

# Argonne In-flight Radioactive Ion Separator

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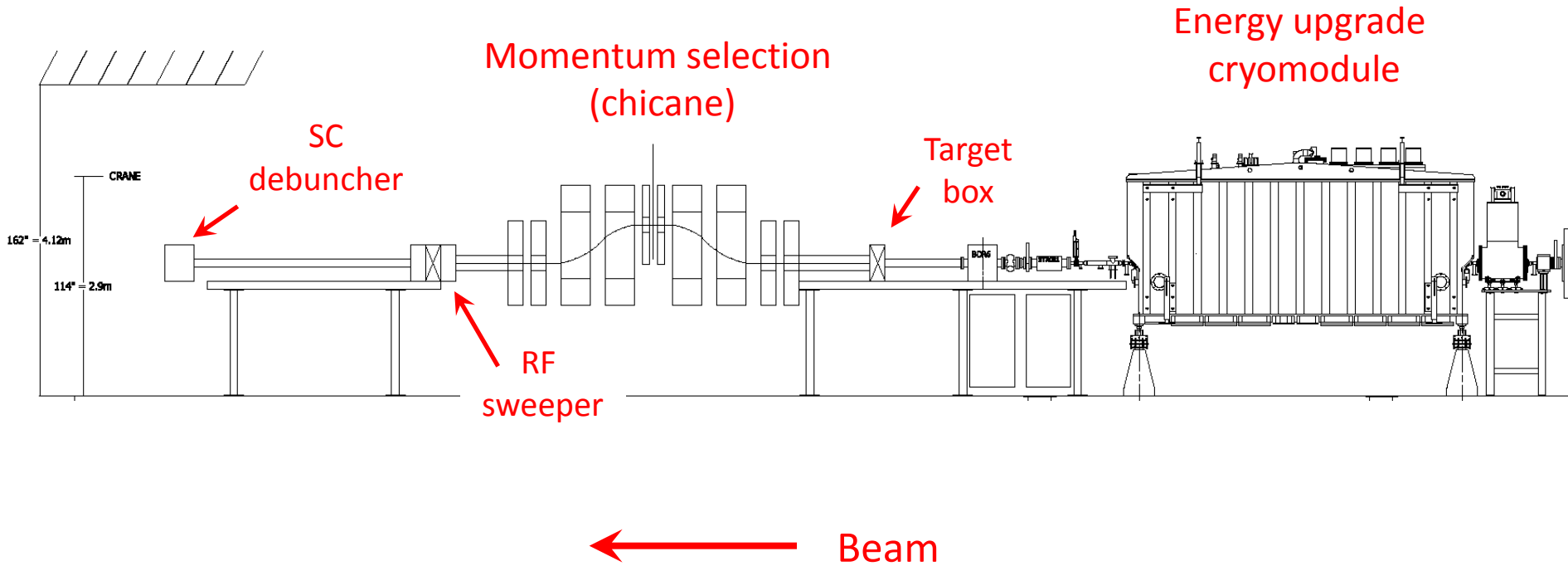
# Introduction

- The Argonne In-flight Radioactive Ion Separator (AIRIS) is a new large recoil separator that is being designed as a part of proposed future upgrade of the ATLAS facility
- It will provide at least **10 times** more collection efficiency than the existing system
- In combination with other proposed upgrades it will provide a **2 orders** of magnitude gain in the intensity for the in-flight produced secondary beams compared to the existing facility
- The resulting unprecedented intensities for the recoil beam open new opportunities in several physics domains, e.g. gamma ray spectroscopy after secondary reactions, reactions for rp-, vp-,  $\alpha$ p- processes and CNO cycle

beam	reaction	I (pnA)	E(pro) (MeV)	sigma (mb)	thickn. mg/cm2	N_prod counts/s	ch. st.	F(q)	E(rib) MeV	DE(r) fwhm	E(pr) MeV	DE(p) fwhm	N(max) /sec	achieved /sec	contaminants (rate multiplier)
14O	1H(14N,14O)n	1000	140	8	1.5	4.50E+07	8	1	124	3	132.5	0.1	4.50E+07	1.00E+05	14N, 11C(6)
33Cl	2H(32S,33Cl)n	1000	200	75	3	4.00E+08	15 16	0.3	145	7	150	0.2	1.00E+08	2.00E+04	32S, 33S(5)
56Ni	12C(52Cr,56Ni)4n	1000	450	60	1.2	2.20E+07	25 26	0.3	340	16	391	0.7	6.70E+06	2.00E+04	52Cr,56Co(10), 57Co(10),57Ni(2)
19O	2H(18O,19O)p	1000	180	37.5	3	2.10E+08	8	1	169	3	170	0.1	2.10E+08	2.00E+05	18OA



# Conceptual layout of in-flight separator upgrade



- The proposed design for the AIRIS device is based on four multipole magnets and four dipole magnets arranged in a so called broadband spectrometer configuration
- This arrangement will be followed by two RF cavities to provide further selection based on velocity differences between the primary beam tail and the recoiling RIB

# Design using multipoles

- Max quad poletip field=1.5T
- Half aperture=10cm
- Max Dipole field=1T
- Angle=22.5deg
- Radius=1m
- Total S-Length=5.87m (Z length 5.8m)



# Design using multipoles

## First order transfer map at the center

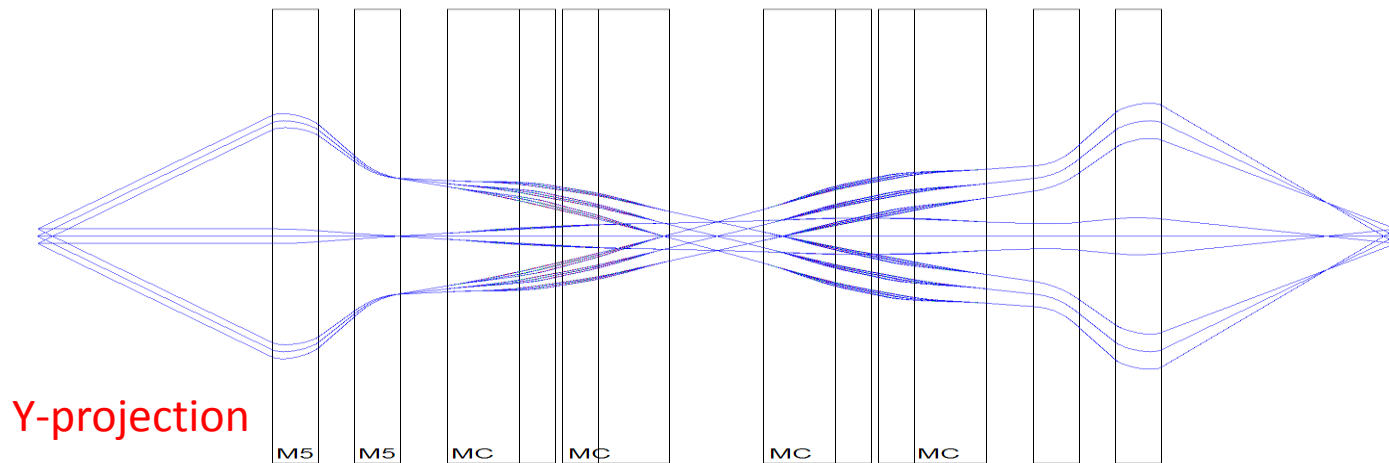
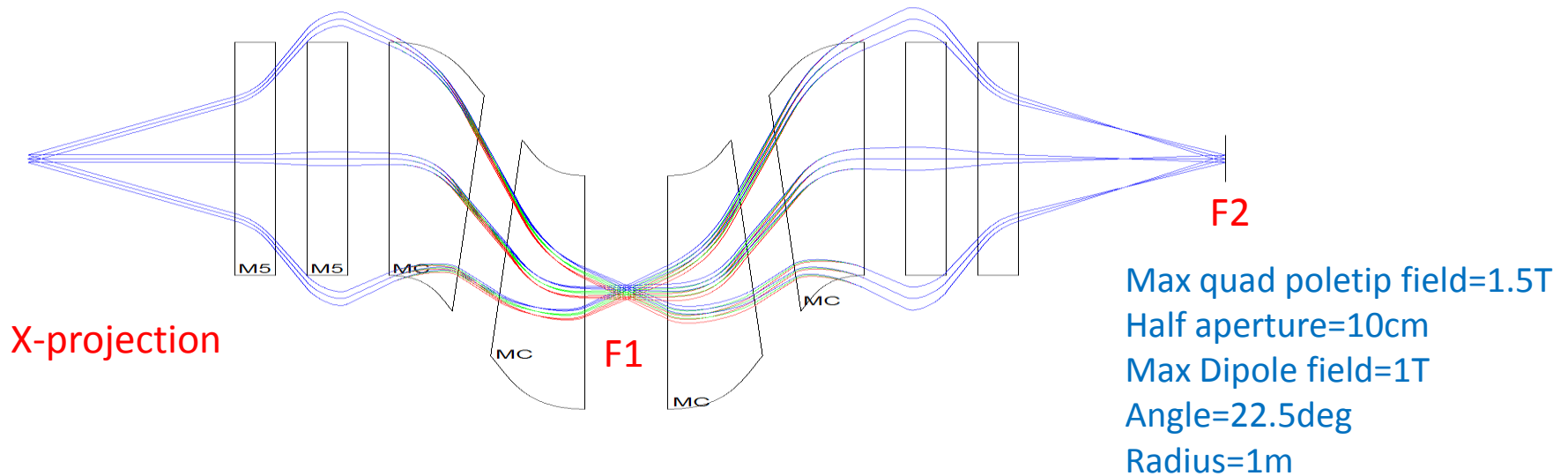
x	a	y	b	t	xaybtdmq
-0.6178139	-1.667354	0.0000000E+00	0.0000000E+00	-0.2131190	10000000
0.0000000E+00	-1.618610	0.0000000E+00	0.0000000E+00	-0.2068887	01000000
0.0000000E+00	0.0000000E+00	-1.981845	-0.8527079	0.0000000E+00	00100000
0.0000000E+00	0.0000000E+00	0.0000000E+00	-0.5045804	0.0000000E+00	00010000
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.0000000E+00	1.000000	00001000
0.1278187	0.0000000E+00	0.0000000E+00	0.0000000E+00	0.7465485	00000100
0.1266340	0.0000000E+00	0.0000000E+00	0.0000000E+00	-0.7076967	00000010
-0.2544527	0.0000000E+00	0.0000000E+00	0.0000000E+00	-0.3885182E-01	00000001

