Theoretical Study of Emittance Transfer

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Liouville's theorem

- Suppose a dynamical system of multi-particles interacting each other.
- Define a probability density \overline{F} in Γ -space $(q_1, q_2, ..., q_n; p_1, p_2, ..., p_n); \overline{Fd\Gamma}$ ($d\Gamma = dq_1 dq_2 \cdots dq_n dp_1 dp_2 \cdots dp_n$) is the probability of finding the system in the region $(q_i, q_i + dq_i)$ and $(p_i, p_i + dp_i)$ where i = 1, 2, ..., n.
- <u>Provided that q_i's and p_i's satisfy the Hamiltonian equations of motion</u>, it is possible to show

$$\frac{\partial F}{\partial t} + \sum_{i=1}^{n} \dot{q}_{i} \frac{\partial F}{\partial q_{i}} + \sum_{i=1}^{n} \dot{p}_{i} \frac{\partial F}{\partial p_{i}} = 0.$$

n = 3N for a charged-particle beam consisting of N particles.

$$\longrightarrow \frac{DF}{Dt} = 0$$

An important statement of the incompressibility of the flow in phase space !

 $d\Gamma$ is an invariant.

Emittance

Beam emittance \equiv 6D phase-space (μ -space) volume occupied by a beam.

- *Emittance* is the most important parameter representing the beam quality.
- In standard accelerator theories, we explore the dynamical behavior of a beam in 6D phase space spanned by canonical coordinates $(x, y, z; p_x, p_y, p_z)$.
- The particle distribution function f in μ -space obeys

$$\frac{Df}{Ds} = \frac{\partial f}{\partial s} + x' \frac{\partial f}{\partial x} + y' \frac{\partial f}{\partial y} + z' \frac{\partial f}{\partial z} + p_x' \frac{\partial f}{\partial p_x} + p_y' \frac{\partial f}{\partial p_y} + p_z' \frac{\partial f}{\partial p_z} = \left(\frac{\partial f}{\partial s}\right)_{col}$$

The collision term appears in μ -space; thus, strictly speaking, the emittance is not $\longrightarrow \int d\mu$ is not an invariant ! conserved even without dissipation.

Emittance preservation

In many cases of interest to us, the collision term (in other words, the effects of intra-beam scattering) is negligible because an ordinary beam is very hot and thin.

 $\frac{Df}{Ds} \approx 0$: Emittance is an approximate invariant in accelerators !

- In order to improve the beam quality, we have to introduce dissipative interactions (cooling effect) into an accelerator.
- Typical electromagnetic elements (magnets, rf cavities, etc.) only provide conservative forces that never affect the 6D volume of a beam.
- Beam cooling is very difficult in practice.

Only few cooling techniques have been developed so far.

Why cooling?

 The volume occupied by a beam in phase space is the measure of *beam quality*.

A smaller volume means a higher quality.

• A particle accelerator is, in general, a conservative dynamical system.

The beam volume in 6D phase space is an approximate invariant.

We have to introduce a dissipative force into an accelerator, in order to improve the beam quality for users.

Cooling and damping

- Transverse projected emittances conventionally defined in *x*-*x*' and *y*-*y*' phase planes damp when the beam is accelerated (adiabatic damping).
- In one word, this is because a pair of variables (x, x') or (y, y') are not canonical conjugate where the prime stands for s-derivative, i.e. ' ≡ d/ds.
- Since a beam is accelerated in general by a conservative force (such as RF electric fields), the 6D emittance is certainly unchanged.



Do not confuse adiabatic damping with cooling !

Non-dissipative manipulation of μ -space

Concept of emittance manipulation

"Cooling" is difficult because the 6D volume of a beam is invariant in Hamiltonian systems.

It is much easier to manipulate 2D subspaces (emittance projections).

- We often consider projections of the 6D emittance onto 2D phase planes.
- *Projected emittances* of a beam are defined in $x-p_x$, $y-p_y$, and $z-p_z$ phase planes.
- In general, projected emittances are not invariant; it is easy to change them by introducing coupling potentials that correlate the degrees of freedom.



