

ABSTRACT

The superconducting parallel-bar cavity is a deflecting/crabbng cavity with attractive properties, compared to other conventional designs, that is currently being considered for a number of applications. The new parallel-bar design with curved loading elements and circular or elliptical outer conductors have improved properties compared to the designs with rectangular outer conductors. We present the designs proposed as the deflecting cavities for the Jefferson Lab 12 GeV upgrade and for Project-X and crabbng cavities for the proposed LHC luminosity upgrade and electron-ion collider at Jefferson Lab.

INTRODUCTION

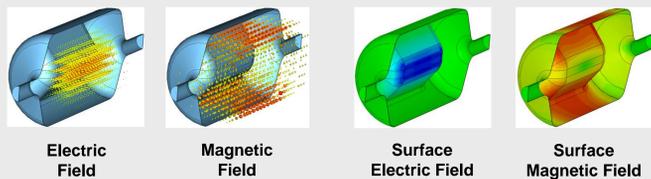
The superconducting parallel-bar cavity [1] geometry with a cylindrical outer conductor and trapezoidal shaped bars is proven to have better properties compared a variety of geometries with rectangular, cylindrical and elliptical outer conductors and straight, curved bars [2, 3].

The geometry has

- lower and balanced surface fields
- higher shunt impedance
- wider mode separation in the HOM spectrum

Field Profile

Surface Fields

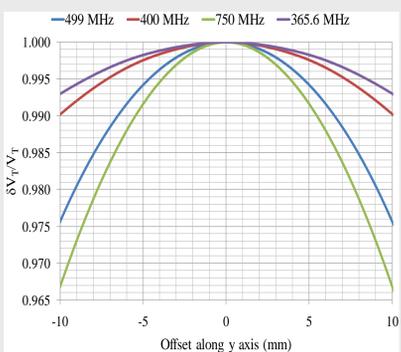
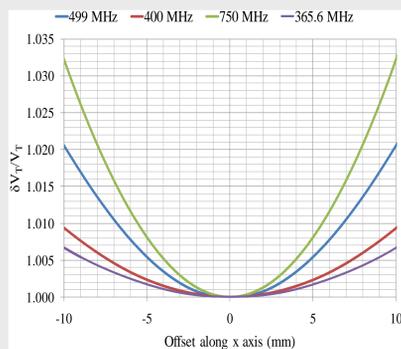


Applications of the Parallel-Bar Cavity

- 499 MHz deflecting cavity for the Jefferson Lab 12 GeV upgrade
- 400 MHz crabbng cavity for the proposed LHC luminosity upgrade
- 750 MHz crabbng cavity for medium energy electron ion collider (MEIC) at Jefferson Lab
- 365.625 MHz deflecting cavity for Project-X

ANALYSIS OF FIELD NON-LINEARITY

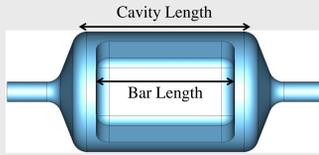
- Change in the transverse voltage across the beam aperture is determined in horizontal (along x axis) and vertical (along y axis) directions
- If needed, the non-linearity can be reduced by increasing the inner bar height and/or by giving it a curvature



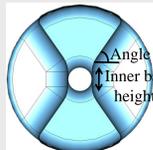
DESIGN OPTIMIZATION AND PROPERTIES FOR EACH APPLICATION

Design Optimization

- Cavity length and bar length is optimized to lower peak surface electric (E_p) and magnetic (B_p) fields



