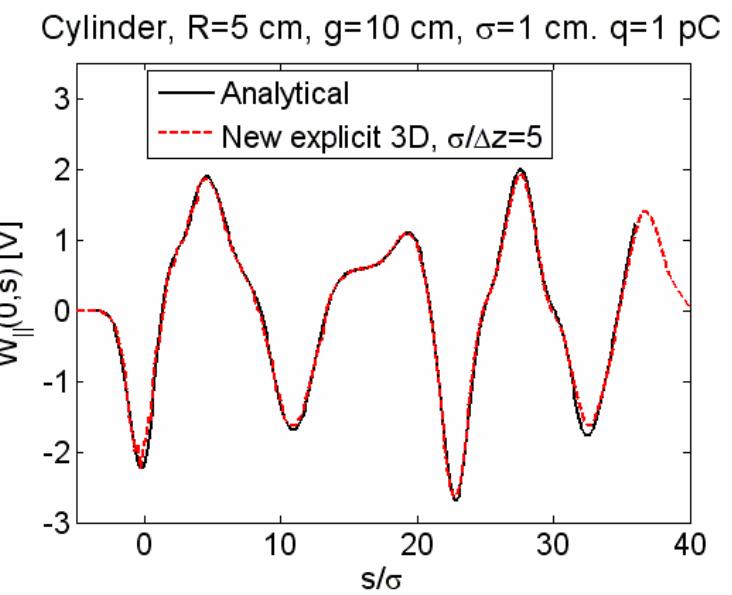
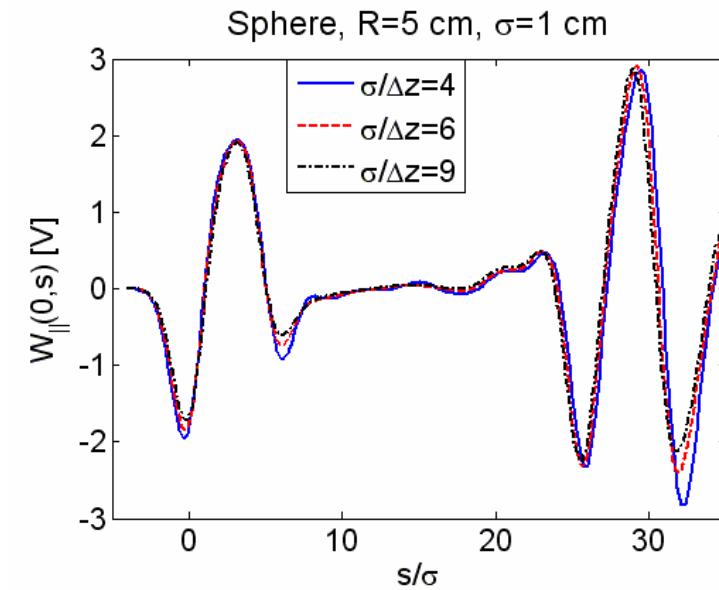
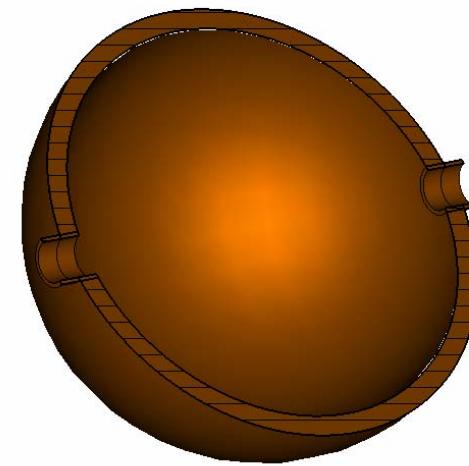
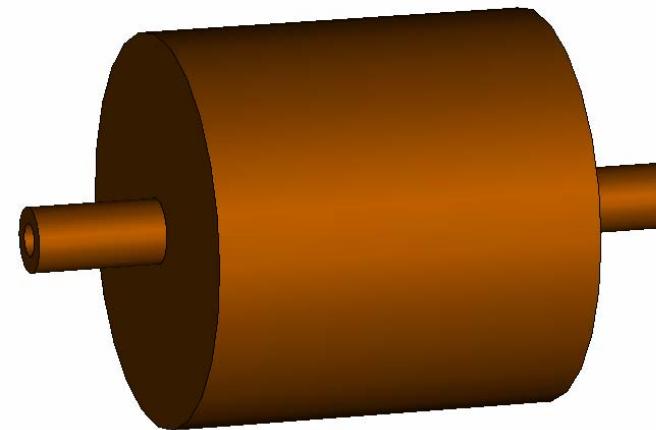