## First order transfer map at the end

x	a	y	b	t	xaybtdmq
1.000000	2.027434	0.0000000E+00	0.0000000E+00	0.0000000E+00	10000000
0.1363363E-09	0.9840816	0.0000000E+00	0.0000000E+00	0.0000000E+00	01000000
0.0000000E+00	0.0000000E+00	1.000000	3.326067	0.0000000E+00	00100000
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.9840816	0.0000000E+00	00010000
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.0000000E+00	1.016022	00001000
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.0000000E+00	1.517020	00000100
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.0000000E+00	-1.438071	00000010
0.0000000E+00	0.0000000E+00	0.0000000E+00	0.0000000E+00	-0.7894863E-01	00000001



# Design 1: Using Multipole magnets

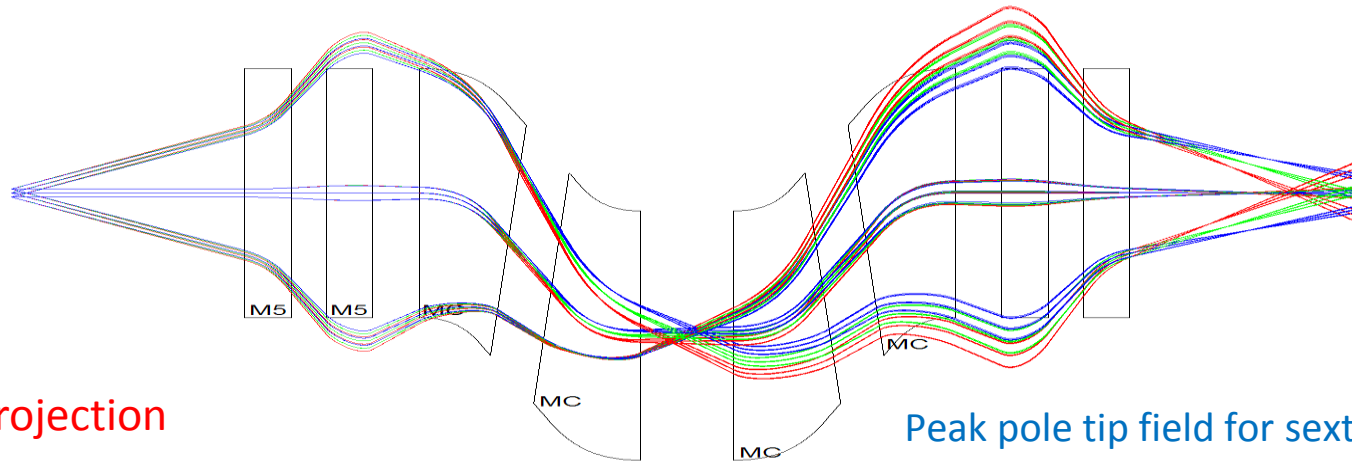


# Second Order Optics

- Peak pole tip field for sextupoles = 0.05 T at 10cm.
- First half (up to center of the device, dispersive image):
  - 4 sextupoles available for 2<sup>nd</sup> order aberration corrections
  - Two in multipole magnets (in the front)
  - Two in dipoles
  - Only two sextupoles (in dipoles) can be used for correcting chromatic terms
- Two options for the second half:
  - mirror symmetric to the first half
  - Independently tuned to reduce aberration at the final image

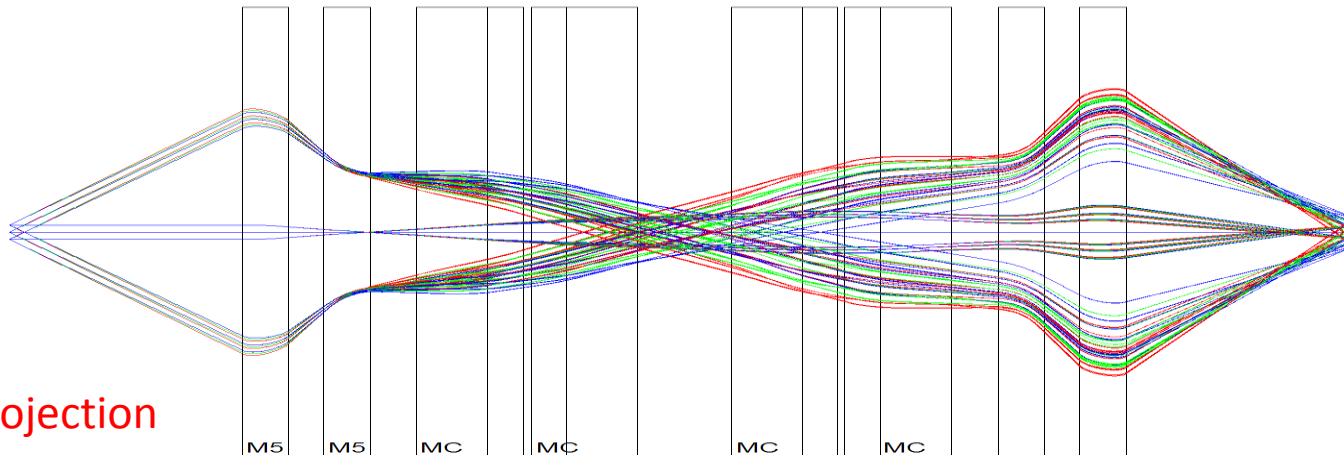


# Second order plots



X-projection

Peak pole tip field for sextupoles = 0.05 T  
Half aperture = 10cm



Y-projection





# Aberration at the center

Aberrations at the center of In-flight separator

Aberration Term	Before Correction (mm)	After Correction (mm)
(X,AD)	4.94	4.7
(X,AA)	2.79	0
(X,XA)	0.37	0.13
(X,XD)	0.24	0.23
(X,YB)	0	0.28
(X,DD)	0	0.11
(X,BB)	0	0.07
(Y,BD)	3	3.1
(Y,YD)	0.18	0.15
(Y,AB)	0.15	0.46
(Y,AY)	0	0.9
(Y,XB)	0	0.09
(Y,XY)	0	0.03