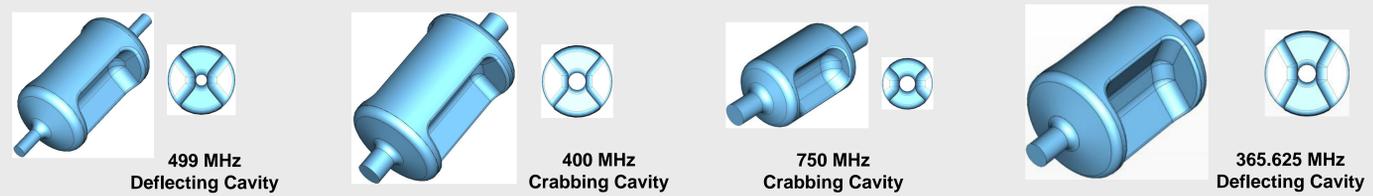
- Shape of the bar is optimized for lower and balanced surface fields by changing the inner bar height and angle



| Parameter | 499 MHz | 400 MHz | 750 MHz | 365.6 MHz | Units |
|----------------------------------|--------------------|-------------------|-------------------|-------------------|------------|
| Frequency of π mode | 499.0 | 400.0 | 750.0 | 365.625 | MHz |
| $\lambda/2$ of π mode | 300.4 | 375.0 | 199.9 | 410.0 | mm |
| Frequency of 0 mode | 1035.9 | 729.5 | 1314.4 | 659.7 | MHz |
| Frequency of near neighbour mode | 771.2 | 593.4 | 1143.1 | 571.9 | MHz |
| Cavity length | 440.0 | 520.0 | 300.0 | 530.0 | mm |
| Cavity diameter | 241.9 | 339.8 | 193.0 | 388.4 | mm |
| Bars length | 260.0 | 345.0 | 185.0 | 350.0 | mm |
| Bars inner height | 50.0 | 80.0 | 57.5 | 85.0 | mm |
| Angle | 50.0 | 50.0 | 36.2 | 55.0 | deg |
| Aperture diameter | 40.0 | 84.0 | 60.0 | 84.0 | mm |
| Deflecting voltage (V_T^*) | 0.3 | 0.375 | 0.2 | 0.41 | MV |
| Peak electric field (E_p^*) | 2.96 | 3.82 | 4.95 | 3.61 | MV/m |
| Peak magnetic field (B_p^*) | 4.49 | 7.09 | 8.74 | 6.41 | mT |
| B_p^* / E_p^* | 1.52 | 1.86 | 1.77 | 1.77 | mT/(MV/m) |
| Energy content (U^*) | 0.029 | 0.19 | 0.056 | 0.19 | J |
| Geometrical factor | 105.6 | 119.7 | 136.9 | 115.9 | Ω |
| $[R/Q]_T$ | 982.2 | 312.2 | 152.9 | 378.5 | Ω |
| $R_p R_s$ | 1.04×10^5 | 3.7×10^4 | 2.1×10^4 | 4.4×10^4 | Ω^2 |

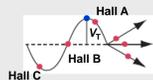
At $E_T^* = 1$ MV/m

CAVITY DESIGNS FOR EACH APPLICATION



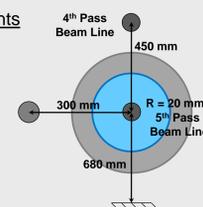
499 MHz DEFLECTING CAVITY

- Is required to separate the 11.025 GeV beam into 3 beams



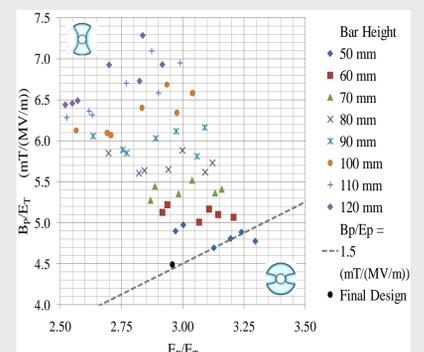
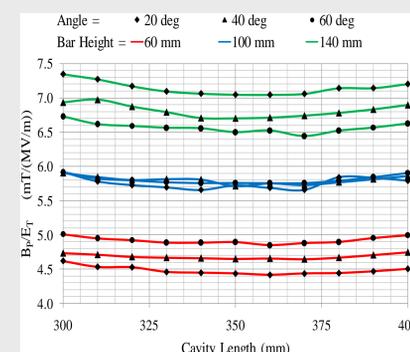
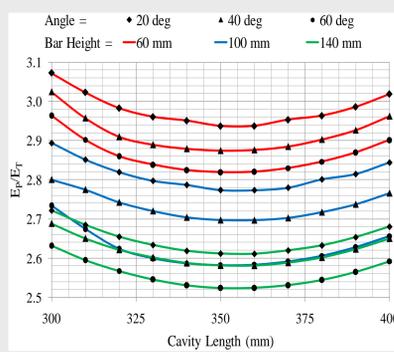
- Required peak transverse voltage = 5.6 MV