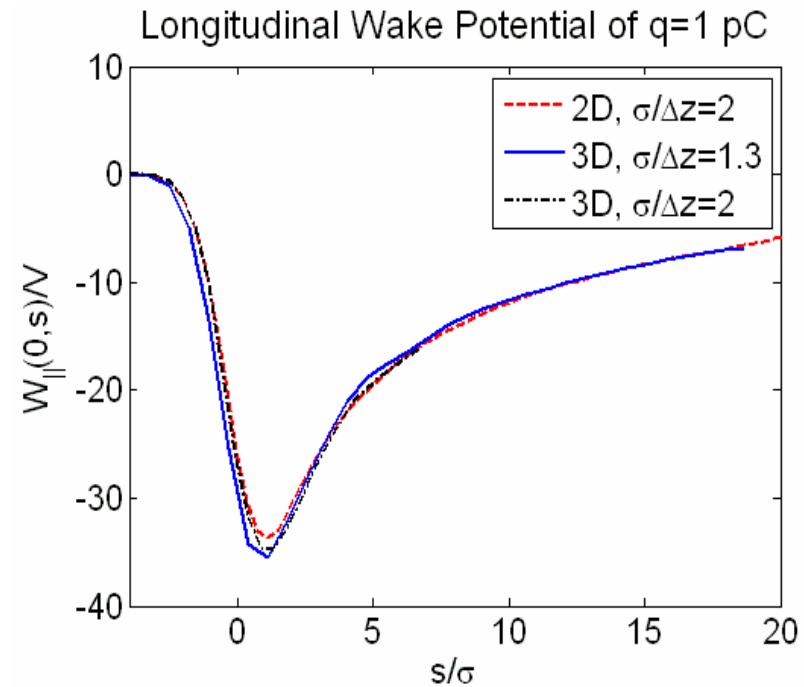
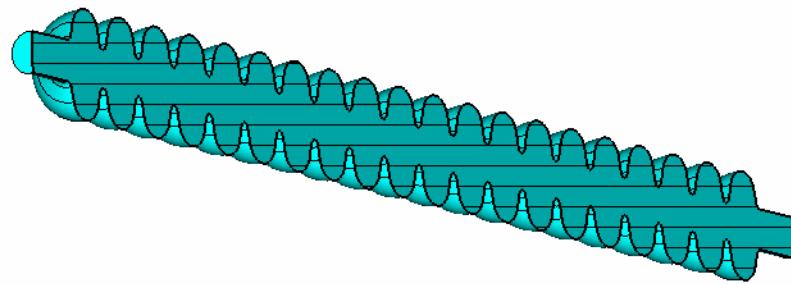
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# Spherical Cavity & Pillbox