Coupling storage ring

A COMPACT STORAGE RING FOR THE OPTIMIZATION OF CHARGED-PARTICLE BEAMS IN 6D PHASE SPACE

- 2D subspaces are connected through various coupling potentials artificially controllable.
- Not only a full emittance exchange but also a partial emittance transfer are feasible.
- It is possible to develop various correlations between the three degrees of freedom.



Model

For the sake of simplicity, ignore the following effects:

- Interparticle interactions through the Coulomb fields
- Details of the lattice design (smooth approximation)
- Radiation, wakefields, etc.

The Hamiltonian of the dynamical system of interest to us can then be written as

$$H = \frac{1}{2} \left[p_x^2 + \left(\frac{v_x}{R} \right)^2 x^2 \right] + \frac{1}{2} \left[p_y^2 + \left(\frac{v_y}{R} \right)^2 y^2 \right] + \frac{1}{2} \left[p_z^2 + \left(\frac{v_z}{R} \right)^2 z^2 \right] + \phi_c(x, y, z; s).$$

 (v_x, v_y, v_z) : tunes

- *R* : average radius of the coupling ring
- ϕ_c : artificial coupling potential

Example:

$$\phi_c = g_1 x^m z^n \delta_p (s - s_1) + g_2 y^m z^n \delta_p (s - s_2)$$

In general, the coupling constants g_1 and g_2 are *s*-dependent; it is possible to change gradually or switch on and off individual coupling terms.

Resonant emittance transfer

- The coupling between the degrees of freedom can be strengthened by increasing the coupling constants.
- The enhancement of coupling is, however, almost useless for the present purposes.
- In order to achieve an efficient emittance transfer, the coupling ring must operate near resonances:

 $mv_x - nv_z \approx \text{integer},$

 $mv_{y} - nv_{z} \approx \text{integer},$

for the case where

 $\phi_c = g_1 x^m z^n \delta_p (s - s_1) + g_2 y^m z^n \delta_p (s - s_2).$



Invariants

• 2D (g_1 or $g_2 = 0$)

$$I_{2D} \equiv \frac{\mathcal{E}_{x(y)}}{m} + \frac{\mathcal{E}_z}{n} = \text{const.}$$

• 3D (full coupling)

$$I_{3D} \equiv \frac{\varepsilon_x + \varepsilon_y}{m} + \frac{\varepsilon_z}{n} = \text{const.}$$

We have again assumed:

 $\phi_c = g_1 x^m z^n \delta_p (s - s_1) + g_2 y^m z^n \delta_p (s - s_2).$

Different forms of the invariant can be found for different coupling potentials.

Scaling law :
$$g\left(\frac{R}{v_{\perp}}\right)^{\frac{m}{2}} \left(\frac{R}{v_{z}}\right)^{\frac{n}{2}} = \text{const.}$$

 $(g \equiv g_1 = g_2, v_{\perp} \equiv v_x = v_x)$

Third-order emittance transfer (m = 1, n = 2)



Equilibrium emittance ratio

In a 2D case where $g_2 = 0$, we can find another invariant by averaging the singleparticle motion near resonance, i.e. $\Delta \equiv (mv_x - nv_z - \ell) / R \approx 0$:

$$\bar{H} = \begin{cases} \Delta J \pm h_{mn} J^{n/2} (1-J)^{m/2} \cos \psi & \text{for } m+n = \text{even}, \\ \Delta J \pm h_{mn} J^{n/2} (1-J)^{m/2} \sin \psi & \text{for } m+n = odd, \end{cases}$$

where h_{mn} is a constant parameter, $J = \varepsilon_z / nI_{2D}$ and ψ is the relative phase variable conjugate to *J*. \overline{H} can be considered as the Hamiltonian of the averaged system. The equilibrium emittances are then given by

$$\varepsilon_x \approx \frac{m^2}{m+n} I_{2D}, \quad \varepsilon_z \approx \frac{n^2}{m+n} I_{2D}.$$

Assuming that an incident beam eventually come close to this equilibrium state,

$$\frac{\varepsilon_x}{\varepsilon_x(0)} \to \frac{1 + \frac{m}{n} \frac{\varepsilon_z(0)}{\varepsilon_x(0)}}{1 + \frac{n}{m}}, \qquad \frac{\varepsilon_z}{\varepsilon_z(0)} \to \frac{1 + \frac{n}{m} \frac{\varepsilon_x(0)}{\varepsilon_z(0)}}{1 + \frac{m}{n}}.$$

