

# PRELIMINARY TEST RESULTS FROM 650 MHz SINGLE CELL MEDIUM BETA CAVITIES FOR PROJECT X\*

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## Abstract

We have fabricated two single cell 650 MHz  $\beta = 0.61$  cavities of a JLab design [1], which possibly can be used for the proposed Project X proton linac application. Both cavities were manufactured at JLab from RRR>250 niobium sheet of 4 mm thickness using standard techniques such as deep drawing, electron beam welding, buffered chemical polishing, hydrogen degassing heat treatment, high pressure ultrapure water rinsing and clean room assembly. A detailed description of the design and fabrication procedures is forthcoming [2].

Initially cavity #1 was – after final surface treatment by buffered chemical polishing (BCP) – measured without any provisions for stiffening. As expected, the pressure sensitivity and the Lorentz Force detuning coefficients were relatively high; however, the RF performance was very encouraging: the cavity exhibited a Q-value  $> 10^{11}$  at 1.6K, corresponding to a residual resistance of  $< 1.5$  n $\Omega$ . The initial gradient was limited to  $E_{acc} \sim 18$  MV/m, limited by field emission.

In a subsequent test, the cavity was re-rinsed and stiffened up, resulting in a somewhat improved mechanical behavior, but no improvement in rf performance. The second cavity was also tested twice-before and after low temperature baking. The results from all tests are reported in this contribution.

## INTRODUCTION

Project X is a multi-MW proton accelerator - complex proposed to be built at Fermi National Accelerator Laboratory based on a CW H<sup>-</sup> linac utilizing superconducting cavity technology. In the present early design stage many national laboratories as well as international partners from Indian, European and Asian institutions are supporting this effort.

The presently proposed layout as outlined in the P5 report of the High Energy Physics Advisory Panel envisages three low beta, 325 MHz spoke cavity sections, two families of medium beta ( 0.61 and 0.9), 650 MHz elliptical-type 5-cell cavities and a final beta=1 section of 1300 MHz 9-cell ILC-type cavities. J Lab has proposed a 5-cell cavity design for the beta=0.61 section as an alternative to an existing FNAL design. One of the major differences of the JLab design to the FNAL designs an increased beam aperture, which has some advantages with respect to cell-to-cell coupling, mechanical stability, less

field flatness distortions, chemical surface treatment, reduced possibility for HOM trapping and HOM field tilts to name a few. However, this larger iris diameter does not come without the expense of sacrificing some the rf properties of the structure. In table 1 the major properties of both designs are listed:

Table1: Comparison between a JLab and FNAL 5-cell,  $\beta=0.61$  cavity design for Project X

Parameter	Unit	JLab	FNAL
# of cells		5	5
Frequency	MHz	650	650
Iris aperture	mm	100	83
Equator diameter	mm	380.4	389.9
Active length	mm	694	705
c-to-c coupling	%	1.4	0.75
G	$\Omega$	190	191
R/Q	$\Omega$	296.6	378
$E_{peak}/E_{acc}$		2.71	2.26
$B_{peak}/E_{acc}$	mT/(MV/m)	4.78	4.21

## CAVITY FABRICATION

Both cavities – “A” and “B” – were fabricated from 4 mm thick high purity niobium sheet of RRR>300 by standard fabrication techniques:

After the deep drawing of the half cells from round discs, the half cells were trimmed for iris and equator butt welds. Beam pipes were rolled from reactor grade niobium and welded along the seams. After trimming and attachment of the flanges made from NbTi flanges by EWB they were welded to the half cells with an interpenetrating inside/outside electron beam weld. Prior to the final equator weld the half cell subassemblies were inspected for surface imperfections, which were removed by mechanical grinding with a fibrous wheel with embedded Al<sub>2</sub>O<sub>3</sub>.

During the fabrication sequence the mechanical dimensions were carefully monitored and the frequencies of the half cells were recorded. This information is of importance for the fabrication of multi-cell cavities, if one wants to minimize the amount of “after fabrication” tuning to achieve the appropriate frequency and a “flat” field.

In preparation for the cryogenic testing the cavities received a bulk removal of the damage layer by BCP (app. 250  $\mu$ m) and a 600C, 10 hr hydrogen degassing heat treatment. Wall thickness measurements at 12 points on the cavity surface were carried out before and after the bulk chemistry to determine the actual material removal.