# 20 Tesla Cells



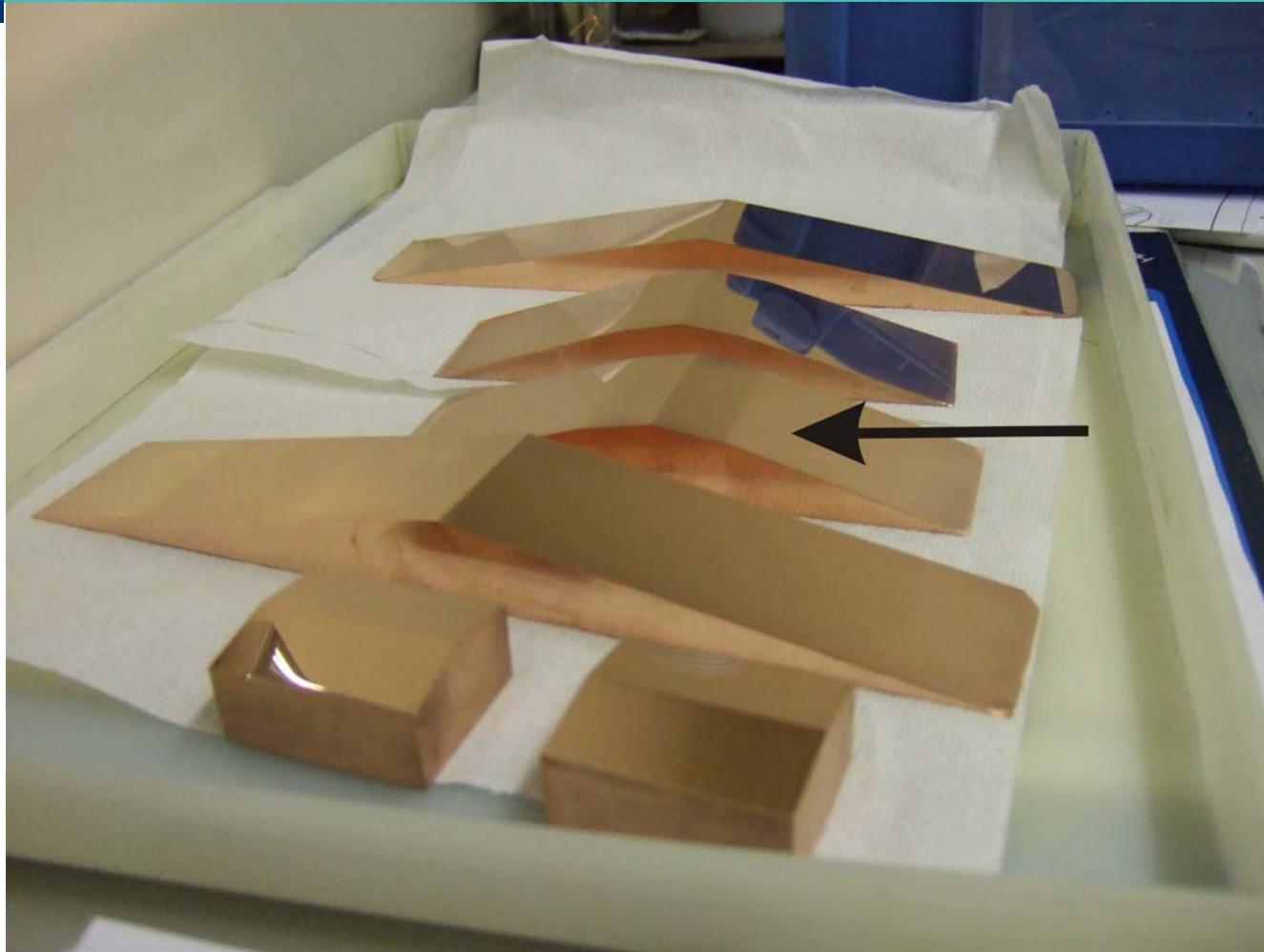
Simulation on a single processor using  $\sigma/\Delta z=2$  takes about 24 hours. Total number of cells in the structure: 1 712 815 142. Number of cells within the **moving window**: 8 668 824.



Only the fields in the vicinity of the bunch  
(i.e. inside the „moving window“) are updated



# ILC-ESA Collimator Prototype



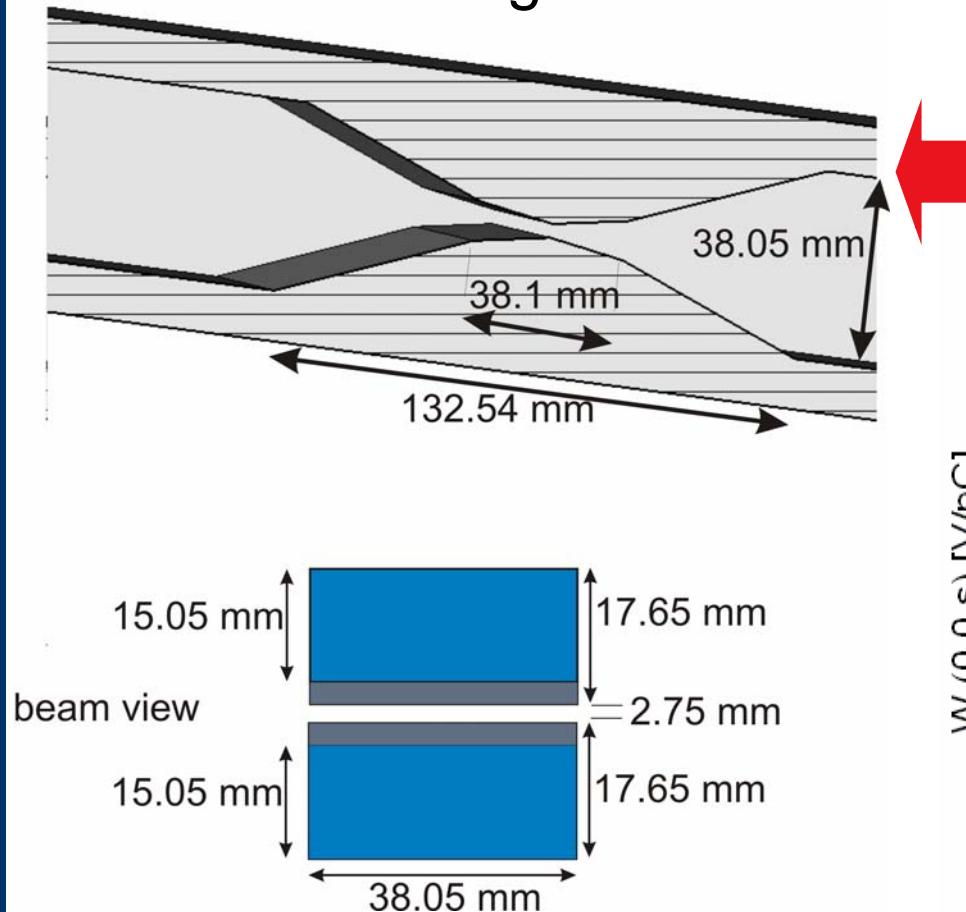
Dr.-Ing. Mikko Kärkkäinen  
Institut für Theorie Elektromagnetischer Felder

