

THE SHORT-RANGE WAKEFIELDS IN THE BTW ACCELERATING STRUCTURE OF THE ELETTRA LINAC

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Abstract

Future FEL operations in the ELETTRA LINAC require a high quality beam with an ultra short bunch. The knowledge of the short-range wakefields in the backward traveling wave (BTW) accelerating structure is needed to predict the beam quality in term of the single bunch energy spread and emittance. To calculate the effect of the longitudinal and transverse wakefields we have used the time domain numerical approach with a new implicit scheme for calculation of wake potential of short bunches in long structure [1, 2]. First the wake potentials of the BTW structure are numerically calculated for very short bunches, than an analytical approximations for wake functions in short range are obtained by fitting procedures based on analytical estimations. Finally the single bunch energy spread induced by short-range longitudinal wakefields is analyzed for the first phase of the project FEL-I (up to 40 nm).

INTRODUCTION

The FERMI@ELETTRA project aims to construct a single-pass FEL user-facility in the spectral range 100-10 nm using the exiting normal conducting 1.0 GeV linac. Figure 1 shows the proposed machine layout for the two phase of the project: FEL-I (100-40 nm) and FEL-II (40-10 nm) [3].

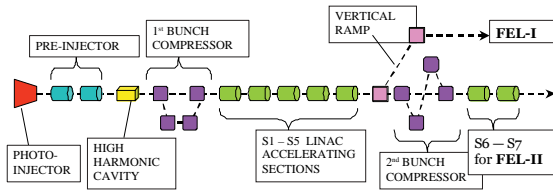


Figure 1: Schematic layout of the configuration for the FEL-I and FEL-II stages.

The new scheme foresees the installation of an RF photocathode gun [4], providing a high quality electron beam, with parameters directly related to those required at the entrance of the undulator lines [3]. At the photoinjector exit the beam is further accelerated with a 100 MeV preinjector, composed by two 3 m accelerating sections with focusing solenoids, that get the beam out of the space-charge energy domain and creates an energy-position correlation for

bunch compression. After the first magnetic chicane, five accelerating structures of the exiting linac, each equipped with an RF pulse compression system (SLED), allow the beam to reach the energy required by FEL-I, 700 MeV. In total the present linac includes seven 6 m accelerating sections, the remaining two accelerating sections will be located after the second bunch compression and will be used for the FEL-II to rise the beam energy up to 1 GeV. Each accelerating section is a backward traveling wave (BTW) structure composed by 162 nose cone cavities magnetically coupled and operated in the $3/4\pi$ mode. In this scenario, to avoid undesirable beam degradations, in term of energy spread and emittance, the wakefields effects have to be carefully considered. We have studied the longitudinal and transverse cases using the time domain code ECHO with a new implicit scheme for the calculation of the wake potentials of short bunches in long structures [1, 2]. We have considered the wakefields evolution for bunches of different lengths passing through a single cell, a multi-cell and a complete accelerating structure [5]. This paper reports the longitudinal and transverse wakefields calculations for a complete BTW accelerating structure and the single bunch energy spread induced by short-range longitudinal wakefields for the FEL-I. A preliminary optimization of the energy spread has been carried out by varying the energy gain and RF phase of the accelerating structure.

LONGITUDINAL WAKE FUNCTION OF THE BTW STRUCTURE

The wake potentials of Gaussian bunches with length ranging from $1000\mu\text{m}$ to $50\mu\text{m}$ are calculated for a whole BTW accelerating structure. In figure 2 the calculated longitudinal wake potentials (solid lines) are reported. To find an analytical approximation of the wake function we have chosen a combination of periodic [7] and one cell [6] dependence since the BTW structure can be treated as a periodic structure of finite length. From the fit of the numerical wake potentials we have obtained an analytical expression approximating the wake function (in V/pC):

$$w_{\parallel}^0(s) = A_{01}e^{-\sqrt{s/s_0}} + \frac{A_{02}}{\sqrt{s}} \quad (1)$$

where $A_{01} = 7300$, $s_0 = 3.2 \cdot 10^{-4}$ and $A_{02} = 3.4$.