# Aberration at the End

Aberrations at the end of In-flight separator

Aberration Term	Befor Correction (mm)	After Corrections-Symm (mm)	After Correction (mm)
(X,AD)	16	15.3	15.6
(X,XD)	1	1	1
(X,YB)	0.08	0.9	0.2
(X,XA)	0	0.42	0.1
(X,YY)	0	0.09	0.08
(Y,BD)	3	3.1	3.1
(Y,AY)	0.07	0.9	0.23
(Y,YD)	0.33	0.34	0.33
(Y,XY)	0	0.06	0
(Y,YB)	0	0.9	0.23

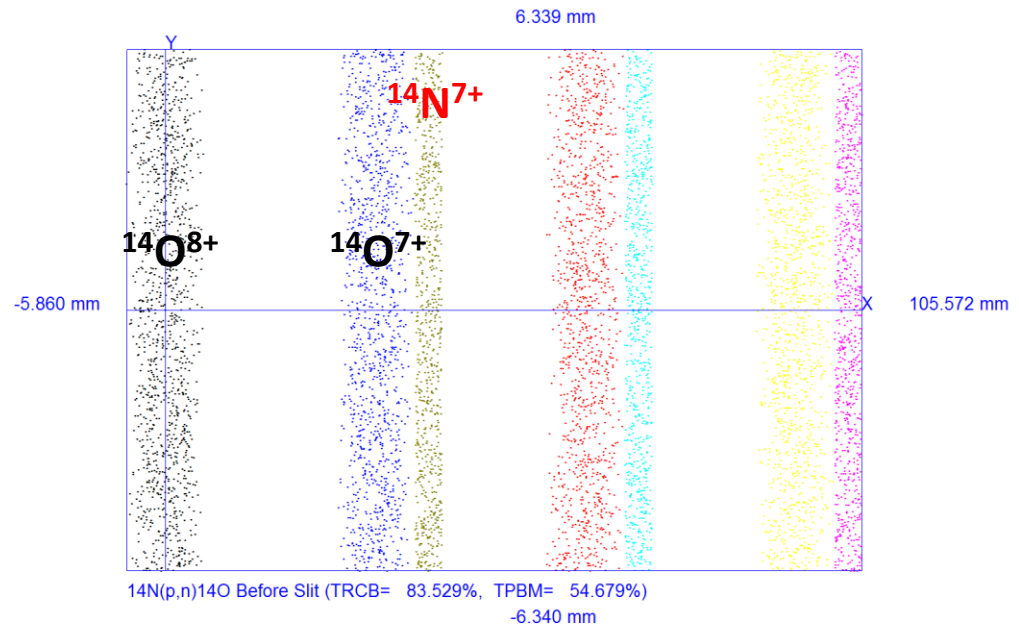


# $^{14}\text{N}(p,n)^{14}\text{O}$

Ion	Mass	Charge	BRHO	DBRHO(%)	Beta	QF
<b>Oxygen</b>	<b>14</b>	<b>8</b>	<b>0.743</b>	<b>0.000</b>	<b>0.135</b>	<b>1.000</b>
Oxygen	14	7	0.849	14.286	0.135	0.000
<b>Nitrogen</b>	<b>14</b>	<b>7</b>	<b>0.876</b>	<b>17.877</b>	<b>0.140</b>	<b>1.000</b>
Oxygen	14	6	0.991	33.333	0.135	0.000
<b>Nitrogen</b>	<b>14</b>	<b>6</b>	<b>1.022</b>	<b>37.523</b>	<b>0.140</b>	<b>0.000</b>
Oxygen	14	5	1.189	60.000	0.135	0.000
<b>Nitrogen</b>	<b>14</b>	<b>5</b>	<b>1.226</b>	<b>65.028</b>	<b>0.140</b>	<b>0.000</b>

Parameters from data files:

- Average spread for  $^{14}\text{O}$  (121 MeV)
  - $X=\pm 3.2\text{mm}$ ,  $Y=\pm 3.2\text{mm}$ ,
  - $\theta=\pm 50\text{mrad}$ ,  $d\text{KE}=\pm 2.2\%$  ( $\pm 3\%$ )
- Average spread for  $^{14}\text{N}$  (129 MeV)
  - $X=\pm 3.2\text{mm}$ ,  $Y=\pm 3.2\text{mm}$ ,
  - $\theta=\pm 75\text{mrad}$ ,  $d\text{KE}=6.6\% \pm 2.7\%$  (**0.1%**)
- Average spread for  $^{11}\text{C}$  (114 MeV)
  - $X=\pm 3.2\text{mm}$ ,  $Y=\pm 3.2\text{mm}$ ,
  - $\theta=\pm 105\text{mrad}$ ,  $d\text{KE}=-5.7\% \pm 2.7\%$

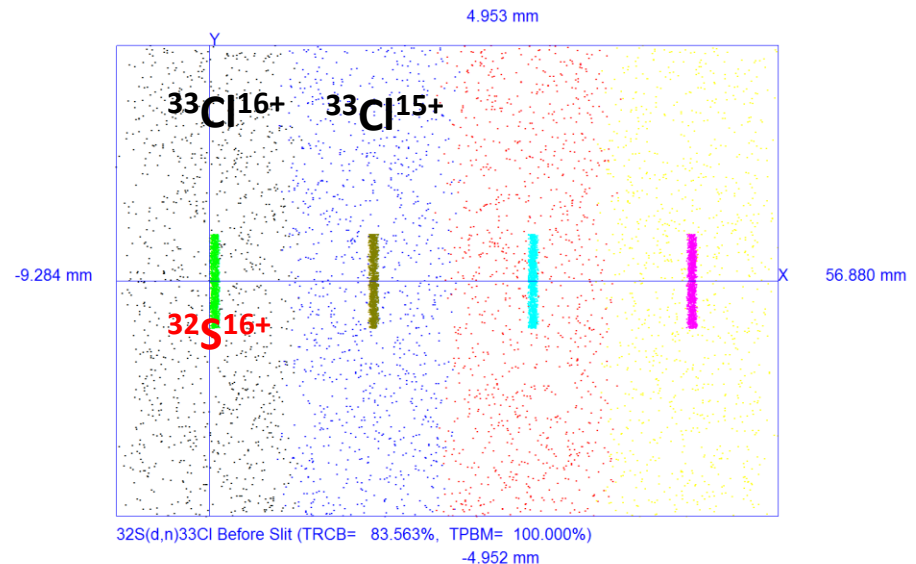


# $^{32}\text{S}(d,n)^{33}\text{Cl}$

Ion	Mass	Charge	BRHO	DBRHO(%)	Beta	QF
Chlorine	33	17	0.587	-5.882	0.097	0
<b>Chlorine</b>	<b>33</b>	<b>16</b>	<b>0.623</b>	<b>0</b>	<b>0.097</b>	<b>0.3</b>
Sulphur	32	16	0.624	0.164	0.1	1
Chlorine	33	15	0.665	6.667	0.097	0.3
Sulphur	32	15	0.666	6.842	0.1	0
Chlorine	33	14	0.712	14.286	0.097	0
Sulphur	32	14	0.713	14.474	0.1	0
Chlorine	33	13	0.767	23.077	0.097	0

Assumed input:

- Average spread for  $^{33}\text{Cl}$  (145 MeV)
  - $X=\pm 2.5\text{mm}$ ,  $Y=\pm 2.5\text{mm}$ ,
  - $\theta=\pm 50\text{mrad}$ ,  $d\text{KE}=\pm 6.15\%$
- Average spread for  $^{32}\text{S}$  (150 MeV)
  - $X=\pm 0.5\text{mm}$ ,  $Y=\pm 0.5\text{mm}$ ,
  - $\theta=\pm 5\text{mrad}$ ,  $d\text{KE}=3.45\% \pm 0.17\%$

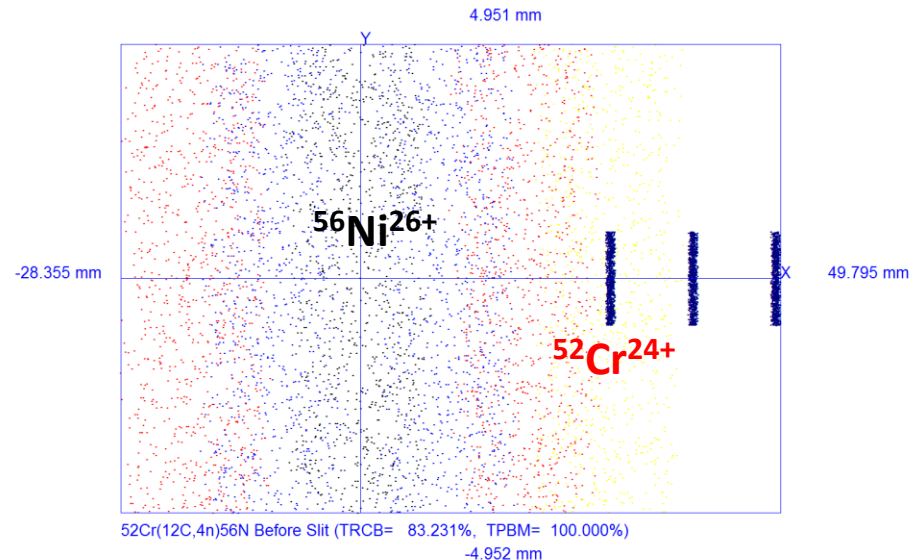


# 52Cr(12C,4n)56Ni

Ion	Mass	Charge	BRHO	DBRHO(%)	Beta	QF
Nickel	56	28	0.711	-7.143	0.114	0
Nickel	56	27	0.737	-3.704	0.114	0
<b>Nickel</b>	<b>56</b>	<b>26</b>	<b>0.765</b>	<b>0</b>	<b>0.114</b>	<b>0.3</b>
Nickel	56	25	0.796	4	0.114	0.3
Nickel	56	24	0.829	8.333	0.114	0
<b>Chromium</b>	<b>52</b>	<b>24</b>	<b>0.857</b>	<b>11.992</b>	<b>0.126</b>	<b>1</b>
Nickel	56	23	0.865	13.043	0.114	0
<b>Chromium</b>	<b>52</b>	<b>23</b>	<b>0.894</b>	<b>16.861</b>	<b>0.126</b>	<b>0</b>
<b>Chromium</b>	<b>52</b>	<b>22</b>	<b>0.935</b>	<b>22.173</b>	<b>0.126</b>	<b>0</b>

Assumed input:

- Average spread for 56Ni (**340 MeV**)
  - $X=\pm 2.5\text{mm}$ ,  $Y=\pm 2.5\text{mm}$ ,
  - $\theta=\pm 50\text{mrad}$ ,  $dKE=\pm 6\%$
- Average spread for 52Cr (**391 MeV**)
  - $X=\pm 0.5\text{mm}$ ,  $Y=\pm 0.5\text{mm}$ ,
  - $\theta=\pm 5\text{mrad}$ ,  $dKE=15\% \pm 0.23\%$

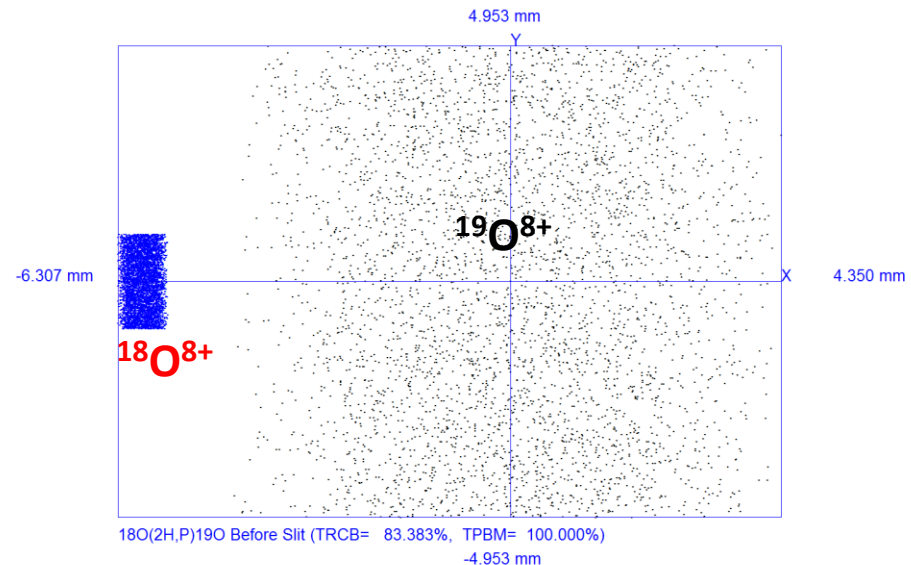


# 18O(2H,P)19O

Ion	Mass	Charge	BRHO	DBRHO(%)	Beta	QF
18Oxygen	18	8	0.998	-2.365	0.141	1
19Oxygen	19	8	1.022	0	0.137	1

Assumed input:

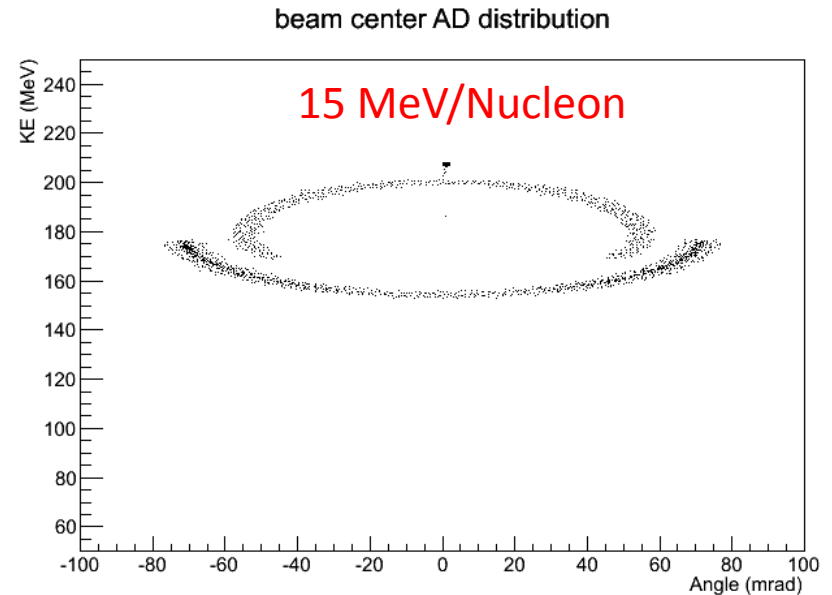
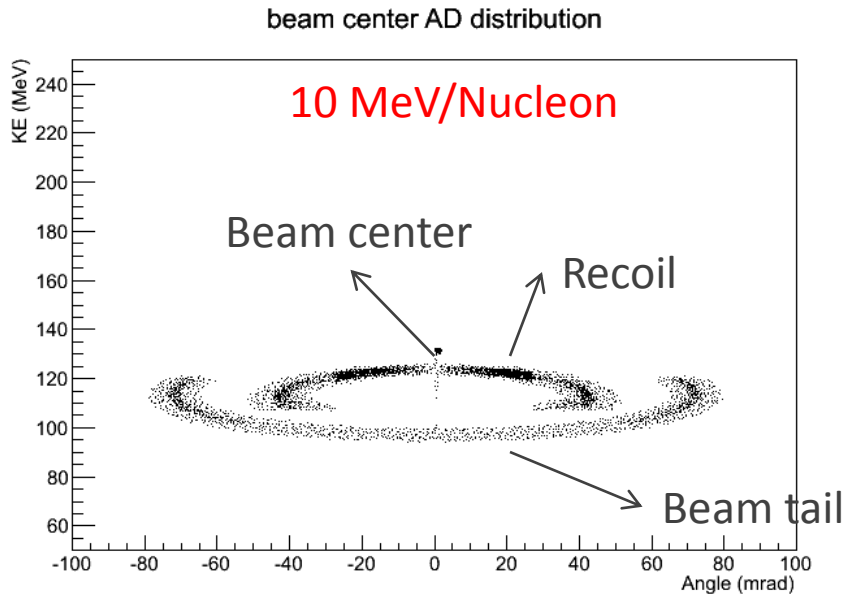
- Average spread for 19O (**169 MeV**)
  - $X=\pm 2.5\text{mm}$ ,  $Y=\pm 2.5\text{mm}$ ,
  - $\theta=\pm 50\text{mrad}$ ,  $dKE=\pm 2.26\%$
- Average spread for 18O (**170 MeV**)
  - $X=\pm 0.5\text{mm}$ ,  $Y=\pm 0.5\text{mm}$ ,
  - $\theta=\pm 5\text{mrad}$ ,  $dKE=15\% \pm 0.075\%$