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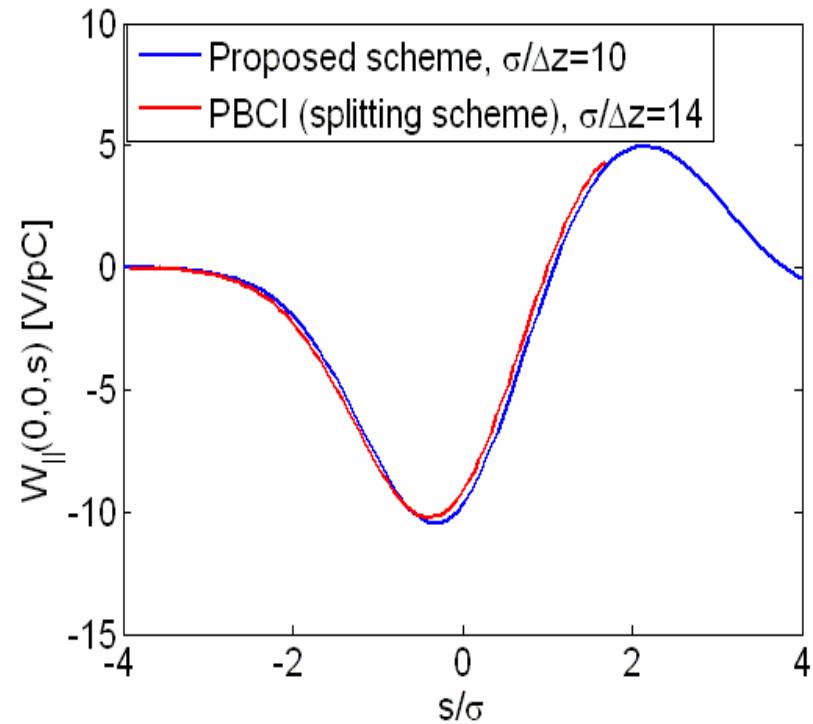
Collimators were built within the project Spoiler Wakefield and Mechanical Design (SWMD), and were measured with [SLAC](#). Picture from Nigel Watson, CCLRC.

# ILC-ESA Collimator Prototype

With a long bunch (1mm) the results are accurate with about 10 cells over the bunch length

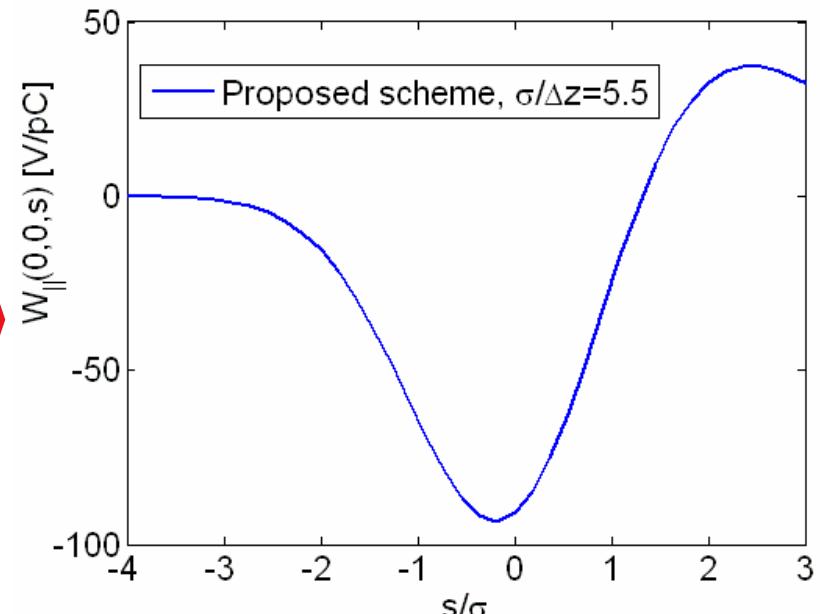


Beam pipe truncated here,  
indirect wake calculated by  
solving Poisson's equation