Figure 2 shows the longitudinal wake function (1) (black dotted line), which tends for small s to be an envelope function to the wakes and fits the numerical results up to 1.5mm . To find an analytical approximation up to 5mm , we have added to expression (1) an additional term with

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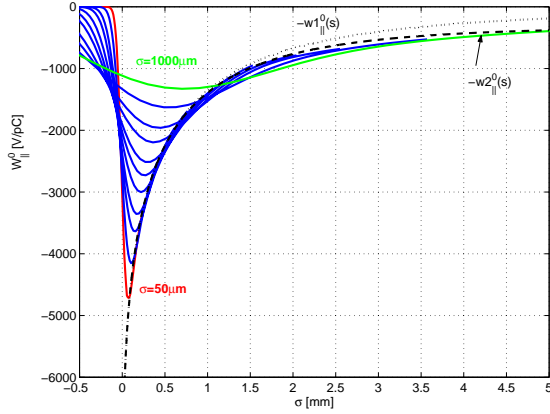


Figure 2: Longitudinal wake potentials (solid lines) and longitudinal wake functions (1)(black dotted line) and (2) (black dashed line) of the BTW structure.

\sqrt{s} dependence. Taking into account the last correction term the fit gives the following analytical expression for the wake function:

$$w2_{||}^0(s) = A_{01}e^{-\sqrt{s/s_0}} + \frac{A_{02}}{\sqrt{s}} + A_{03}\sqrt{s} \quad (2)$$

where $A_{01} = 7450$, $s_0 = 3.1 \cdot 10^{-4}$, $A_{02} = 3$ and $A_{03} = 3000$.

The previous relation approximates the longitudinal wake function on a wider range compared to expression (1). Figure 2 shows the longitudinal wake function (2) (black dashed line) that tends to be an envelope function to the wakes up to 5mm. Figure 3 presents the calculated longitudinal wake potentials (blue solid lines) together with analytical approximation (2) (red dashed lines). A more detailed analysis of figures 2 and 3 shows that the analytical expression 2 approximates very well the longitudinal wake function up to 5mm.

TRANSVERSE WAKE FUNCTION OF THE BTW STRUCTURE

Figure 4 shows the calculated transverse wake potentials (solid lines) for different bunch length σ . As in the previous case, the BTW structure is treated as a periodic structure of finite length and to find an analytical approximation for the transverse wake function, a combination of periodic [7] and one cell [6] dependence was chosen. The expression for the wake function is obtained with a fit of the numerical wake potentials (in V/pC/m):

$$w1_{\perp}^1(s) = A_{11} \left[1 - \left(1 + \sqrt{\frac{s}{s_1}} \right) e^{-\sqrt{s/s_1}} \right] + A_{12}\sqrt{s} \quad (3)$$

where $A_{11} = 1.7 \cdot 10^5$, $s_1 = 1.2 \cdot 10^{-4}$ and $A_{12} = 8.5 \cdot 10^4$.

Figure 4 shows the transverse wake function (3) (black dashed line), which tends to be envelope function for the

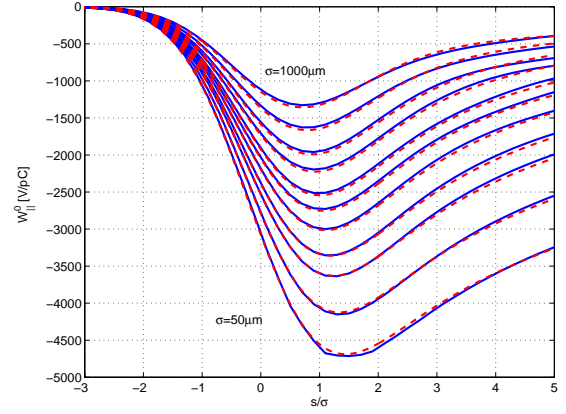


Figure 3: Longitudinal numerical (blue solid lines) and analytical (red dashed lines) wake potentials of the BTW structure.

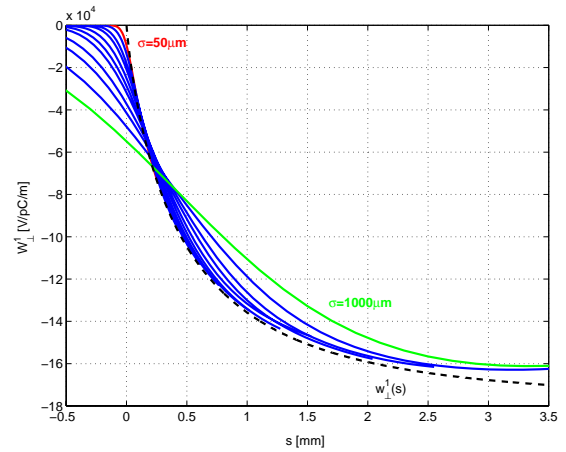


Figure 4: Transverse wake potentials (solid lines) and transverse wake functions (black dashed line) of the BTW structure.

wakes up to distance $s = 2mm$ after the bunch center. Figure 5 plots the calculated transverse wake potentials (blue solid lines) together with their analytical approximations (3) (red dashed lines). For transverse case no additional term is introduced and the wake function fits the results up to 2mm.

