

PROGRESS OF THE DIAMOND STORAGE RING AND INJECTOR DESIGN

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Abstract

DIAMOND is a state of the art 3 GeV synchrotron light source that will be available to users in 2007[1]. Considerable further progress has been made on the accelerator physics design of the storage ring, booster and other associated injector systems. Detailed analysis of injection processes, lifetime, coupling, instabilities, feedback systems and dynamic aperture have been undertaken driven by the procurement activity and the desire to fully understand all aspects of the accelerator's performance.

INTRODUCTION

DIAMOND is a new 3rd generation light source currently under construction near Oxford in the UK. The 3 GeV 560m circumference machine has twenty one free straights for insertion devices as well as the option of up to 24 dipole sources. The design features a small 2.7nm-rad emittance and coupling of 1% or less. Strong focusing and the relatively low symmetry of the machine produce difficult non-linear behaviour that must be optimised to maintain a good dynamic aperture and lifetime. The injector system includes a full-energy booster synchrotron with minimised apertures to reduce the stored magnetic energy. This is required in order to use switch-mode power supplies allowing flexible top-up operation. The limited aperture, coupled with a large energy ratio, leads to tight tolerances on booster injection errors and a requirement for careful control of the orbit and non-linear behaviour during the ramp. The requirement to operate in top-up injection mode in the future also produces stringent implications for the storage ring injection system, which must be designed for as close to unity injection efficiency as possible. Another key aspect of the machine's performance from the users' perspective is the quality of closed-orbit correction and instability correction systems to deal with orbit perturbations over a wide range of timescales.

INJECTION STUDIES

Booster Injection

The booster injection process is a single turn on-axis system using a fast kicker and a single septum. The effects of higher order magnetic field errors in all main magnet families, taken from 3D modelling, are included in the analysis, as well as realistic assumptions on the tolerances of the pulsed injection magnets (which leads to

an effective emittance increase). A realistic assumption on the beam loading from the linac is also included. The results show that the injection efficiency under semi-realistic conditions is an average efficiency of ~96%, sufficient for top-up injection.

The analysis also determined the likely loss points in the booster, and highlighted possible improvements to the design. It was seen that the highest losses occurred in the injection and extraction straights.

Storage Ring Injection

Injection into the DIAMOND storage ring has been simulated in more detail by tracking a realistic distribution of particles over the machine damping time. Non-linear effects have been included in the tracking and beam filamentation observed. A more precise calculation of beam stay-clear requirements for injection has been obtained, allowing beam stay-clear requirements around the storage ring to be finalised. The defining physical apertures have also been found, indicating the most likely locations for injection beam losses, although this is predicted to be negligible due to collimation in the booster-to-storage ring transfer line. Sufficient contingency has also been to allow for matched beta function errors at injection, and non-static errors in the injection pulsed magnets.

The injection straight layout and magnet specification have been revised in order to allow for the possible placement of collimators and additional diagnostics in the injection straight. The septum magnet has been specified at the reduced magnetic length of 1.67m, and increased maximum operational field of 0.9T. The septum pulse length is 160 μ s. The separation of the kicker magnets has been reduced from 1.98m to 1.75m, increasing their maximum operational field to 0.2T over the 5 μ s pulse. This has freed space to insert a vertical collimator between the 3rd and 4th kickers, a horizontal collimator after the 4th kicker, and an OTR screen after the septum. This layout is shown in Figure 1.

The horizontal position of the injection septum will be adjustable, and the useful range of adjustability of the septum has been investigated, as well as the impact on machine layout of introducing this adjustability.

The horizontal separation between storage ring axis and septum plate inner side will be adjustable between 12 and 20 mm, with the range of movement which will cover all scenarios of tune and dynamic aperture studied so far being 13 to 19 mm.

in the 168 sextupoles were used for correction. The correction method is based upon the analysis of the cross response matrix[3] and was set up to reduce linear coupling and the residual vertical dispersion. Using all 168 correctors the coupling was reduced to 0.15% on average. Due to the lowered Touschek lifetime, less aggressive schemes were considered. A system of 36 skew quadrupoles reduces the coupling to less than 0.8% whilst maintaining adequate lifetime.