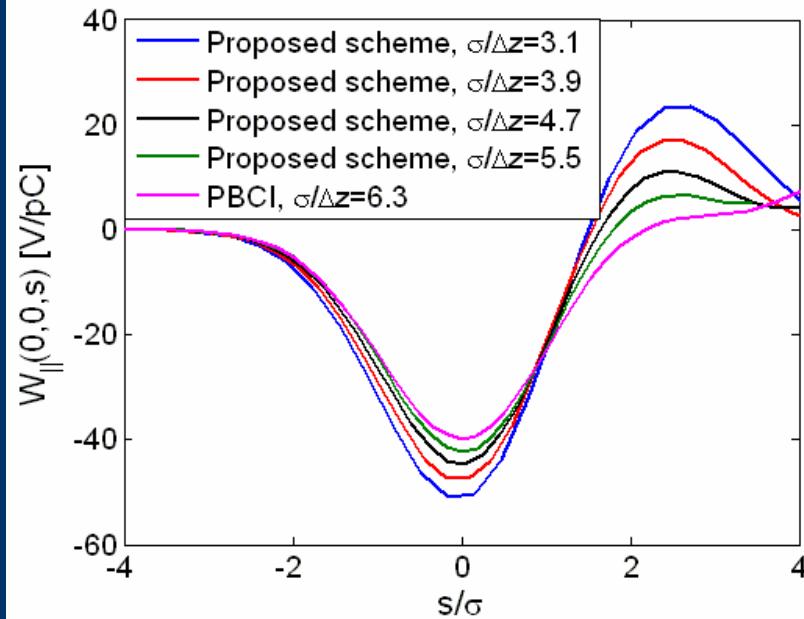
GdfidL produces fairly similar results



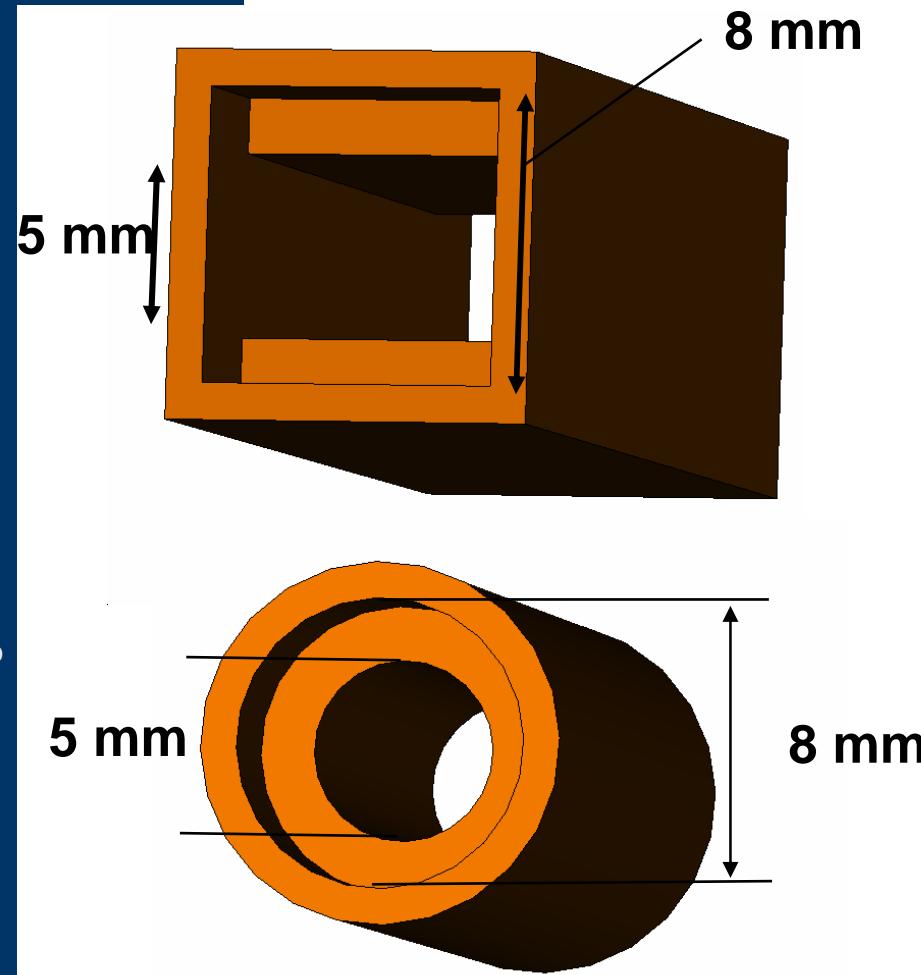
Indirect integration included,  
i.e. infinite outgoing pipe