Emittance transfer and correlation

★ Example (linear case)

Second-moment matrix: $\mathbf{S} = \begin{pmatrix} \mathbf{S}_{xx} \\ \mathbf{S}_{yy} \end{pmatrix}$

The off-diagonal sub-matrices S_{vv} and S_{vv} describe correlation.

where \mathbf{S}_{ij} (*i*, *j* = *x*, *y*, *z*) are 2x2 sub-matrices such as $\mathbf{S}_{xx} = \begin{pmatrix} \langle x^2 \rangle & \langle xp_x \rangle \\ \langle p,x \rangle & \langle p^2 \rangle \end{pmatrix}$

✓ Projected emittances are defined as $\varepsilon_x^2 = \det \mathbf{S}_{xx}$ and $\varepsilon_y^2 = \det \mathbf{S}_{yy}$.

- ✓ The emittance (the 4D volume) is invariant and given by $\epsilon_{4D}^2 = \det \mathbf{S}$.
- ✓ With a transfer matrix **M**, the second moments are transformed to **MSM**^{*T*}.

Even if we start with an ordinary "uncorrelated" beam, the elements of the off-diagonal matrices become non-zero during an emittance transfer process where ε_{4D} and $\varepsilon_x + \varepsilon_y$ are both conserved. (At each moment of a full emittance exchange, the correlation disappears.)

Linear correlation in phase space

Example Linear coupling (m = n = 1) $(v_x, v_y, v_z) = (1.1, 1.1, 0.1)$ R = 1 $g_1 = g_2 = 0.01$

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Nonlinear correlation in phase space



Phase-space evolution



Coupling sources

The electromagnetic fields of typical coupling sources can be derived from vector potentials of the form $\mathbf{A} = \begin{pmatrix} 0, 0, A_z \end{pmatrix}$.

• Transverse - transverse

It is straightforward to develop linear and nonlinear couplings between the two transverse directions; we can employ various magnets such as a solenoid (linear), a skew quadrupole (linear), a sextupole (third-order), an octupole (fourth-order), etc.

For instance, $A_z = g_{skew} xy \delta_p(s)$ for a skew quadrupole magnet.

• Transverse - longitudinal

In order to couple the transverse motion with the longitudinal motion, we employ radio-frequency devices or momentum dispersion.

Linear coupling rf cavity (rectangular): $A_z \approx g_{rf} x \sin(\omega t) \delta_p(s)$

Nonlinear coupling rf cavity (cylindrical): $A_z \approx g_{rf} J_m \left(\zeta_{mn} \frac{r}{r_0}\right) \cos(m\theta) \sin(\omega t) \delta_p(s)$

(TM_{mn0} -mode operation)

Hamiltonian

• Coupling potential

$$A_{z} = \frac{p_{0}\Gamma_{q}}{qR}xy\delta_{p}(s-s_{q}) + \frac{V_{1}}{\omega}\left(\frac{\pi x}{a}\right)\sin(\omega t + \phi_{1})\delta_{p}(s-s_{1}) + \frac{V_{2}}{\omega}\left[1 - \left(\frac{\zeta_{01}}{2}\frac{r}{r_{0}}\right)^{2}\right]\sin(\omega t + \phi_{2})\delta_{p}(s-s_{2})$$

(Skew quadrupole)

(Linear coupling cavity)

(Third-order coupling cavity)

