

Figure 3: Input Coupler for Injector Cavities.

Couplers will be assembled to cavity in the clean-room before installation to a cryostat, so it should be short as possible. Then thermal intercept becomes difficult, and requires the 5k and 80k anchors at outer conductors. Inner conductors and the windows are cooled by water. High power test of a pair of couplers (Figure 4.) was performed using a newly developed 300kW CW klystron. Couplers were tested up to 100kW, so far. Farther test is planed in autumn.

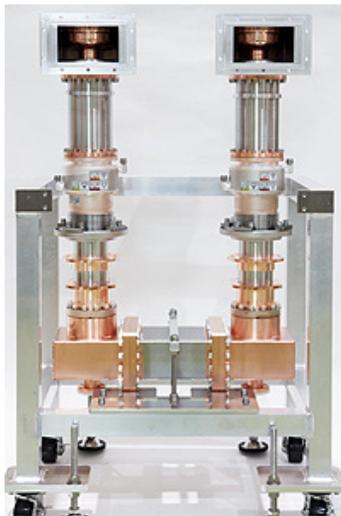


Figure 4: Prototype Input Coupler

HOM COUPLER

We decided to use HOM couplers instead of beam pipe HOM absorbers to damp HOMs, because absorbers are not well established in cold and they need extra drift space. TESLA –type HOM couplers are considered as the best choice, but it is well known that thermal instability appears above 10 MV/m in the CW operation. It is also well known that heating happens at pick-up proves of HOM couplers, but it is not yet understood why niobium antenna becomes normal conducting. One may expect that if the current density at antennae is reduced, the threshold gradient increases. TESLA HOM couplers are modified by introducing second stub and a boss as can be seen in Figure 5 [3]. Figure 6 shows the H field distribution of the modified HOM coupler, the H field is reduced by a half, to 2000 A/m at 15 MV/m. The first cold test was performed with these HOM couplers. After some processing, we could rise the gradient to 30 MV/m. Heating appeared in one HOM coupler, but we could keep the gradient of 16 MV/m for 6 hours. Major HOMs are summarized in Table 2.

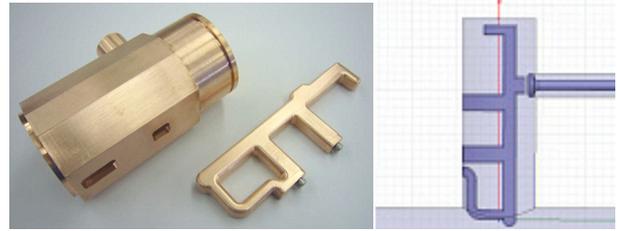
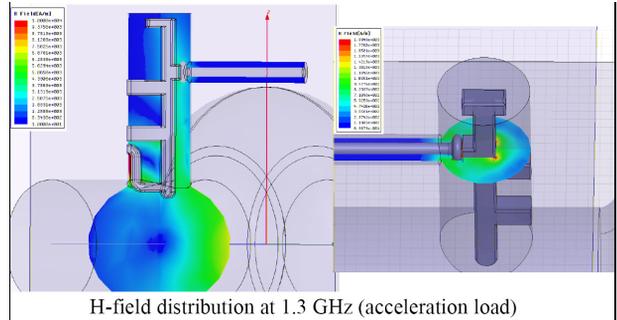


Figure 5: Two Stub HOM Coupler



H-field distribution at 1.3 GHz (acceleration load)

Figure 6: H-Field Distribution

Table 2: Major HOMs in 5 loop-type HOM couplers

Mode	Frequency	R / Q	Measured Q_L
TE111	1.54 GHz	0.59 Ω/cm^2	900
	1.60 GHz	1.8 Ω/cm^2	500
TM110	1.77 GHz	4.0 Ω/cm^2	400
	1.80 GHz	1.9 Ω/cm^2	3500
TM011	2.26 GHz	64 Ω	900
	2.30 GHz	12 Ω	1200
TM020	2.67 GHz	0.4 Ω	
	2.69 GHz	31 Ω	

FREQUENCY TUNER

We will use Slide Jack tuners [4, 5] which are used in STF cavities as is shown in Figure 7. Two pairs of wedge are set on both side of jacket cylinder flanges and driven by one shaft from outside of a cryostat. One piezo system is put in series with a slide jack tuner, and will be replaceable from a cryostat opening. Stroke of the tuner is listed in Table 3.



Figure 7: Slide Jack Tuner

Table 3: Stroke of the tuner

	Type	Stroke	Δf
Mechanical Tuner	Slide Jack	1mm	1.3MHz
Fine Tuner	Piezo	4 μ m	2.6kHz

CRYOSTAT

Figure 8 and 9 show a cryostat containing three 2-cell cavities. Final design is in progress. Cavities are dressed with He vessel made of Titanium, and magnetic shields are put inside of He vessel. The estimated cryogenic load in 100mA and 10MV operation is summarized in Table 4. As is seen from this table, it is critical to take dynamic load of input couplers and HOM power extraction cables. They will be anchored to 4.5k reservoir panels put on both side of cavities, which works as a thermal shield as well. Because of this difficulty the operating gradient may be lowered.

Table 4: Cryogenic Load per Cavity

	2k		4.5k	
	Static	Dynamic	Static	Dynamic
Cavity	0	6W	0	0
Input Coupler	2W	4W	8W	16W
HOM Cable	1W	7W	5W	14W
Beam Pipe	1W	0	2W	0
Others	5W	0	10W	0
Total	9W	17W	25W	30W

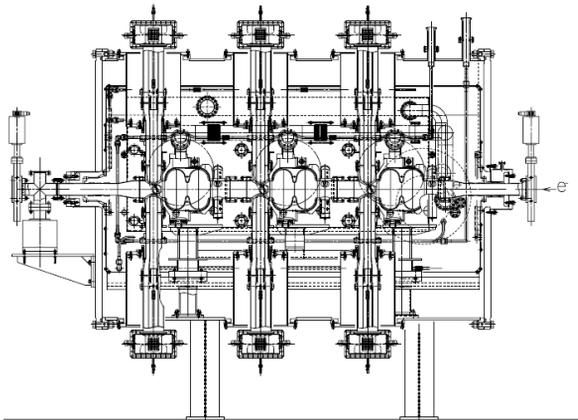


Figure 8: Injector Cryomodule

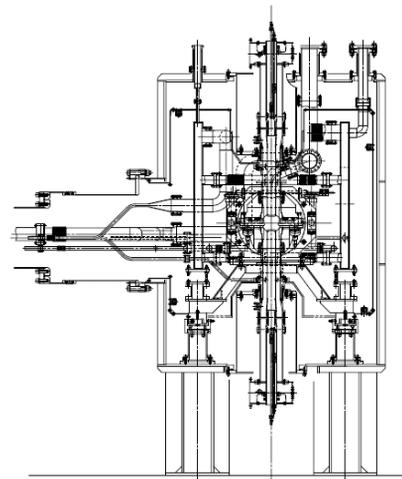


Figure 9: Injector Cryomodule

SUMMARY

Development of Injector cryomodule is in progress. Assembly of cryomodule is scheduled in late 2011. Depending on test results, the number of cavities for the real ERL may be increased to 4.

REFERENCES

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