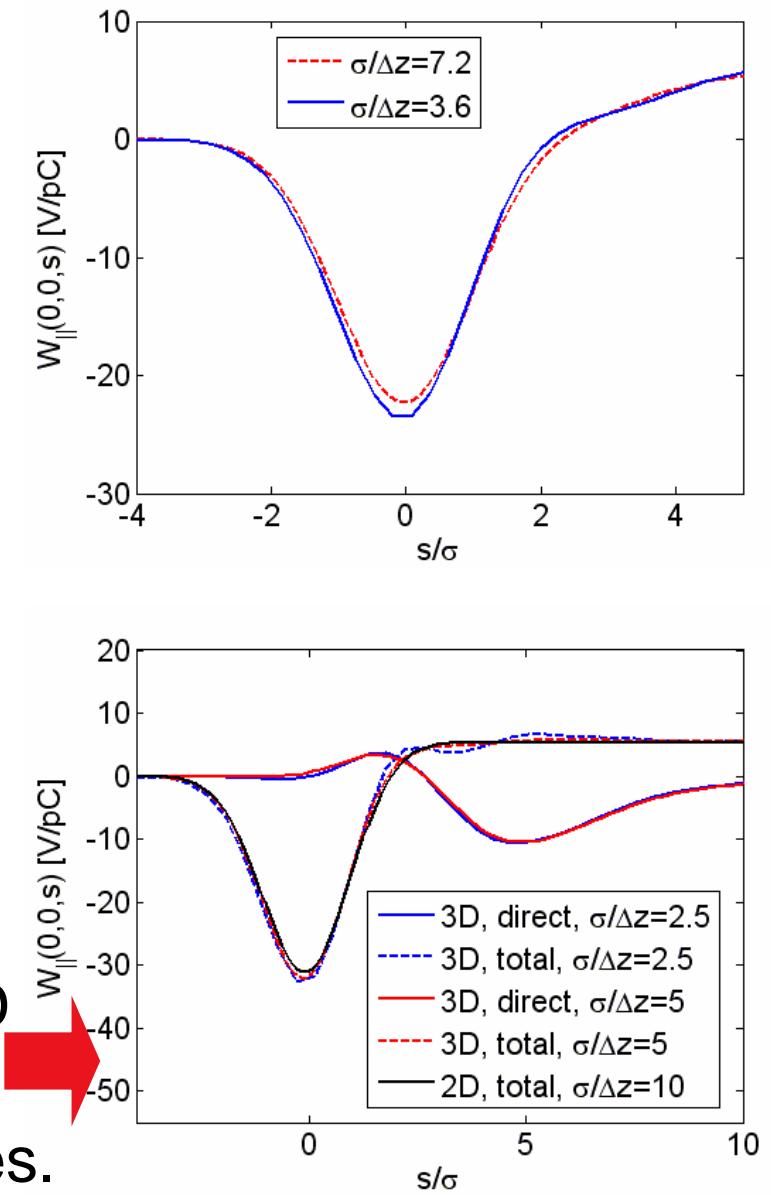
Finer mesh or a conformal  
scheme is needed !



