

Status of SILUND-21 Linear Induction Accelerator Project

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Abstract

SILUND-21 accelerator is constructed in the framework of experimental program to study free electron laser physics, a problem of two-beam acceleration and microwave electronics. Experiments are planned to adopt the FEL bunching technique for generation of the CLIC driving beam.

1 INTRODUCTION

Linear induction accelerator SILUND-21 is constructed using the equipment of LUEK-20 accelerator developed for experimental investigations of the collective method of acceleration [1]. It is assumed to upgrade the main pieces of the LUEK-20 equipment using the experience of construction and operation of SILUND, SILUND-II, SILUND-20 and LUEK-20 linear induction accelerators developed at JINR [1] - [5].

2 ACCELERATOR DESIGN

SILUND-21 accelerator consists of seven accelerating modules. Each module provides 1.5 MV accelerating voltage at 1 kA beam load. The general layout of the accelerating module is presented in Fig.1. Induction section (1) consists of 36 permalloy cores. The core exciting windings are commutated in parallel and the input impedance of the section is equal to 0.5Ω at nominal beam load. Pulses of accelerating voltage with 42 kV amplitude and 50 – 70 ns duration are formed by modulator (2) with 0.5Ω internal resistance. TGII-2500/50 hydrogen thyatron (2500 A, 50 kV), which is used as a commutator, does not provide commutation of the required level of the peak power, so nonlinear power compression schemes are used to increase the peak power.

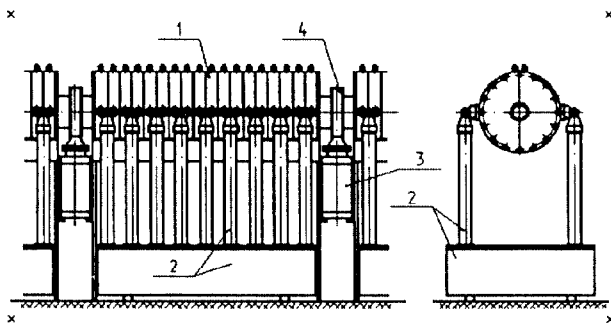


Figure 1: Accelerating module

Vacuum pumping of the accelerator volume is provided by sputter-ion pumps (3) via channels placed in the gap (4). Electron beam diagnostic devices are also placed there.

2.1 Induction section

Design of SILUND-21 inductors is similar to that of the SILUND-20 inductors [6, 7] (see Fig.2).

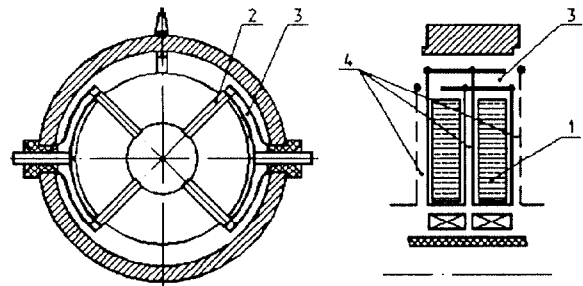


Figure 2: Inductor scheme

Inductor consists of two permalloy cores (1) excited by four windings (2). The feed of the pulsed power to the windings is provided by strip supply lines (3). The wave impedance of each strip supply line is equal to 40Ω . The wave impedance of strip lines (4), located between the cores, is equal to the impedance of the electron beam.

The voltage of six lines (4), commutated in a consecutive order, is fed to the accelerating gap (2) which is formed by cone diaphragm (1) (see Fig.3). The amplitude of accelerating voltage at each of six accelerating gaps of the accelerating section is equal to 250 kV.

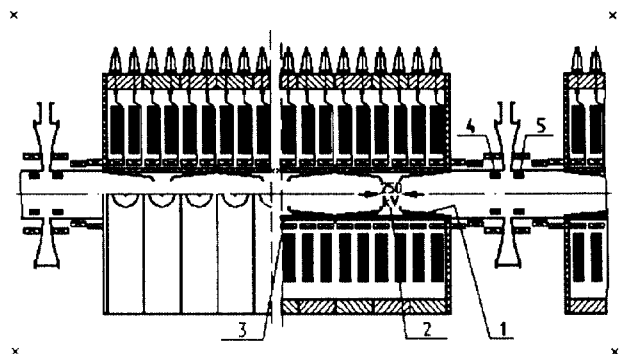


Figure 3: Accelerating section

Focusing of the electron beam is provided by guiding field of solenoid. The solenoid winding is sectional and the number of the sections is equal to the number of permalloy cores. Parameters of the solenoid power supply, developed for accelerator LUEK-20, allow one to provide the guiding magnetic field with the amplitude up to 1.4 T and pulse duration about of 0.8 ms.