Dimensional Constraints



- Shape of the bar is optimized to achieve a field balancing ratio of $B_p/E_p=1.5$ mT/(MV/m)

| E_p/E_T | B_p/E_T (mT/(MV/m)) | E_p at $V_T=3$ MV | B_p at $V_T=3$ MV |
|-----------|--------------------------|------------------------|------------------------|
| 2.96 | 4.49 | 30 MV/m | 45 mT |



CONCLUSION

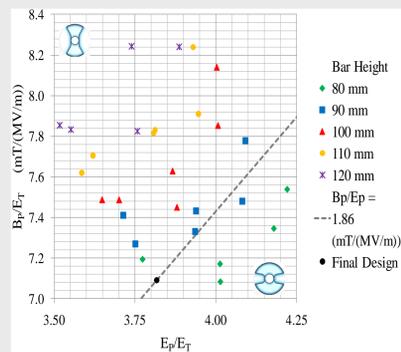
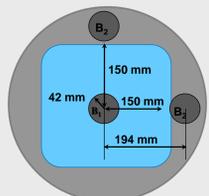
The parallel-bar geometry with the cylindrical outer conductor and trapezoidal shaped bars has proven to have improved properties compared to other parallel-bar geometries, therefore have been considered for a number of deflecting/crabbng cavity applications. This geometry is capable of delivering lower and well balanced peak surface fields with higher shunt impedance. Another attractive feature is the fact that this geometry has no lower-order mode and the nearest higher-order mode is far removed from the fundamental mode [3]. The shape of the bars connecting to the outer conductor with sloped end plates adds rigidity to the design in terms of mechanical deformations [4]. The parallel-bar geometry for the applications of the 499MHz and 365.625 MHz deflecting cavities and 400 MHz crabbng cavities have shown very attractive properties in meeting the requirements. The 499 MHz deflecting and 400 MHz crabbng cavities are in the stage of prototype fabrication [4].

400 MHz CRABBING CAVITY

- Required peak transverse voltage = 10 MV

- Shape of the bar is optimized to achieve a field balancing ratio of $B_p/E_p=1.86$ mT/(MV/m)

Dimensional Constraints



| E_p/E_T | B_p/E_T (mT/(MV/m)) | E_p at $V_T=3.4$ MV | B_p at $V_T=3.4$ MV |
|-----------|--------------------------|--------------------------|--------------------------|
| 3.82 | 7.09 | 34.6 MV/m | 64.3 mT |

750 MHz CRABBING CAVITY

- Is required for head on collision of the 60 GeV proton beam and the 12 GeV electron beam

- Design is very compact and has higher surface fields

365.625 MHz DEFLECTING CAVITY

- Is required to separate the 3 GeV proton beam into 3 beams

- Required peak transverse voltage = 10 MV

- Shape of the bar is optimized to achieve a field balancing ratio of $B_p/E_p=1.77$ mT/(MV/m)

| E_p/E_T | B_p/E_T (mT/(MV/m)) | E_p at $V_T=3.4$ MV | B_p at $V_T=3.4$ MV |
|-----------|--------------------------|--------------------------|--------------------------|
| 3.61 | 6.41 | 30.0 MV/m | 53.2 mT |

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