High Pole tip fields for quads  $\approx 1.35\text{T}$  at 10cm



# $^{14}\text{N}(p,n)^{14}\text{O}$ case: Initial AD distribution



Ration of number of particle in recoil/beam tail:

- 1:10 for 15MeV/Nucleon case
- 1:2.5 for 10MeV/Nucleon case



# Final transmission (slit $\pm 5\text{mm}$ )

## 15MeV/nucleon case

	1 <sup>st</sup> order	1 <sup>st</sup> order + Fringe fields	2 <sup>nd</sup> order	2 <sup>nd</sup> order+ Fringe fields	5 <sup>th</sup> order+ Fringe fields
Recoil	92.33%	91%	89.8%	88.67%	78.42%
Beam tail	5.27%	4.21%	15.7%	13.5%	11.5%
Beam Center	0%	0%	2.5E-3	2E-3%	0%

## 10 MeV/nucleon case

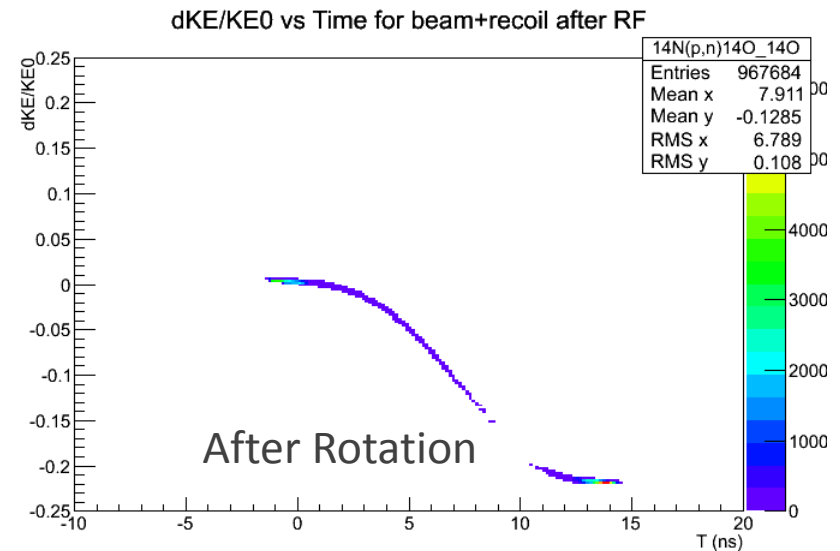
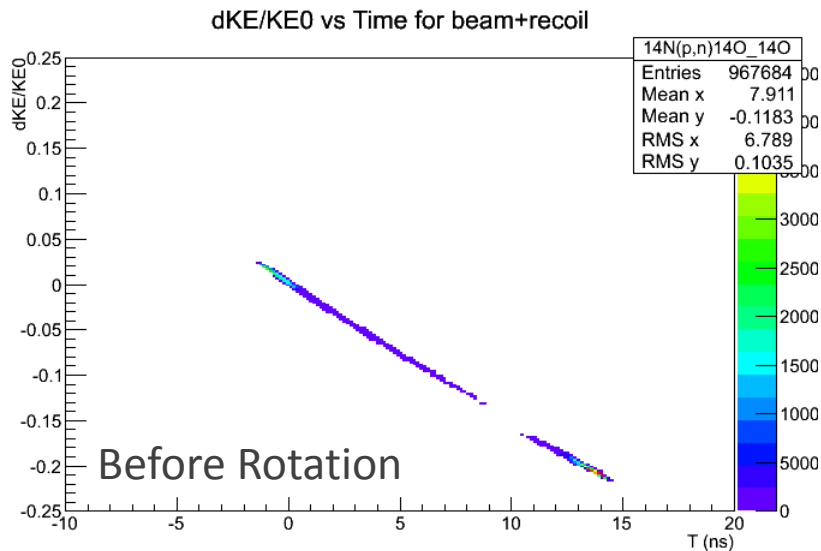
	1 <sup>st</sup> order	2 <sup>nd</sup> order	5 <sup>th</sup> order
Recoil	65%	66%	64%
Beam tail	1.7%	7.36%	7.6%
Beam Center	0%	1E-4%	0%





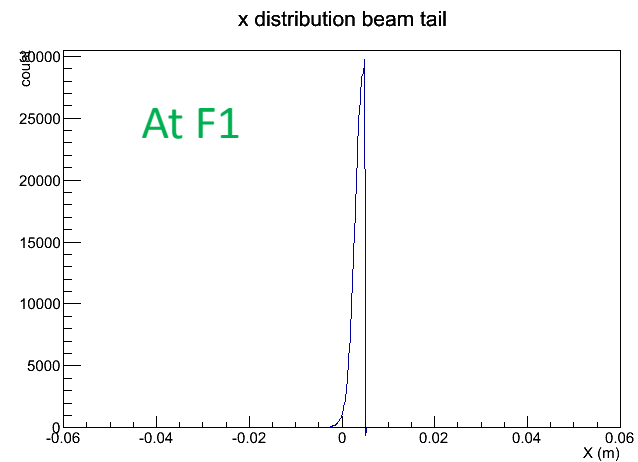
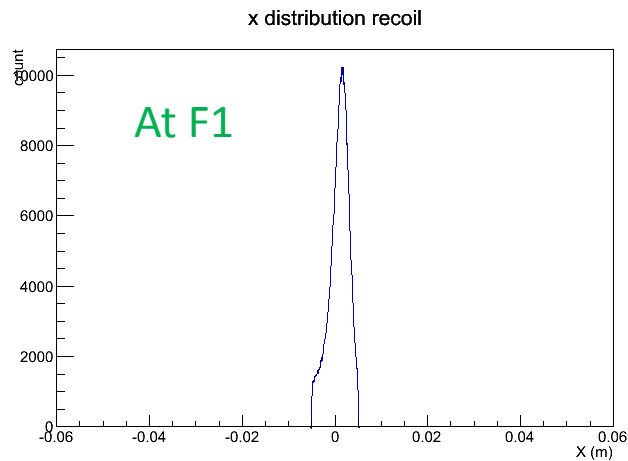
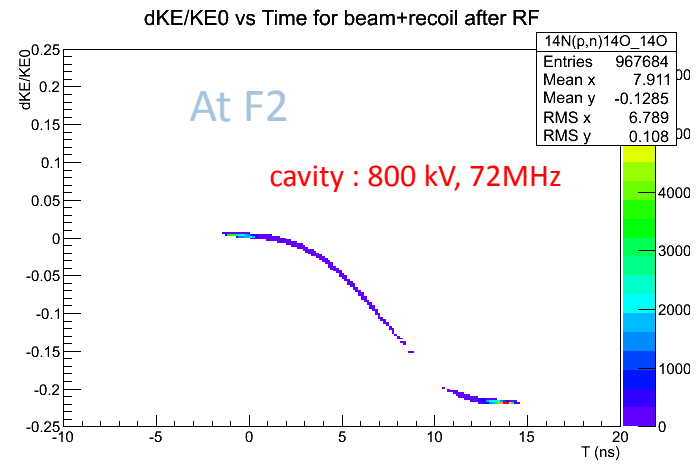
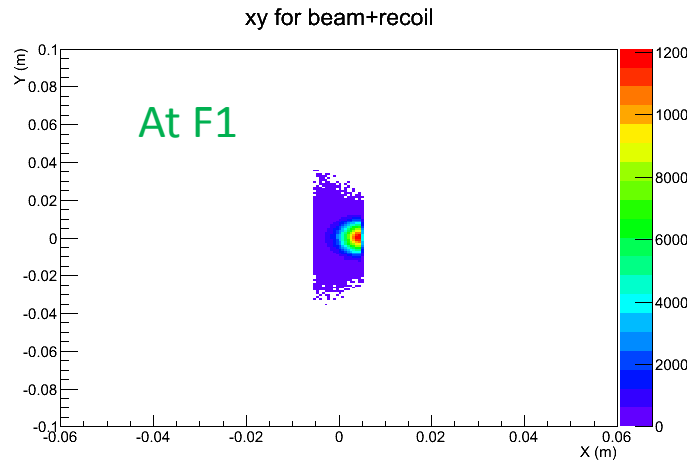
# Rotation in T-dKE phase plane