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## FINAL TREATMENT AND TESTING

Prior to the cryogenic testing, both cavities received the same final surface treatment after the hydrogen degassing: an ultrasonic degreasing in soap/water solution (“Micro”) was followed by 50  $\mu\text{m}$  of BCP, rinsing in hot and cold water and a subsequent high pressure ultrapure water rinsing (HPR).

The respective cavity was dried in our class 10 clean room for app. 12 hrs before the auxiliary parts ( input coupling probe/pump-out port and transmission probe), which were carefully clean by blowing off remaining particles with nitrogen, were attached with AlMg- gaskets. The cavity was attached to the test stand (see Figure 1) in front of a laminar flow wall and evacuated for  $\geq 12$  hrs.



Figure 1: Cavity assembled to test stand; as discussed below, an attempt was made to stiffen up the cavity with Ti rods.

### Cavity “A”

This cavity was tested and assembled three times; between the tests only HPR was applied.

#### Test #1

The cavity vacuum prior to cooldown was  $p=1.2 \times 10^{-8}$  mbar and improved to  $< 5 \times 10^{-9}$  mbar at 4.2K. During this test the Q-value was measured between 4.2K and 2K to derive the temperature dependence of the surface resistance. Simultaneously data for the pressure sensitivity of the cavity were taken. At 2K then the Q-value as a function of the accelerating gradient was measured.

Two circumstances made the test quite difficult: the  $Q_{\text{ext}}$  of the input probe was quite high, which challenged the rf system ( locking the cavity), especially – as it turned out – since the frequency of the cavity shifted significantly with

decreasing He- bath pressure. Additionally, the Q-value of the cavity was unexpectedly very high at the lower temperatures and e.g. at 2K the bandwidth of the cavity was only  $\sim 1/100$  Hz. However, this circumstance reduced the error of the Q- measurement, because a large part of  $Q_0$  came from the decay time and errors in coupling factor Measurements were minimized. Therefore, the high Q-values are quite believable. Figure 2 shows the best fit of the R(T) data to the BCS theory, based on the program of ref. [3].

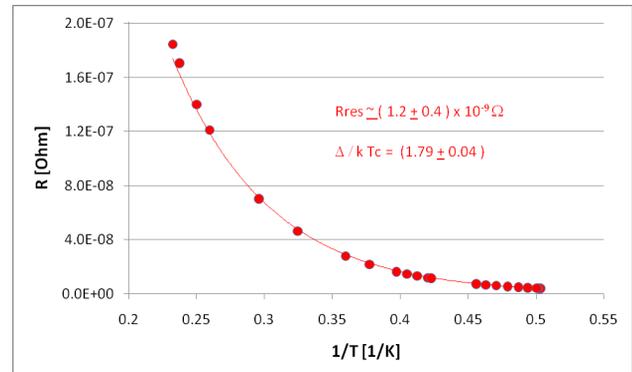


Figure 2: Temperature dependence of the surface resistance; the values for residual resistance and energy gap are obtained from a best fit to BCS with fixed parameters for  $T_C=9.25\text{K}$ , coherence length  $\xi = 62$  nm and London penetration depth  $\lambda_L = 32$  nm.

As shown in Figure 3, the cavity frequency shifted significantly with decreasing He bath pressure. Resulting in a sensitivity coefficient of  $\Delta f/\Delta p \sim -4.4$  kHz/mbar. Because of the large frequency shifts an attempt was made in the subsequent tests to stiffen up the cavity as discussed below.

At 2K the  $Q_0$  vs  $E_{\text{acc}}$  curve was measured; as can be seen in figure 4 the initially high Q-value of  $4 \times 10^{10}$  degraded rapidly at  $\sim 11$  MV/m, caused by a combination of strong field emission, which initially processed quite rapidly, and insufficient helium level in the dewar. Because of time constraints the test was aborted and a 2nd test with increased input coupling was carried out.

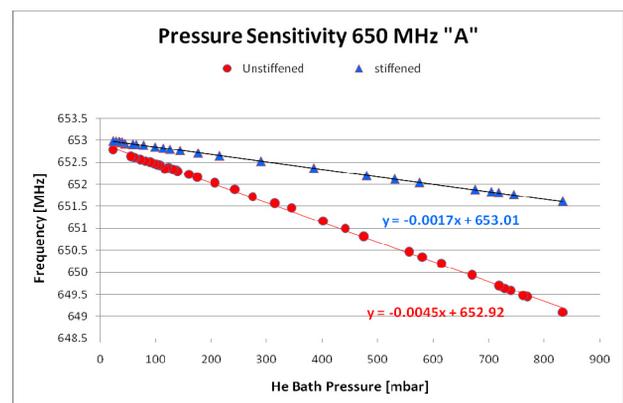


Figure 3: Pressure sensitivity of the single cell cavity, without stiffening and with stiffening (Figure 1) as discussed below.