• Hamiltonian in betatron space

$$\begin{aligned} \hat{H} &= \frac{1}{2} \left(\frac{1}{\gamma_0^2} - \frac{D_x}{\rho} \right) \left(\frac{\omega \Delta \hat{E}}{\beta_0 c} \right)^2 + \frac{\hat{p}_x^2 + \hat{p}_y^2}{2} + \frac{1}{2} (K_x \hat{x}^2 + K_y \hat{y}^2) \\ &+ \frac{q V_b}{2 \omega p_0} \left[\hat{\psi} - \frac{\omega}{\beta_0 c} \left(D_x \hat{p}_x - D'_x \hat{x} \right) \right]^2 \delta_p (s - s_b) + \frac{\Gamma_q}{R} \left(\hat{x} + \frac{\omega D_x}{\beta_0 c} \Delta \hat{E} \right) \hat{y} \delta_p (s - s_q) \\ &- \frac{\pi q V_1}{a \omega p_0} \left(\hat{x} + \frac{\omega D_x}{\beta_0 c} \Delta \hat{E} \right) \left[\hat{\psi} - \frac{\omega}{\beta_0 c} \left(D_x \hat{p}_x - D'_x \hat{x} \right) \right] \delta_p (s - s_1) \\ &- \frac{q V_2}{\omega p_0} \left[1 - \left(\frac{\zeta_{01}}{2r_0} \right)^2 \left(\hat{x} + \frac{\omega D_x}{\beta_0 c} \Delta \hat{E} \right)^2 - \left(\frac{\zeta_{01}}{2r_0} \right)^2 \hat{y}^2 \right] \left[\hat{\psi} - \frac{\omega}{\beta_0 c} \left(D_x \hat{p}_x - D'_x \hat{x} \right) \right] \delta_p (s - s_1) \end{aligned}$$

Canonical variables : $(\hat{x}, \hat{y}, \hat{\psi}; \hat{p}_x, \hat{p}_y, -\Delta \hat{E})$

Application to FEL

Necessary conditions

Resonance Condition for FEL : $\lambda = \left(1 - \frac{v_z}{c}\right)\lambda_w \approx \frac{1 + K^2}{2\gamma^2}\lambda_w$

(*K* is the normalized strength of the undulator.)

- The transverse normalized emittance ε_n of the electron beam must be less than $\lambda / 4\pi$.
- The energy spread of the electron beam must be less than the FEL parameter ρ .
- The current of the electron beam should be high so as to make the FEL parameter large and the saturation distance short.

These conditions suggest that an optimization of the three projected emittances may improve the performance of an FEL system.

Emittance optimization

- The recent progress of accelerator technologies has made it feasible to produce a high-quality electron beam with a very low longitudinal emittance.
- The FEL gain is then limited mainly by the transverse beam quality.

Reduce ε_x and ε_y at the sacrifice of ε_z !





| Radiation wavelength λ [nm] | 6 |
|-------------------------------------|------|
| Beam energy [GeV] | 1 |
| Peak current [A] | 250 |
| Undulator period λ_W [cm] | 2 |
| Undulator parameter K | 1.14 |

Beam conditioning

Ideal resonant wavelength : $\lambda = \left(1 - \frac{v_z}{c}\right)\lambda_w \approx \frac{1 + K^2}{2w^2}\lambda_w$

• The FEL resonance condition for an electron with a finite transverse amplitude can be given by

$$\lambda pprox rac{1}{2} \left(rac{1+K^2}{\gamma^2} + rac{2J_x}{eta_x} + rac{2J_y}{eta_y}
ight) \lambda_w.$$

where $J_{x(y)}$ are the transverse actions.

- The energy (γ) of each individual electron is different from the ideal design value (γ_0) .
- Substituting $\Delta \gamma = \gamma \gamma_0$ into the above equation, we find that the number of resonant electrons increases considerably when the beam has the following correlation:

$$\frac{\Delta\gamma}{\gamma} = \kappa_x J_x + \kappa_x J_y,$$

where $\kappa_{x(y)}$ are the conditioning parameters; when $\kappa_x = \kappa_y$, we have $\kappa_x = (\lambda_w / \lambda) / 2\beta_x$.



Radiation wavelength $\lambda = 6$ nm $\lambda_w = 2$ cm; K = 1.14 nm; Beam energy=1 GeV Transverse normalized emittance $\varepsilon_x = \varepsilon_y = 3 \mu m$

A possible conditioning in a coupling ring

Third-order emittance transfer (m = 2, n = 1)





Phase-space evolution (mismatched)



GENESIS result



Summary

- Non-dissipative manipulation of charged-particle beams should be useful in practice.
- An efficient emittance transfer is achievable by resonantly coupling the degrees of freedom.
- A coupling storage ring enables one to optimize the ratios of three projected emittances for specific purposes.
- Various linear and nonlinear correlations in phase space can naturally be developed during an emittance transfer process.

The present method thus offers a possibility of controlling charged-particle beams in 6D phase space; an optimization of not only emittance ratios but also detailed structures of particle distributions in subspaces may be feasible.