- RF Parameters:
  - Field = 4 MV/m
  - Length = 10 cm (voltage = 800 kV)
  - frequency = 72 MHz
  - Phase = 0 deg
  - Half aperture = 2cm



# 5<sup>th</sup> order with Fringe fields

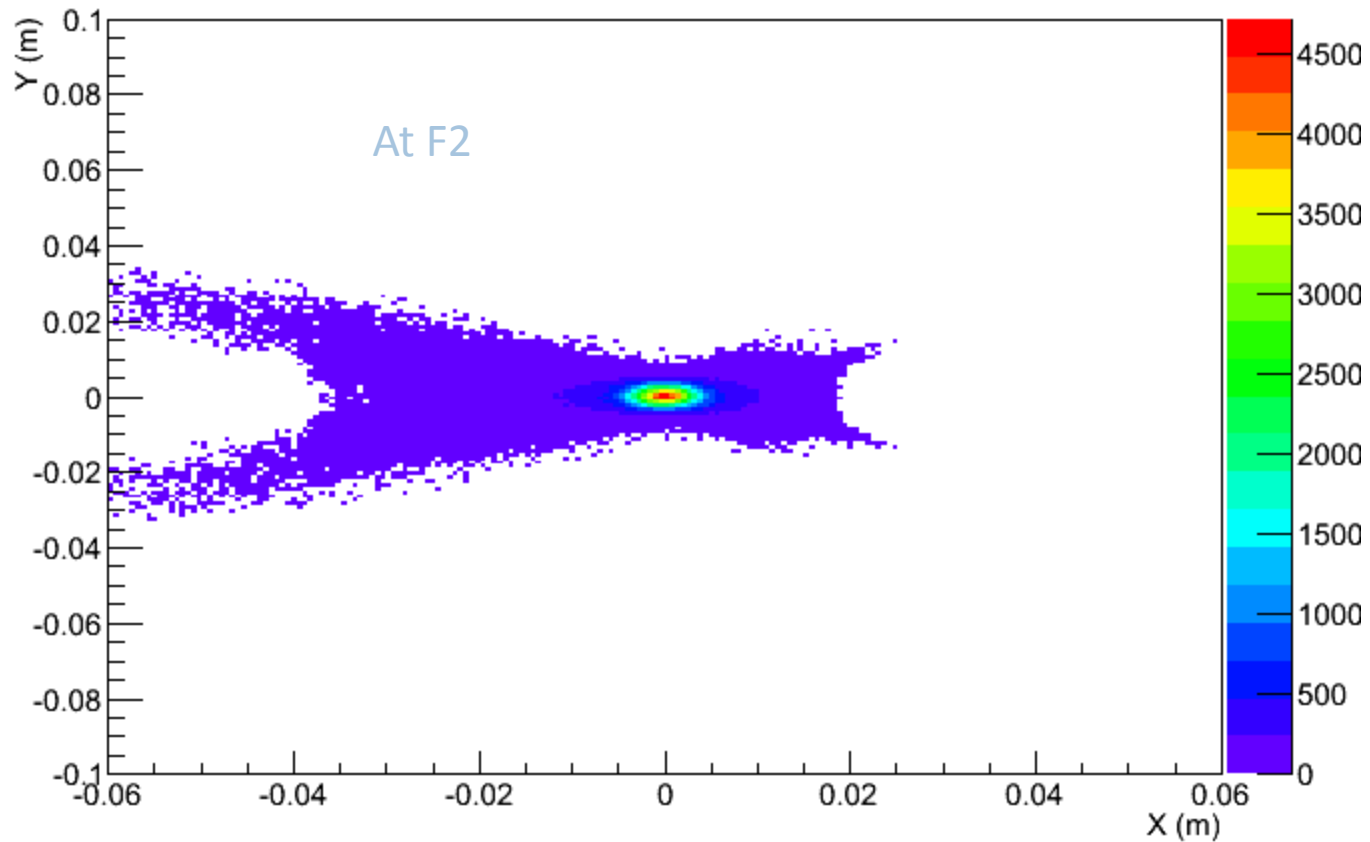
15MeV/nucleon case



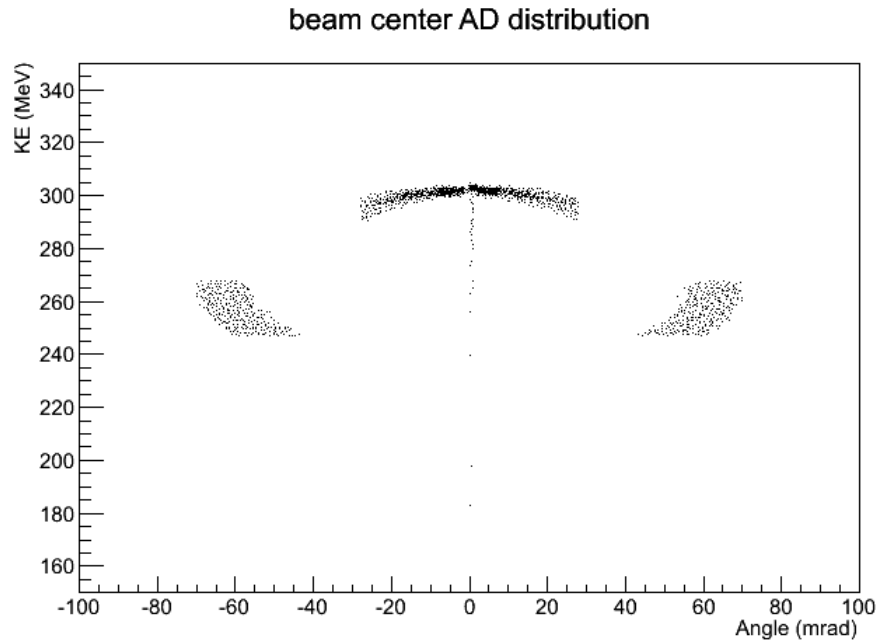
# $^{14}\text{N}(p,n)^{14}\text{O}$ case