The beam diagnostics is performed by Rogovsky coil (4) and beam position monitor (5).

In conclusion of this section we should stress one problem. In our accelerator, ceramic tube (3) plays a role of the vacuum chamber. Theoretical calculations and experimental research at present accelerators have shown that intensive electron beam can excite microwave field in this dielectric waveguide. Under certain conditions, when the phase velocity of the excited waves is close to the velocity of electrons, instabilities of the electron beam may take place. With respect to this effect, cone diaphragms (1) fulfil the role of screens reducing the intensity of interaction between the electron beam and dielectric waveguide. One more problem may be connected with the accelerating gap (2) because it forms a cavity. The interaction of the electron beam with such a cavity may lead to some unwilling effects. At the design stage of the project it is assumed to study resonance properties of the accelerating gap and find out the ways to suppress the dangerous modes of oscillations.

2.2 Injection module

The first accelerating module differs from all the other modules and is combined with the electron source. Accelerating voltage of the electron source is equal to 500 kV – 1/3 of the total accelerating voltage of the module (see Fig.4)

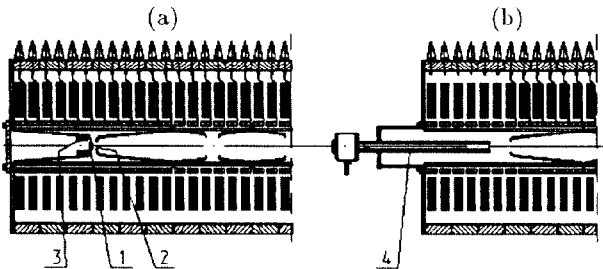


Figure 4: Injection section

The choice of the electron source type depends on the mode of the accelerator operation. Our experience of work at the present accelerators has shown that at a low repetition rate (about of several cycles per second) it is more preferable to use the electron gun with graphite cathode (1) and gridded anode (2) [8](see Fig.4a). The value of magnetic field at the cathode is controlled by magnetic lens (3) to minimize the value of the electron beam emittance. At a high repetition rate (about of 50 cycles per second), we assume to use a plasma electron source without anode grid (see Fig.4b) [9, 10]. Ceramic tube (4) is destined to inject the plasma

into the diode gap.

The both types of electron sources have demonstrated a high level of reliability and good output parameters during their operation at the accelerators SILUND, SILUND-II and SILUND-20.

2.3 Modulator

The scheme of the modulator is close to that of the SILUND-20 accelerator [11]. More than ten years of successful operation of the latter accelerator have proved the validity of technical solutions for the modulator whose peculiar features have a high level of reliability and high quality of output characteristics. The modulator scheme is based on the application of the nonlinear power compression technique.

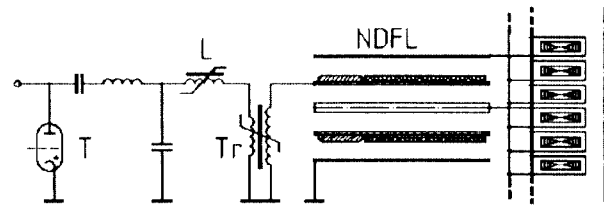


Figure 5: Modulator scheme

Its key element is nonlinear double forming line (NDFL) which consists of 18 double forming lines evenly spaced along the accelerating module. Hydrogen thyratron T operates in a pulsed mode with 3 μ s pulse duration and provides the following parameters: $U = 30$ kV and $I = 10$ kA. Permalloy reactor L and transformer Tr fulfil the roles of ferromagnetic switches. Transformer Tr is composed of three transformers with the transfer factor equal to 2/3 which are placed along the accelerating module. NDFL is charged within the time period 1 μ s and then produces high-voltage pulse ($U = 42$ kV, $I = 84$ kA, pulse duration 50 – 70 ns, rise time about of 5 ns).

3 ELECTRON BEAM PARAMETERS

SILUND-21 will provide the electron beam with the following parameters: energy about of 10 MeV, peak current ~ 1 kA and pulse duration $\sim 50 - 70$ ns. Instant energy spread of electrons in the beam will be about of a fraction of per cent and the energy spread averaged over pulse duration will be $\sim 2 - 3$ %.

As a rule, the normalized emittance of the intensive electron beam is growing during acceleration process due to the nonlinearities of focusing field and strong space charge fields. The experience of work at our linear induction accelerators has shown that the emittance growth rate is saturated at the electron beam energy about of 2 – 3 MeV. If such a tendency takes place at higher energies, at the accelerator exit we may expect to obtain the values of the normalized emittance to be equal to 0.4π cm-rad, 0.15π cm-rad and 0.1π cm-rad at 90 %, 70 % and 50 % of the nominal value of the beam current.

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