CLOSED ORBIT FEEDBACK SYSTEMS

Booster

Closed orbit correction in the booster is provided by up to 22 horizontal and 22 vertical dipole corrector magnets positioned close to the F and D quadrupoles respectively, with up to 22 BPMs for position data. As in the storage ring, the correction scheme is global and uses the Singular Value Decomposition (SVD) technique. The magnets have the capability of being ramped, and can therefore provide accurate CO correction throughout the booster cycle. This has benefits for the required booster apertures.

Storage Ring

Closed orbit (CO) correction in the storage ring is to be performed using up to 168 of the dipole corrector magnets housed in the sextupoles and 96 dedicated fast correctors at the ends of the straight sections. Beam position information is provided by a state of the art BPM system, which is capable of delivering data with a resolution of $0.3\mu\text{m}$ [4]. The correction scheme is global, and uses the SVD technique to invert the machine response matrix.

The correctors in the sextupoles can deliver electron beam deflections of up to 0.8mrad full-swing at a frequency of 1Hz , and will be used predominately to tackle CO errors resulting from sources such as magnet imperfections and ground motion. Recent work has focussed on improving the correction scheme through the use of optimisation techniques such as genetic algorithms. Selection of the most efficient combination of corrector magnets, along with removal of inefficient Eigenvalues from the SVD significantly reduces the corrector strengths required, whilst also reducing the residual CO. Simulations using these techniques show RMS residual CO distortions of $50\mu\text{m}$ horizontally and $10\mu\text{m}$ vertically can be achieved in the straight sections, with maximum corrector strengths of 0.3mrad in both planes. The correctors in the sextupoles can also be used at higher frequencies to suppress higher frequency error sources, up to limits imposed by the power supplies and vacuum chambers of around 25Hz .

Dynamic CO errors are also tackled using the dedicated fast correctors in the straight sections. They are specified to give 0.3mrad full-swing deflections at 50Hz , and can be used as part of a global dynamic correction scheme operating at 100Hz . Simulations of the expected vibrations have shown the position and angle of the electron beam can be stabilized to less than $1/10$ of the beam dimensions at the source points using either the fast

correctors or the sextupole correctors, with the BPM resolution found to be the limiting factor.

The dedicated fast correctors can also be operated at higher frequencies as part of local correction or feed-forward systems, should the demands of a particular beam line require it.

COLLECTIVE EFFECTS

Current thresholds for microwave instability (MI) and transverse mode coupling instability (TMCI) were analysed to assess the impedance budget for DIAMOND operation in various modes. A 2D tracking code for the longitudinal dynamics in the presence of a broad band impedance (BBI) was used to determine the MI current threshold and the longitudinal BBI budget. For operation in multi-bunch mode, with a 500mA in a $2/3$ filling, the impedance was set to $Z/n\ 0.2\Omega$, corresponding to $6.3\text{k}\Omega$ at the cut off frequency of the beam pipe. A significant bunch lengthening is expected due to potential well distortion with a beneficial effect on Touschek lifetime. This is shown in Figure 2.

The effect of a third harmonic cavity on the instability threshold was computed numerically, and is shown in Figure 2. Although the bunch lengthens by a factor of 3, the simulations showed the microwave instability threshold could be increased only by a factor of 2.

The analysis of the current threshold for the TMCI was performed with the MOSES code[5] using a BBI model for the transverse impedance. Setting the current threshold to a single bunch operation, 0.8mA , an upper limit for the BB transverse impedance was found to be $3\text{M}\Omega/\text{m}$. The current threshold can be increased by setting large chromaticity values; however the impact of this procedure on the dynamic aperture, as well as a possible feedback system is under consideration.

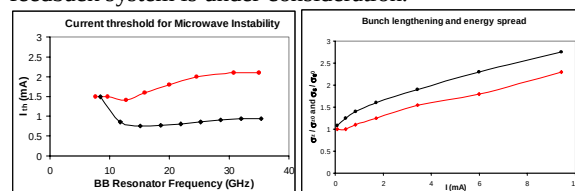


Figure 2: MI current threshold vs. resonator frequency with (red) and without (black) a 3HC (left) and the bunch lengthening (black) and energy widening (red) curves as a function of current (right) of a BBI modelled by an RLC resonator circuit

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