15MeV/nucleon case

xy distribution recoil



# 32S(d,n)33Cl case



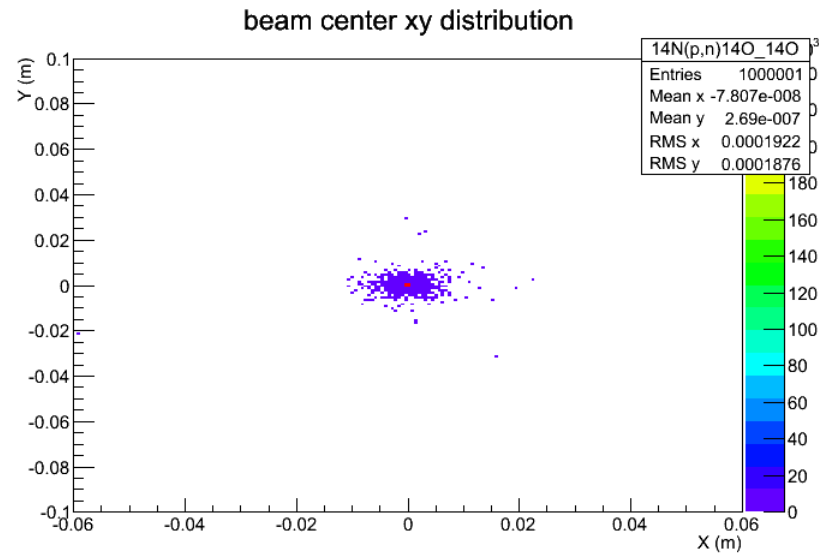
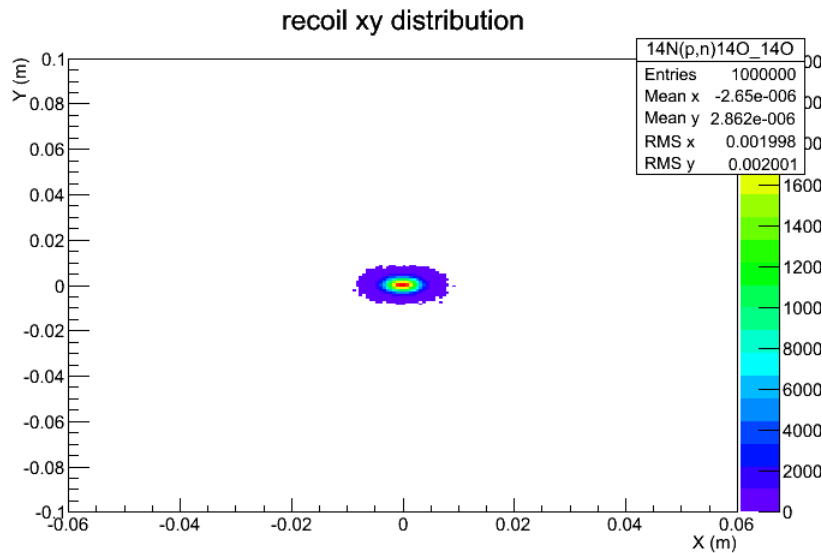
Beam tail [247,267] MeV

Ion	Mass	Charge	BRHO	DBRHO(%)	Beta	QF
Chlorine	33	17	<b>0.846</b>	0.000	0.139	0.618
Sulphur	32	16	<b>0.888</b>	5.021	0.142	1.000
Chlorine	33	16	<b>0.899</b>	6.250	0.139	0.344
Chlorine	33	15	<b>0.959</b>	13.333	0.139	0.036
Chlorine	33	14	<b>1.027</b>	21.429	0.139	0.001

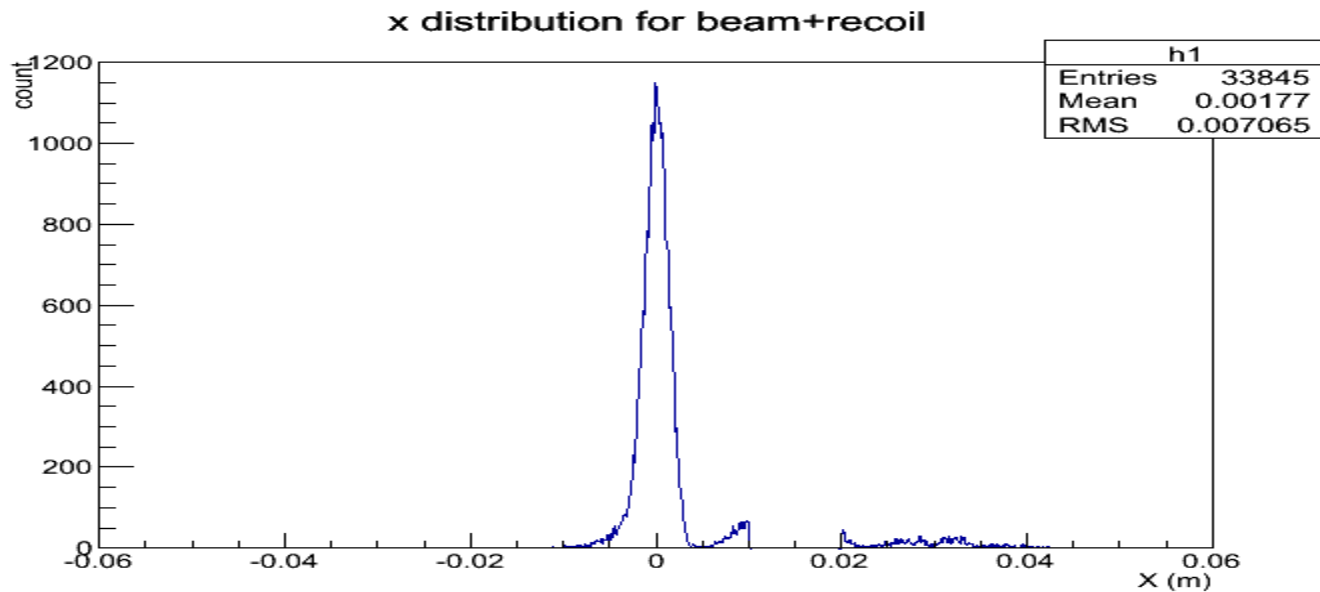
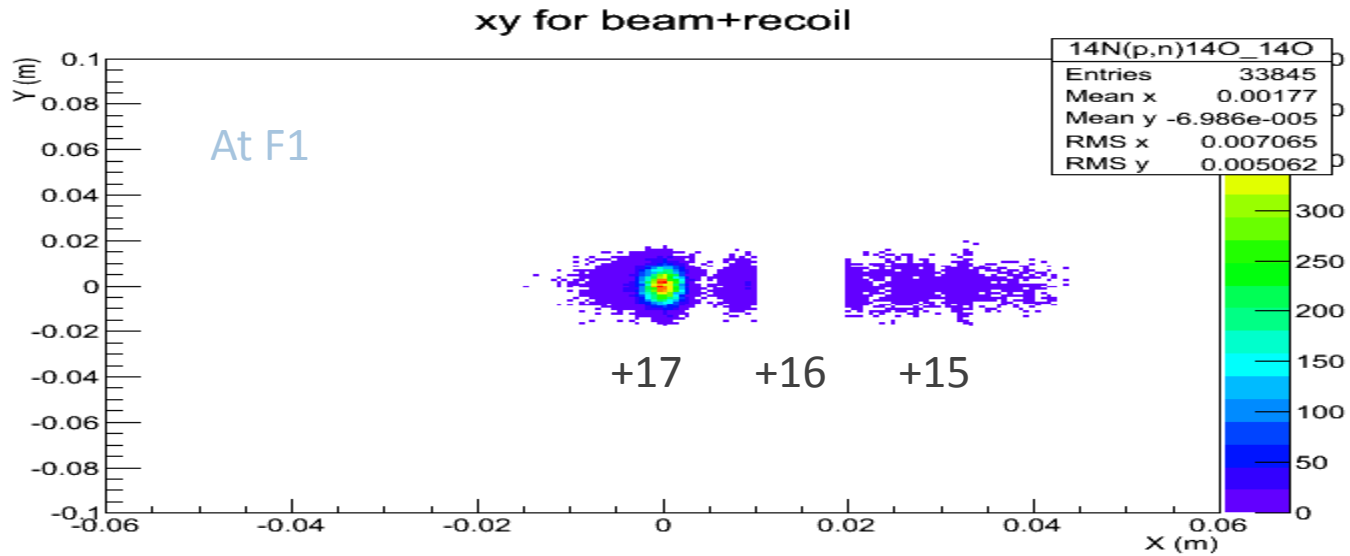


