

TUPB006

Impedance Optimization of Sirius Stripline Kicker

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Abstract

Two approaches to design a transverse feedback (TFB) stripline kicker are well known in the accelerators community: one with bare strips in a tapered cavity and other whose shrouded strips are ended with parallel-plate capacitive gaps. This work presents a comparison between both models in terms of electromagnetic performance, proposes alternative solutions for increasing the gap capacitance and analyzes the performance of a hybrid stripline kicker design.

1. Geometry Alternatives



Figure 1: Considered transverse profiles: a) Bare Strip (g_1 = 1.09) and b) Shrouded Strip (g_{\perp} =1.01) designs.



Table 1: Geometric single-bunch (Eq. 1)

2. S1,1 Optimization



Figure 6: S1,1 parameters evolution stages. In the first (blue curve), a rectangular waveguide (WG), centered with the pin, was inserted between the coaxial line and the gap teeth in order to add an inductive component, but was not enough for achieving the desired goal. In the second stage (green & red curves), as

shown by Fig. 7, two alternative geometries for reducing the gap capacitance have been



multi-bunch (Eq. 2) loss factor and comparison among the three designs from Fig. 1, for two bunch length σ_s scenarios.

	Geon	netric κ _{loss} , mV/pC			
Geometry	σ _s = 2.65 m		$\sigma_s = 3.8 \text{ mm}$		
Туре	SB	MB	SB	MB	
Tapered Cavity	614.7	559.7	423.9	361.6	
Capacitive Gap	74.9	43.2	48.5	21.8	
Hybrid	131.2	75.3	84.9	40.6	

Table 2: Geometric SB and MB loss

factor comparison among the four

designs from Fig. 4, for two bunch

Gap Type $\sigma_s = 2.65 \text{ mm}$ $\sigma_s = 3.8 \text{ mm}$

40

Geometric κ_{loss}, mV/pC

SB

48.5

30.8 8.2

24.6 23.7

MB

21.8

length scenarios.

Sliding 45.2

Comb-type 35.5

Standard

Figure 2: Simulation models of three different stripline concepts. a) The Tapered Cavity Stripline (based on NSLS-II design) consists of Bare Strips (see Fig. 1) placed inside a 1/15 linearly tapered cavity that reaches the 24 mm diameter vacuum chamber profile on both ends. b) The Capacitive Gap one (based on SOLEIL design), consists of Shrouded striplines (see Fig. 1) with 0.5 mm capacitive gaps at both ends and follows the vacuum chamber profile. c) The Hybrid design consists of the Bare Strips ended by capacitive gaps. In the horizontal plane, the round profile gets complete after the 1/15 taper.



designed. Both reached -16.4 dB (15%) maximum within the 250 MHz BW.



Geom. 2 was preferred: 55.15 mV/pC and 42.91 mV/pC SB and MB loss factors, respectively. Geom 2: 29% and 84% higher.

Figure 7: a) Geom. 1 has the gap between teeth b = 0.7 mm and the lateral gaps increased. b) Geom. 2 has 4 teeth instead of 6 and kept the comb-type geometry parameters a-d to their original values.



Figure 8: Feedthrough pin holder considered in the simulations.

(4)

3. Vertical Shunt Impedance



Figure 9: Shunt impedance obtained from Eqs. 3 and 4 (cyan curve) compared with the ones from Eq. 4 and simulated vertical coupling impedances for Geometry 2 (red asterisk) and original Comb-type Gap design (brown triangle). Good agreement was found.

The gap capacitance interferes with the shunt impedance frequency response by distorting the symmetry of the vertical impedance's fundamental mode.



Figure 3: Real part of longitudinal impedance of the Tapered Cavity, Capacitive Gap and Hybrid striplines.

Despite stronger HOMs, Capacitive Gap type was chosen since its feedthroughs receive lower beam load. Alternative gap geometries were further analysed, as shown by Fig. 4



Figure 4: Considered alternative gap types for increasing the gap capacitance and allowing

alternative mechanical solutions for expected thermal expansions. a) Standard Gap: previous Capacitive Gap. b) Sliding Gap: 1 mm longitudinal gap, 0.5 mm thick alumina ceramics. c) Upper Gap: 20 mm long and 1 mm thick alumina ceramics. d) Comb-type Gap: *a* = 5 mm, *b* = 0.5 mm, *c* = 2mm and *d* = 10 mm.

 $Z_{\perp}(k) = \frac{g_{\perp}^2 Z_{ch,\perp}}{kr^2} [\sin^2(kL) + j\sin(kL)\cos(kL)] \quad (3)$

$4 \times \text{Re}(Z_{\perp}(k))$ $R_{sh}^{\perp} =$

4. Thermo-mechanical Analysis

Using GdfidL resistive wall (RW) boundary conditions (for $I_{av} = 500$ mA and $\sigma_s = 2.65$ mm):

 $P_{\text{loss}} = \frac{2\pi}{M\omega_0} \left(\kappa_{\text{loss,RW}}^{\text{MB}} - \kappa_{\text{loss,geom}}^{\text{MB}} \right) I_{\text{av}}^2 = 5.86 W$

Still more conservative!

Tabl

Fee

e 3: Dissipated power among the geometry parts.						
Component	Material	Power, %	Power, W			
v. + end pipes	SS	33.17	3.888			
avity ridges	SS	39.97	4.685			
+ outer coax.	SS	2.91	0.341	/		
tripline (SL)	Cu	8.57	1.004			
SL teeth	Cu	1.48	0.173	•	Fi	
amber teeth	SS	10.85	1.271		st	
dthrough pins	SS	1.04	0.122		a	
Holder slits	SS	0.53	0.062		tł	
older–center	SS	1.01	0.118		W	
older–sides	SS	0.47	0.055		is	

50,76 Max (left) Figure 11: Thermal and



igure 10: Mechanical design of the ripline kicker. A 5 mm thick lumina washer was considered in ne feedthrough. Commercial ones vill be used and a kicker prototype scheduled for late this year.





Figure 5: Comparison between the real part of longitudinal beam impedance of the Standard, Sliding, Upper and Comb-type Capacitive Gap striplines.

Comb-type Gap was chosen due to low loss factor, weak HOMs and since no ceramics brazing is needed.

mechanical (right) simulations, where 80x distortion magnification is shown. Mechanical results provides longitudinal gap 20 only μm contraction and also shows that the holder was not optimized in order to avoid the pin bending. Even though 41,07 Min

the found von Misses equivalent stress (80 MPa) is much below ceramics breaking point, the pin holder will be optimized to reduce the stresses at the feedthrough.

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