SINGLE BUNCH ENERGY SPREAD IN BTW STRUCTURE

The first phase of FERMI foresees a bunch acceleration up to 700 MeV with bunch length $\sigma = 120\mu m$ and total charge $Q=1nC$. At the exit of each accelerating module, the single bunch energy spread is determined by the RF accelerating fields produced by the external generator and the wakefields excited by the beam in the accelerating structure. As already shown in [8], for Gaussian bunch the

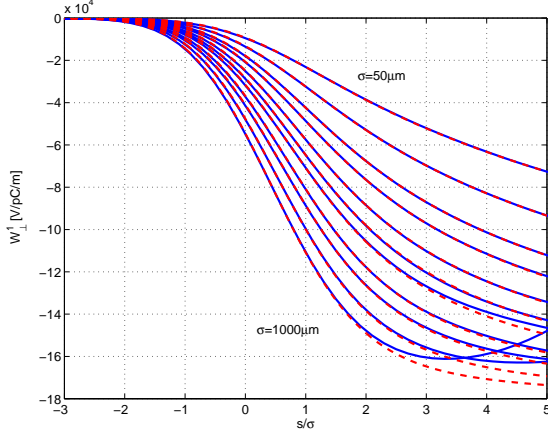


Figure 5: Transverse numerical (blue solid lines) and analytical (red dashed lines) wake potentials of the BTW structure.

RMS energy spread can be evaluated by knowing four integral parameters of the wakefields: the loss factor $K_{||}$, the average wake energy spread $\sqrt{\Delta W^2}$, the cosine-Fourier part I_{cos} and the sine-Fourier part I_{sin} . The last two parameters are needed to take into account the correlation between the wake potentials and the accelerating voltage [8]. Table 1 summarizes the four integral parameters for bunches of different length obtained with numerical time domain simulation (a), and analytical calculations (b) using (1): an excellent agreement between the two sets of data is shown. Figures 6 and 7 show the relative energy spread $\Delta U / \langle U \rangle$ and relative average energy gain $\langle U \rangle / U_0$ as a function of the RF phase ϕ , for different energy gain per section U_0 . The calculations have been made under the assumption that the energy spread is negligible with respect to the total energy gain for acceleration section and considering a maximum energy gain for section up to 170 MeV. We can see that the average energy gain at optimum phase ϕ_{opt} is approximately 27% lower than the corresponding value on crest, $\phi = 0^\circ$, for each value of the peak of the acceleration voltage (figure 7). Table 2 contains the relative energy spread when the beam is accelerated on crest, RF phase $\phi = 0^\circ$, and the minimum relative energy spread at the optimum phase ϕ_{opt} . These parameters are given for different peak of the accelerating voltage. The relative energy spread decrease with the increase of the accelerating voltage. With an maximum energy gain of 170 MeV the minimum relative energy spread is about 2 times lower than the corresponding at $\phi = 0^\circ$.

To obtain the required 700 MeV of FEL-I, the BTW structures have to be operated with a gradient of 21 MV/m [9]. Figure 8 shows different behaviors of the relative energy spread as a function of the electric field gradient (changing the RF phase from -50° to 10°) for different peak accelerating voltage U_0 , for a bunch with length $\sigma = 120 \mu\text{m}$ with a charge $Q = 1 \text{ nC}$. Considering the

Table 1: Numerical and analytical integral parameters of the wake potentials of Gaussian bunches in the BTW structure.

σ [μm]	$K_{ }$ [V/pC]	I_{cos} [V/pC]	I_{sin} [V/pC]	$\sqrt{\Delta W^2}$ [V/pC]
Numerical integral parameters (a)				
50	-2861.7	-0.001477	-4.368020	1459.8
120	-2298.3	-0.009598	-7.860948	1118.4
150	-2145.5	-0.015227	-8.964911	1029.0
Analytical integral parameters (b)				
50	-2861.2	-0.001546	-4.307913	1441.2
120	-2295.4	-0.009476	-7.831107	1112.5
150	-2145.8	-0.014982	-8.961020	1026.3

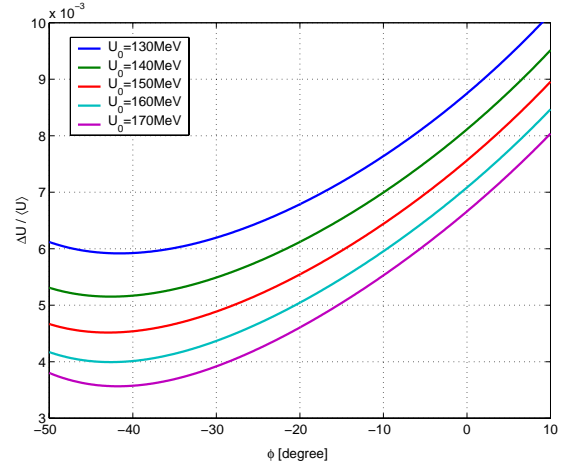


Figure 6: Relative energy spread as a function of the RF phase in the BTW structure (bunch length $\sigma = 120 \mu\text{m}$ and $Q = 1 \text{ nC}$).