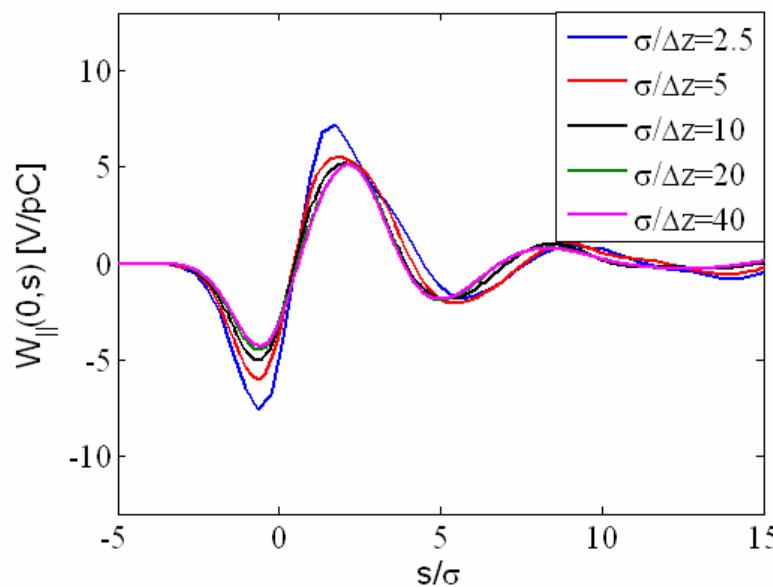
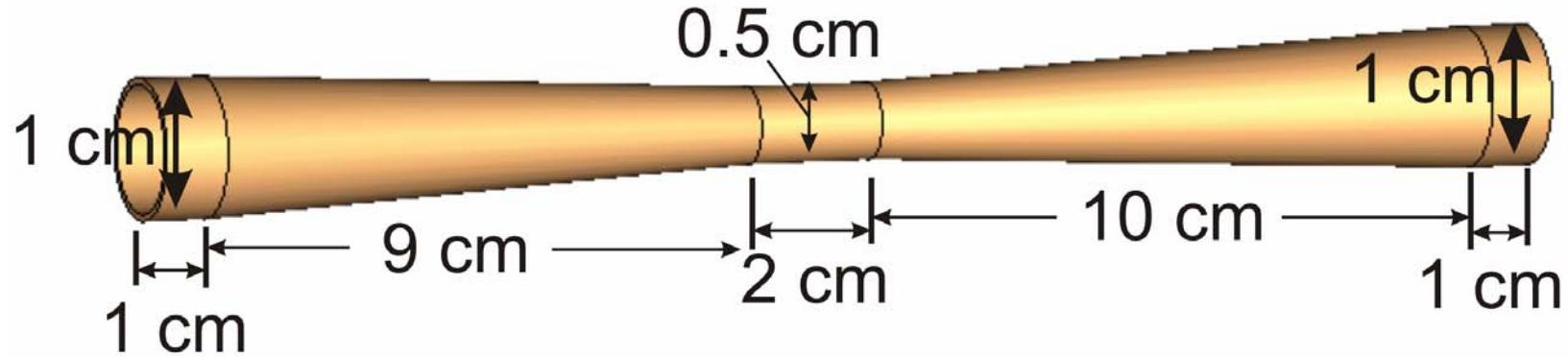
# Step Collimators



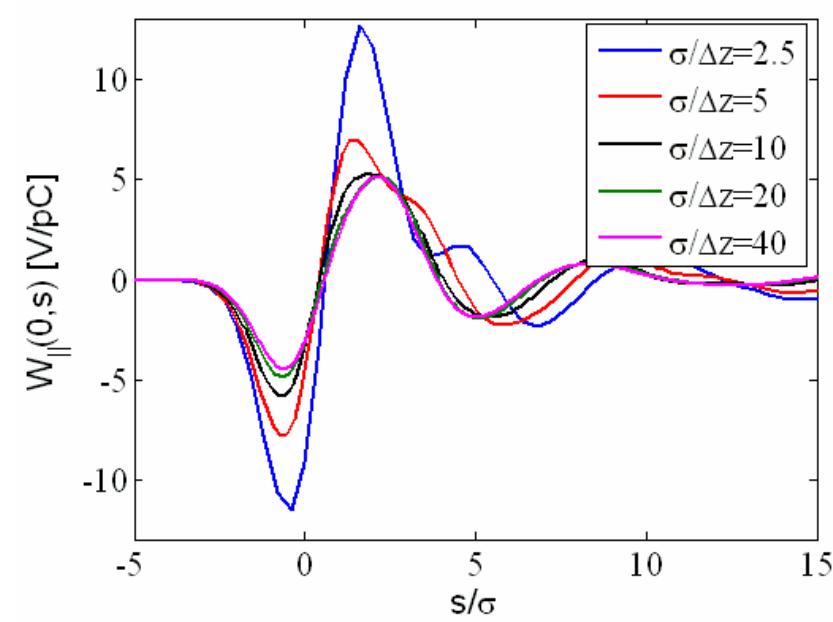
Very good agreement between 2D and 3D.  $\sigma=200\mu\text{m}$  in both cases.  
Total length is 2.8 cm in both cases.