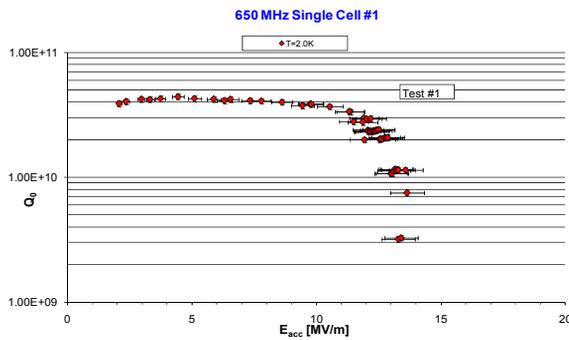


Figure 4:  $Q_0$  vs  $E_{acc}$  in the first test with cavity "A".

The rather high Lorentz Force detuning of  $\sim -63$  Hz/(MV/m)<sup>2</sup> for the unstiffened cavity "A" and the slight improvement for the stiffened cavity "B", test #1 (see below) is shown in figure 5:

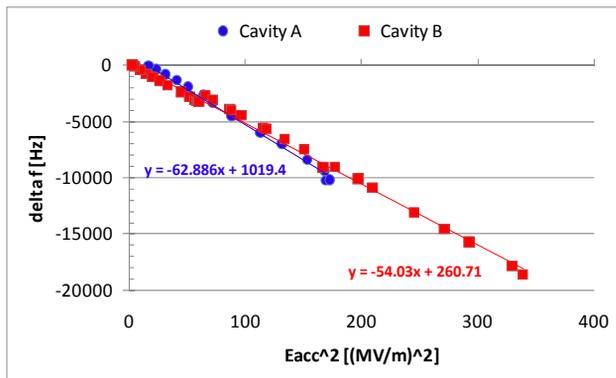


Figure 5: Lorentz Force detuning for the unstiffened cavity "A" and the stiffened cavity "B". The stiffening did not significantly improve the mechanical properties of the cavity.

Test #2

After disassembly, adjustment of coupling probes, re-rinsing and re-assembly the cavity was tested again in a second test, this time with stiffeners as shown in Figure 1. Vacuum conditions were very similar to the one's in test #1.

In this test the bath temperature was lowered to 1.6K in order to get more data points for the R(T) evaluation.

Unfortunately, the cavity was now heavily overcoupled; but nevertheless, the high  $Q_0$ -values from test #1 were re-confirmed, and at 1.6K the  $Q_0$  exceeded a value of  $10^{11}$ . This is one of the highest  $Q_0$ -values obtained on a niobium cavity. Data for  $Q_0$  vs  $E_{acc}$  were taken at three temperatures - 2K, 1.8K and 1.6K. Because of the excellent cavity performance with respect to  $Q_0$ , the cavity was tested subsequently with the SNS 805 MHz rf system – the initial test were carried out with our R&D rf system. Here, a relatively light multipacting barrier appeared between 7-8 MV/m, which could be processed within  $\sim 30$  min.

Within the rather large error bars caused by the highly overcoupled condition of the cavity, both rf systems gave comparable results, giving confidence in the measured cavity performance. Figure 6 shows  $Q_0$  vs  $E_{acc}$  as measured with the R&D system. Added to the graph is the measurement with the 805 MHz system at 2K. It became obvious that the stiffening attempt was not very successful with respect to the Lorentz force detuning – see Figure 5, comparing the results for both stiffening cases. This is no real surprise, since the deformations due to Lorentz forces take place at the cells and an effective stiffener has to be attached between cells and beam pipes. Similarly, the pressure sensitivity was not significantly affected and only a factor of  $\sim 2.6$  could be obtained as shown in Figure 3.