# Input beam

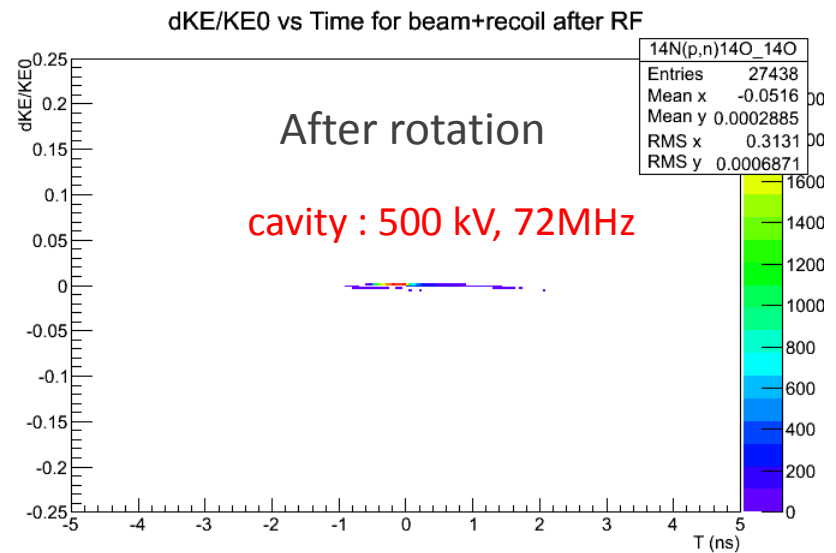
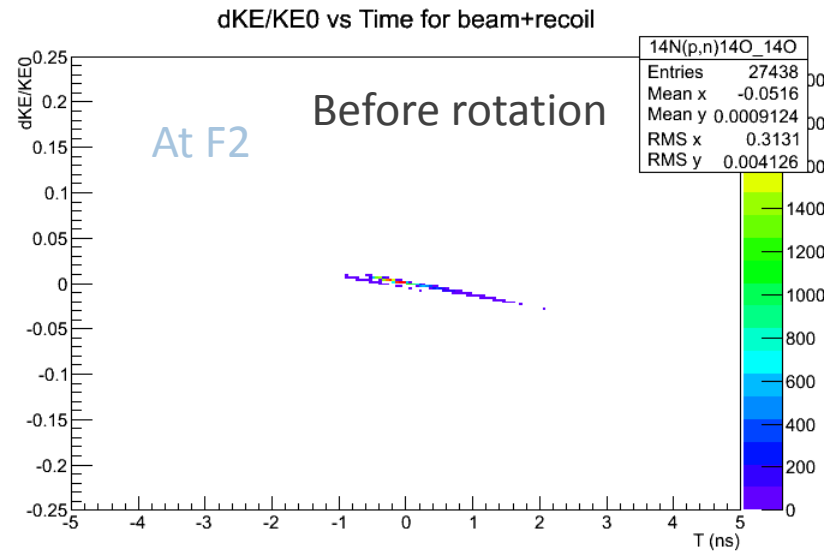
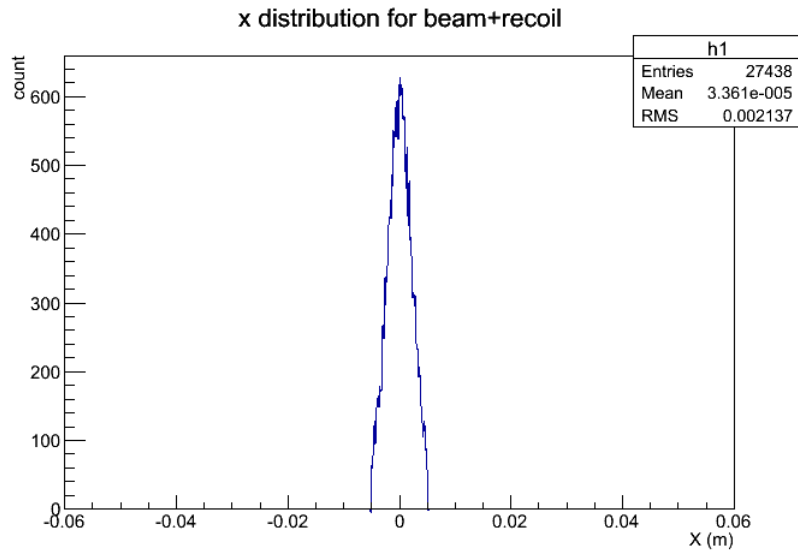
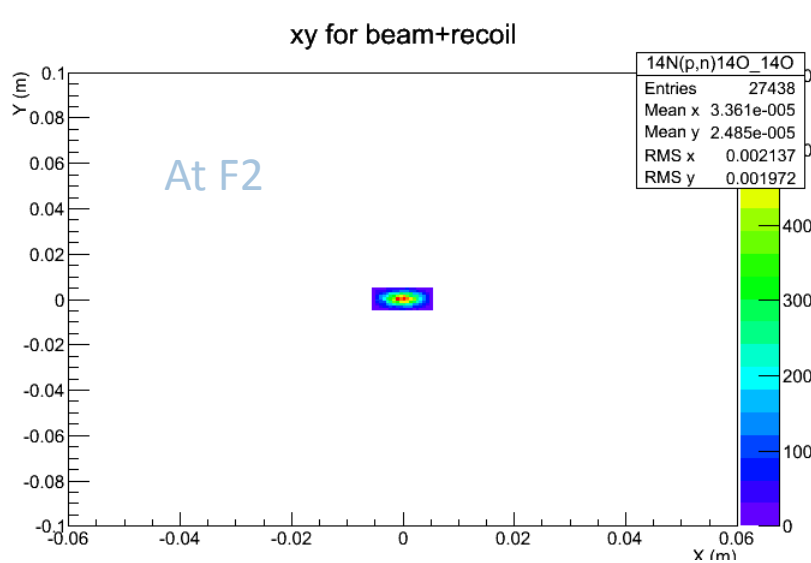
- 9 MeV/nucleon average energy for  $^{33}\text{Cl}$  (+17)
- beam blocker at the center of the device ( $15\text{mm} \pm 5\text{mm}$ )
- Slit at the final focus ( $\pm 5\text{mm}$ )



# Design 1: 5<sup>th</sup> order with Fringe fields



# Design 1: 5<sup>th</sup> order with Fringe fields



# Transmission

	Fraction	5 <sup>th</sup> order+ Fringe fields	5 <sup>th</sup> order+ Fringe fields (with beam blocker)	5 <sup>th</sup> order+ Fringe fields (beam blocker+endslit)
Recoil (+17)	61.8%	100%	100%	87.3%
Recoil (+16)	34.4%	100%	8%	0%
Recoil (+15)	3.6%	100%	93%	28.3%
Recoil (+14)	0.1%	100%	100%	27.5%
Beam Center	NA	100%	0.04%	0
Beam Tail				

Recoil transmission with beam blocker=**68%**

Recoil transmission with beam blocker + end slit=**55%**





# Conclusion and Future Work

- The advantages of AIRIS design was presented
  - Proposed second order corrected design achieves a combination of beam suppression, evaporation residue transmission
  - 10 times collection efficiency improvement
  - 2 orders of magnitude gain in intensity when combined with other ATLAS upgrades
- Performance of the device for two representative reaction cases was shown
- Future work :
  - Realistic simulation of more reaction cases
  - Higher order optimization to improve transmission as well as separation
  - Simulations with inclusion of realistic fringe fields

Thank you!