# Staircasing, Collimator



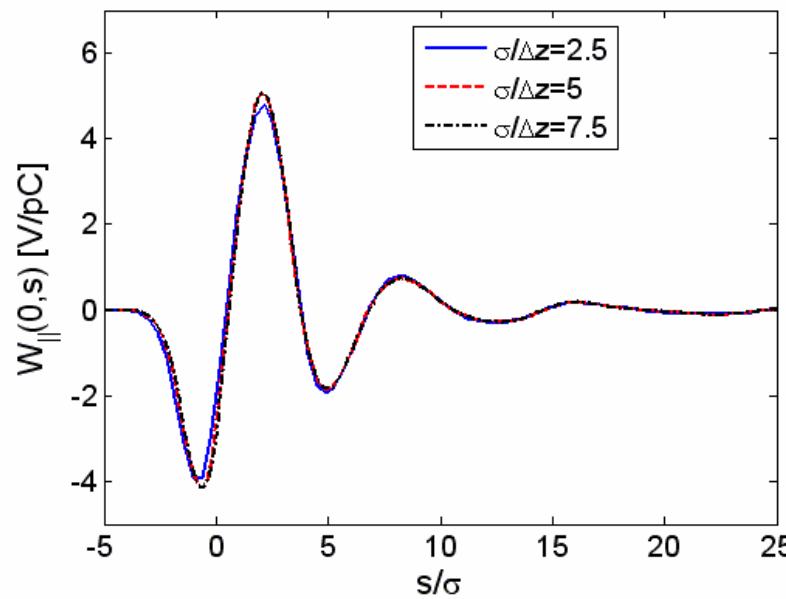
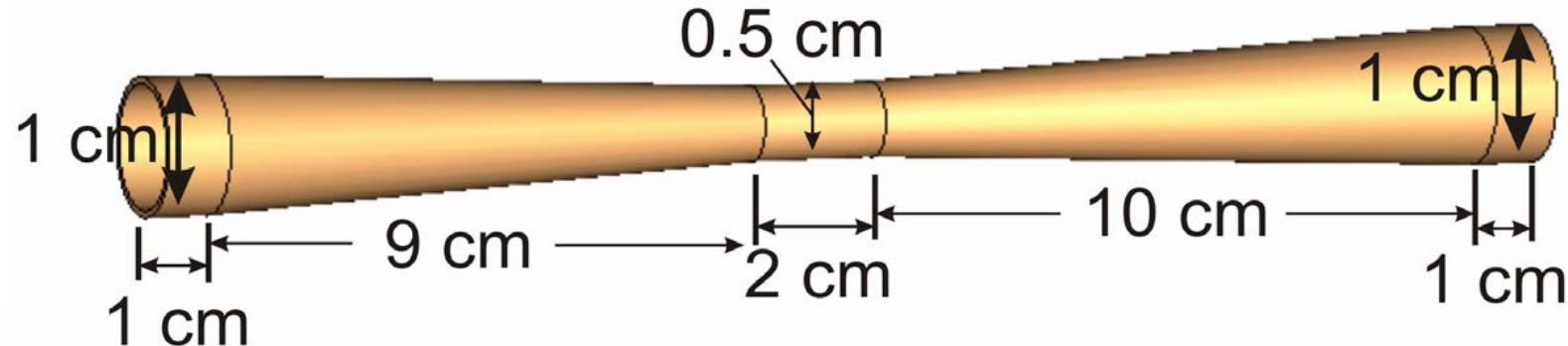
Proposed explicit 2D scheme



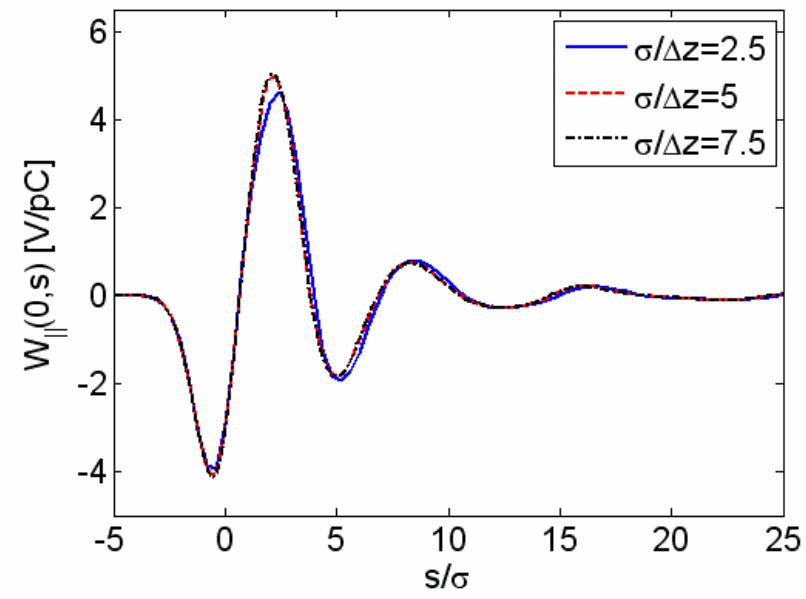
ECHO 2D (implicit scheme)

# Conformal Scheme, Collimator

- Faster convergence with conformal schemes.



Proposed explicit 2D scheme



ECHO 2D (implicit scheme)



# Conclusions, Future Plans

- Conclusions:
  - An FDTD scheme for 3D wake field simulations has been introduced and (partially) validated
  - A scheme for cylindrically symmetric problems was introduced
  - Numerical dispersion properties of the schemes are suitable for simulating long accelerator structures
  - Dissatisfactory accuracy for gently tapered structures with stair-casing
- Future plans:
  - Conformal boundary treatment in 3D (PBCI and the proposed scheme)
  - Other extensions