ANALOG DAMPERS IN THE FERMILAB BOOSTER
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Abstract
With the increase in intensity of the Fermilab Booster accelerator to over \(3 \times 10^{12}\) \(p/\text{pulse}\), active dampers have been required to control several transverse and longitudinal instabilities. The damper systems currently in use are: one narrow-band horizontal damper for the \((+Q_h)\) mode, a wideband horizontal damper for all modes, and four channels of narrow-band longitudinal dampers for coupled bunch modes 1, 48, 49, and 50. We discuss the observations that indicated that damper systems were necessary, the designs and operations of the systems, and their effects on beam quality in the Booster.

INTRODUCTION
The Fermilab Booster Accelerator is the lowest energy synchrotron in the Fermilab complex. The injected beam consists of (400 MeV protons provided by the Linac, and the 8 GeV extracted beam is injected into the Main Ring. The desired quality of the extracted beam is determined by the apertures of the Main Ring. In order to extract \(3 \times 10^{12}\) \(p/\text{pulse}\) from the Main Ring, the Booster transverse emittances must be less than \(17 \pi \text{mm-mrad}\) and \(\Delta p/p\) must be less than \(1.5 \times 10^{-3}\).

At Booster intensities of \(3 \times 10^{12}\) \(p/\text{pulse}\) (much below the \(4 \times 10^{12}\) \(p/\text{pulse}\) needed to extract \(3 \times 10^{12}\) \(p/\text{pulse}\) from the Main Ring) we observed coherent instabilities in the Booster which severely degraded the quality of the beam injected into the Main Ring. The horizontal emittance often exceeded \(35 \pi \text{mm-mrad}\), and the longitudinal coupled bunch oscillations led to beam loss due to the restricted momentum aperture of the Main Ring. We undertook an effort to identify the unstable modes and provide active damping to counteract them.[1] Partly as a result of this program, the Booster has run with intensities of over \(4.0 \times 10^{12}\) \(p/\text{pulse}\) with emittances acceptable to the Main Ring.

We have installed three different types of damper systems: a narrow band horizontal damper acting upon the \((+Q_h)\) mode, a wideband horizontal damper, and longitudinal narrow band dampers acting on non-specific coupled bunch modes. We will describe the measurements indicating the existence of the unstable modes and the designs of the damper systems.

UNSTABLE MODES AND DAMPERS

Horizontal Modes
The first horizontal mode identified was a mode which appeared during the last half of the Booster accelerating cycle at a frequency of approximately 180 KHz, corresponding to the lowest horizontal sideband. The horizontal tune is normally 6.7, the revolution frequency during the second half of the cycle 626 KHz, so the unstable mode is \((7-Q_h)\). We believe that this is a resistive wall mode which is strongly driven at low frequencies. This instability is very strong and dominates the horizontal spectrum.

Figure 1. Schematic diagram of the horizontal narrow band damper system.

Figure 2. Signal on a horizontal BPM before (a) and after (b) installation of the horizontal narrowband amper.

Fig. 1 is a diagram of the damper system used to reduce this oscillation. The beam oscillations are detected using the difference signals on two BPMs 104° apart in betatron phase. After mixing to baseband with the Booster VCO and filtering, the proper phase is established using the two time-dependent ramps.
which multiply the processed BPM signals. The signals are then summed, put through a bandpass filter centered at 120 KHz to reject the synchrotron frequency on the low frequency side and the \((Q_h-6)\) line at approximately 450 KHz on the high frequency side, mixed back up to 53 MHz, and then put into a power amplifier and sent to the kickers. The overall system gain is roughly 112 db.

Figs. 2a and 2b are plots of the signal on a single BPM before (a) and after (b) installation of the damper system.

Once installed, this damper eliminated any significant mode \((+Q_h)\) oscillation (Fig. 1b). However, the emittance was still larger than acceptable for the Main Ring. Examination of the frequency spectrum of a BPM showed that although the mode \((+Q_h)\) frequency was completely absent, oscillations developed at the other mode frequencies, indicating the need for a wideband damper. The system we installed (Fig. 3) uses the difference signal for a BPM. After being mixed down to baseband, filtered, and delayed, the output signal is summed with the signal from the narrow band damper and applied to the same kicker. The phase response of this damper is flat over the frequency range 0-26 MHz and the gain ranges from 20 db at low frequencies to about 7 db at 26 MHz. It has not been necessary to install equalizers. With the installation of this damper system, horizontal instabilities do not appear at intensities of \(4.0 \times 10^{12}\) p/s/pulse.

**Figure 3.** Schematic diagram of the horizontal wide band damper system.

**CONCLUSIONS**

Elimination of transverse and longitudinal instabilities has allowed the Booster to produce extracted intensities of \(4 \times 10^{12}\) p/s/pulse with low emittances. We look forward to increasing the intensities and dealing with the next set of instabilities.

**References**


Figure 5. Error signals for the longitudinal dampers with dampers off (a) and on (b). From top to bottom, the modes are 1, 48, 49, and 50.