21 MV/m required, we can see that the relative energy spread is near its minimum value only for $U_0 = 170 \text{ MeV}$. With lower values of U_0 the relative energy spread don't get its minimum value through the tuning of RF phase.

CONCLUSION

Calculations of the wakefields for short bunches passing through a complete BTW accelerating structure have been presented. The short-range longitudinal and transverse wake potentials are been calculated in time domain with the code ECHO. From the numerical results analytical approximations of the point-charge wake functions were found. For the analytical model we have chosen as a combination of periodic and one-cell dependences. In the longitudinal case the term that describes the finite structure (one cell behavior) is very small compared to the periodic structure term. Hence in range of σ we have considered, the longitudinal wakes shows mainly a periodic structure behavior. In addition, for better fitting of the data up to 5

Table 2: Energy gain and energy spread in the BTW structure (bunch length $\sigma = 120\mu\text{m}$ and $Q = 1nC$).

U_0 [MeV]	RF phase	$\langle U \rangle$ [MeV]	$\Delta U / \langle U \rangle$ %
130.0	$\phi = 0.0^\circ$	127.70	0.87
	$\phi_{opt} = -41.6^\circ$	94.96	0.59
140.0	$\phi = 0.0^\circ$	137.70	0.81
	$\phi_{opt} = -42.6^\circ$	100.69	0.51
150.0	$\phi = 0.0^\circ$	147.70	0.76
	$\phi_{opt} = -43.0^\circ$	107.48	0.45
160.0	$\phi = 0.0^\circ$	157.70	0.71
	$\phi_{opt} = -42.6^\circ$	115.44	0.40
170.0	$\phi = 0.0^\circ$	167.70	0.67
	$\phi_{opt} = -41.8^\circ$	124.47	0.36

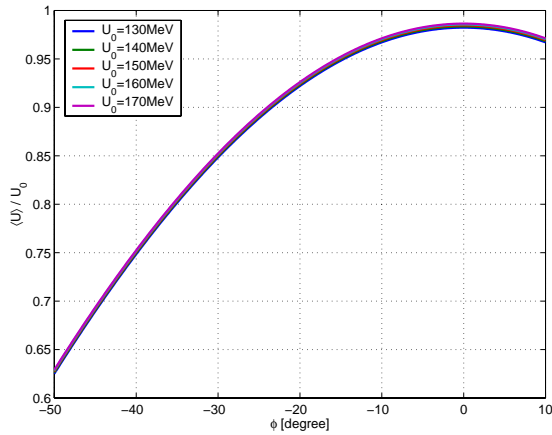


Figure 7: Relative energy gain as a function of RF phase in the BTW structure (bunch length $\sigma = 120\mu\text{m}$ and $Q = 1nC$).

mm, we have used an additional term in the model. Furthermore, the single bunch energy spread induced by longitudinal wakefields has been analyzed for the first phase of the project FEL-I. We have seen that the wakefield effects can be compensated by shifting the bunch injection phase to optimum values, decreasing the energy gain of about 27%. For the 700 MeV energy design of FEL-I and a peak gradient of 27.8 MV/m (170 MeV energy gain for section) this means to operate at $\phi = -41.8^\circ$ and a gradient of 21 MV/m.

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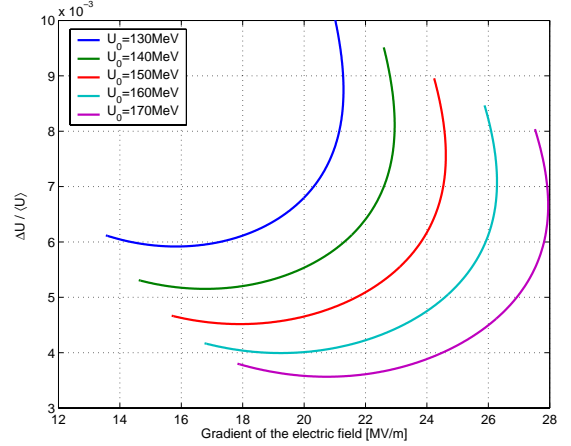


Figure 8: Relative energy spread as a function of the gradient of the electric field in the BTW structure (bunch length $\sigma = 120\mu\text{m}$ and $Q = 1nC$).

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