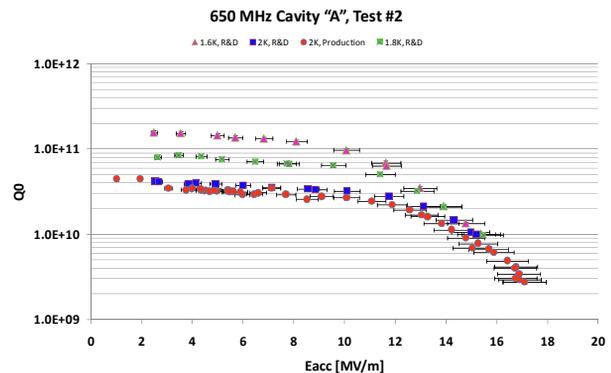


Figure 6:  $Q_0$  vs  $E_{acc}$  at 2K, 1.8K and 1.6K. Added in the figure are the data at 2K taken with the 805 MHz "production" system.

Test #3

For this test the  $Q_{ext}$  of the input coupler was re-adjusted to a value of  $\sim 2 \times 10^{10}$ ; the cavity went through the same procedures as in test #2 – only HPR was applied in anticipation of reducing the onset of field emission. However, no improvement could be realized. As a matter of fact, the residual resistance had nearly doubled, resulting in a Q – degradation at 2K to  $Q_0 \sim 3 \times 10^{10}$  and the cavity exhibited this time a strong MP barrier at 7-8 MV/m, which would not process. Therefore the test was aborted and in a future test we are planning to improve the cleaning and assembly procedures.

Cavity "B"

This cavity received for the initial test the same treatment as cavity "A". Consequently, its behavior was not very different from cavity "A": the Q- value at 2K was somewhat lower –  $Q_0$  (2K)  $\sim 3 \times 10^{10}$  – still corresponding to a residual resistance  $\leq 3 \times 10^9 \Omega$ . The MP barrier around 8 MV/m processed rather easily and a gradient of  $E_{acc} \sim 19$  MV/m was reached, limited by FE in the absence of a quench, which raised the expectations of higher gradients after a 120 C "in situ" baking. The result after the application of the baking is shown in Figure 7 together with the initial performance. As can be seen, not

only was a significant Q-value improvement realized, but also a higher gradient was measured. The Q-degradation at the high field is to a large extent caused by the “Q-drop” ( $H_{\text{peak}} \sim 100$  mT) added by some field emission.

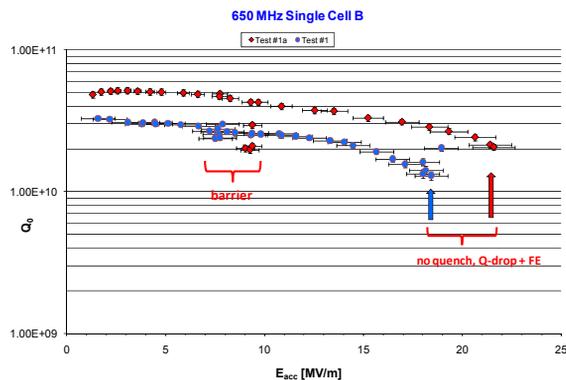


Figure 7: Performance of cavity "B" in test #1,  $T = 2\text{K}$ .

## SUMMARY AND CONCLUSION

Both cavities of the JLab design performed quite well – in particular very high  $Q_0$ -values (low residual resistances) were obtained. In Cavity “A” a seldom achieved  $Q_0 > 10^{11}$  was measured at 1.6K. It is not yet clear, why both cavities exhibited these low residual resistances compared to more common values of a factor of  $\sim 2$ -3 larger [4]; however, during the fabrication and during the subsequent handling, treatment and final surface preparation, meticulous care was taken of the niobium surfaces and the high  $Q_0$ -values might be the result of this.

As the test results showed, both cavities suffered from field emission and one of the goals for future tests is to extend the onset of field emission by improved rinsing and assembly procedures. On the other hand one should not forget, that the highest field obtained in test #1 with cavity “B” corresponds to a surface electric field of  $E_{\text{peak}} > 51$  MV/m. None of the cavities quenched, which raised the expectations of further improvements in  $E_{\text{acc}}$ .

As expected, the single cell cavities are mechanically not very stable, presumable because of the flat cell profile, which resulted in large coefficients for pressure sensitivity and Lorentz Force detuning. However, for prototyping stiffening was ignored with the intention to simplify the fabrication while scrutinizing RF properties. From the beginning it was however considered mandatory to stiffen the 5-cell cavities e.g. as practiced for ILC/TESLA cavities or SNS structures. We hope to receive funding to fabricate a multi-cell structure based on these initial encouraging results.

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