# Geodetical Concept and Alignment of COSY 

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## Abstract

The concept of the geodetical system and the instrumental equipment are briefly described. First results of measurements are shown.

## Tolerances

Exact positioning of the ion optical elements with respect to the closed orbit is essential for high beam quality. Figure 1 shows the distortion of closed orbit due to misalignment. This simulation assumes a deviation of dipoles and quadrupole magnets by $\pm 0,2 \mathrm{~mm}$ in the vertical plane and a tilt of $\pm 0,1 \mathrm{mrad}$ for quadrupoles and $\pm 0,3 \mathrm{mrad}$ for dipole magnets. Detailed theoretical analysis shows a strong dependence of misalignment of neighbouring components.


Figure 1:
Deviation from central orbit

Thus the overall alignment tolerances were specified $\pm 0,2 \mathrm{~mm}$ in all directions and a max. twist of $\pm 0,1$ mrad with a misalignment of neighbouring components of max. $0,1 \mathrm{~mm}$ in all directions.

Additionally short measurment and alignment time were requested to enable long running periods for accelerator and experiments.

## Lattice

50 reference points forming a lattice are the basis for precise geodetical measurement and alignment in the COSY facility. Figure 2 shows the distribution of the reference points in the injector cyclotron, beam lines, experimental areas and the COSY ring.


Figure 2:

Due to the thigter tolerances and a common observation height of $2,8 \mathrm{~m}$ for all target points in the COSY ring, teel pillows are installed as reference and measurement points. The pillow: are thermaly isolated to prevent bending due to asymmetric heat radiation (cold wall, hot magnet coils).

## Instrumentation

Bearings with diameter of 30 mm and a tolerance of max. $0,0005 \mathrm{~mm}$ (identical to CERN and SIN) are used for precise mounting of optical targets and measurement equipment. According to the measurement problem different types of optical targets are available (rank precision balls, illuminated targets for direction and plumbing and invar bars for leveling).

Instrumentation for measurement is listed in table 1.

Table 1
Geodetical instruments

| direction | Wild T 200 OS | 0,5 mpm |
| :---: | :---: | :---: |
| distance |  |  |
| up to 4 m | micrometer | $0,1 \mathrm{~mm}$ |
| up to 6 m | stadion rod | $0,1 \mathrm{~mm}$ |
| 4 to 70 m | ME 5000 | $0,1 \mathrm{~mm}$ |
|  |  | resp. 0,1 ppro |
| niveau | N3 Wild | $\pm 0,02 \mathrm{~mm}$ |
|  | N1 Zeiss | $\pm 0,02 \mathrm{~mm}$ |
| plummet | Nadirlot NL | $\pm 0,02 \mathrm{~mm}$ |
| inclination | Coincidence |  |
|  | libelle Zeiss | $\pm 0,01 \mathrm{~mm} / \mathrm{m}$ |
|  | Minilevel II | $\pm 0,02 \mathrm{~mm} / \mathrm{m}$ |
|  | Whyler |  |

## Software

All measured data are checked for confidence and plausibility during measurement and stored in a computer for detailed calculation with the program system PANDA [1]. The main features of this program system are:

- data base management for all measurement periods
- mesh relaxation
- comparison of actual and rated value
- alignment vectors
- trend analysis from different campaignes


## Results

Figure 3 shows the error ellipses of the reference points in the second measurement campaigne. Table 2 shows the measured values. With this accuracy of the reference points the misalignment error of the accelerator components is slightly better than the specified values.


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Figure 3:
Uncertainty of reference points

Table 2

| Reference COSY ring |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 2. Campagne September 1990 |  |  |  |  |
| Point | Coordinates |  | Access of error ellipse |  |
| No. | xm | ym | A | B |
|  |  |  | MM | MM |
| 1001 | 80.3306 | 101.1017 | . 03 | . 02 |
| 1002 | 119.6393 | 101.0304 | . 04 | . 03 |
| 1003 | 119.7245 | 82.6071 | . 04 | . 03 |
| 1004 | 128.8108 | 83.2318 | . 04 | . 03 |
| 1005 | 135.7903 | 91.8612 | . 04 | . 03 |
| 1006 | 137.7917 | 101.5077 | . 05 | . 03 |
| 1007 | 134.8532 | 109.8694 | . 04 | . 03 |
| 1008 | 128.5319 | 115.6754 | . 04 | . 03 |
| 1009 | 119.6917 | 117.4052 | . 04 | . 03 |
| 1010 | 80.4025 | 117.3896 | . 04 | . 03 |
| 1011 | 71.6967 | 115.6762 | . 03 | . 03 |
| 1012 | 65.1774 | 109.7871 | . 04 | . 03 |
| 1013 | 62.2483 | 101.0848 | . 03 | . 03 |
| 1014 | 64.2693 | 91.8234 | . 04 | . 03 |
| 1015 | 70.9135 | 84.7318 | . 03 | . 03 |
| 1016 | 80.3438 | 82.5999 | . 03 | 03 |

Due to weight of building, shielding and the accelerator components differential settlement of the total plant were expected.

During the construction phase several precission nivellements were performed to observe time dependence of the settlement.

The last measurement 14 month after finishing the bottonplate shows that the settlement has decayed to less than $0,5 \mathrm{~mm}$ per half year. Figure 4 shows the isolines of the $\operatorname{COSY}$ hall for all level measurements accuracy of better than $0,1 \mathrm{~mm}$ was achieved.


Figure 4:
Differential setting of COSY-hall

## REFERENCE

[1] GEOTEC (Forschungsgesellschaft für angewandte geodätische Technologie)

